LIST OF APPENDICES

FEMA has worked to ensure that this EA document is accessible to persons with disabilities, in compliance with Section 508 of the Rehabilitation Act of 1973. Regarding the EA's Appendices, which are provided in a separate document, this EA has reported what was done and how those results affect the decision that will be made based on the totality of the EA findings. In case any of these appendices poses a challenge to be read electronically by persons with disabilities, each appendix is briefly described and summarized below, rather than being simply listed.

Appendix 1. New St. Louis Catholic High School Campus Plans. This 377-page set of construction drawings is dated April 2022. They were prepared by RHH Architects, Associated Design Group, Inc., and Champeaux, Evans, Howard Architects. Due to the inability to make all of the above documents 508 accessible and below our size constraints, they are not included in the published EA but are available by request. The first twenty pages of plans are included in Appendix A of the published EA. Should you have any questions, please contact Tiffany Spann-Winnfield at 504-218-6800 or tiffany.spann@fema.dhs.gov.

Appendix 2. DOLC New SLCHS Property Geo Tech Report. This 96-page study was prepared by Terracon Consultants, Inc dated July 28, 2023. This report presents the findings of the subsurface exploration and provides geotechnical recommendations concerning earthwork and the design and construction of foundations, floor slabs, and pavements for the proposed project. The geotechnical exploration Scope of Services for this project included the advancement of 44 test borings to depths ranging from approximately 6 to 50 feet below existing site grades.

Appendix 3. NRCS USDA Soil Map. This appendix contains the NRCS USDA Soil Map that is provided in its entirety. Page 1 shows an image of the proposed site of relocation with lines indicating the different soil types present. Page 2 shows the legend of the map and page 3 the actual findings from the Web Soil Survey. Map was prepared on August 23, 2023.

Appendix 4. Wetland Delineation. This 52-page Wetland Delineation Report was provided on October 23, 2023. This appendix contains the findings of Southland Environmental, LLC of the 47-acre tract located East of Corbina Road in Lake Charles, Calcasieu Parish. The report discusses findings of vegetation, soils, and hydrology. It was found that this was an undeveloped pastured land with Mowata-Vidrine and Crowley-Vidrine silt loams, and 6.1 acres of wetlands present within the tract boundary. Due to the inability to make the USACE Wetland Determination Data Sheets documents 508 accessible they are included with alternate text in the published EA but are also available by request in their entirety. Should you have any questions, please contact Tiffany Spann-Winnfield at 504-218-6800 or tiffany.spann@fema.dhs.gov.

Appendix 5. EPA Sole Source Aquifer Program Response Letter. This 2-page document was received on December 12, 2023. This appendix contains the EPA determination that the project, as proposed, should not have an adverse effect on the quality of the ground water underlying the project site. This approval is based solely upon the potential impact to the quality of ground water as it relates to the EPA's authority pursuant to Section 1424(e) of the Safe Drinking Water Act.

Appendix 6. U.S. Fish & Wildlife Service Consultation Letter, Species List Louisiana Ecological Services Field Office, and NE Consistency Letter Louisiana Endangered Species Act project. This appendix contains

the USFWS consistency letter for the project named 'St. Louis High School Relocation' for specified threatened and endangered species that may occur in your proposed project location pursuant to the Louisiana Endangered Species Act project review and guidance for other federal trust resources determination key (Louisiana DKey). The Consultation letter is dated September 16, 2020. The initial disaster notification letter divides the disaster-related work into categories and distinguishes what would constitute an adverse effect on T&E species. The Species List from USFWS, dated October 13, 2023, identifies any threatened, endangered, and candidate species, as well as designated and proposed critical habit that may occur within the boundary of the proposed project. A total of 4 threatened, endangered, and candidate species were identified. Red-cockaded Woodpecker Picoides *borealis* (Endangered), Whooping Crane Grus *americana* (Experimental Population, Non-Essential), Alligator Snapping Turtle Macrochelys *temminckii* (Proposed Threatened), Monarch Butterfly Danaus *plexippus* (Candidate). No critical habitat was identified in the proposed area.

Appendix 7. Section 106 Review Consultation and Continuing Consultation. The continued consult was received on October 22, 2024. The State Historic Preservation Office (SHPO) concurs with FEMA's determination that the proposed demolition of the referenced buildings constitutes an adverse effect to the NRHP-eligible St. Louis Catholic High School Neighborhood Historic District and the individually NRHP-eligible Landry Memorial Gymnasium. This appendix contains the continued consultation letter regarding no adverse effect to historic properties.

Appendix 8. Louisiana Nonattainment Maintenance Status USEP. This 4-page document was received on September 30, 2023. This appendix contains the Louisiana Nonattainment/Maintenance Status for Each County by Year for All Criteria Pollutants.

Appendix 9. Phase I Environmental Assessment. This appendix contains the Phase I Environmental Site Assessment for the referenced property, prepared by Southland Environmental, dated April 4, 2023. Site assessment was conducted to identify any recognized environmental conditions. No recognized environmental conditions were identified on the subject property. The assessment encompassed a detailed environmental database search of the Louisiana Department of Natural Resources Strategic Online Natural Resources Information System (SONRIS), historical aerials, topographical maps used to determine elevation, followed by a site reconnaissance to inspect the property for environmental concerns. Interviews with landowners and state regulatory agencies were conducted to determine any additional environmental concerns.

Appendix 10. DR-4559-LA and EM-3538-LA Public Notice and Finding of No Significant Impacts. This appendix contains the Public Notice and Finding of No Significant Impacts (FONSI) that is provided in their entirety.

APPENDIX 1. New St. Louis Catholic High School Campus Plans













JOINT

EACH	LAM.	LAMINATE	RM.	ROOM
EACH WAY	LAV.	LAVATORY	R.O.	ROUGH OPENING
EDGE ANGLE	L.F.	LINEAR FEET	R.B.	RUBBER BASE
ELECTIC WATER COOLER	L.L.H.	LONG LEG HORIZONTAL	SCHED.	SCHEDULE
ELECTRIC HAND DRYER	L.L.V.	LONG LEG VERTICAL	SUTLED.	SEALANT
ELECTRICAL	MFR.	MANUFACTURER	SLT.	SEAM
ELECTRICAL CONDUIT	M.B.	MARKER BOARD	SIM.	SECTION
	MAS.	MASONRY	SLUT.	
ELEVATION		MASONRY OPENING		SHORT LEG VERTICAL
EQUAL	M.O.		SIM.	SIMILAR
EQUIPMENT	MATL.	MATERIAL	S.D.	SOAP DISPENSER
EXISTING	MAX.	MAXIMUM	S.C.	SOLID CORE
EXISTING TO REMAIN	MECH.	MECHANICAL	SPECS.	SPECIFICATIONS
EXPANSION JOINT	MTL.	METAL	SQ.	SQUARE
EXPOSED or EXPANSION	MILLWK.	MILLWORK	S.S.	STAINLESS STEEL
EXTERIOR	MIN.	MINIMUM	STD.	STANDARD
FACE OF	MTG.	MOUNTING	STAND.	STANDING
FIBERGLASS	MULT,	MULTIPLE	STL.	STEEL
FINISH FLOOR	NOM.	NOMINAL	STRUCT.	STRUCTURAL
FINISH FLOOR ELEVATION	NFC	NOT FOR CONSTRUCTION	SGFT	STRUCTURAL GLAZED FACING
FINISH(ED)	N.I.C.	NOT IN CONTRACT	22.2	TILE
FIRE DEPARTMENT CONNECTION	N.T.S.	NOT TO SCALE	SSG	STRUCTURAL SILICONE GLAZED
FIRE EXTINGUISHER	NO.	NUMBER	S,A,	SUPPLY AIR
FIRE EXTINGUISHER CABINET	0.C.	ON CENTER	SYN.	SYNTHETIC
FLOOR	OPNG.	OPENING	T.B.	TACKBOARD
FLOOR DRAIN	O.H.	OPPOSITE HAND	Τ.	TALL
FLUORESCENT	O.D.	OUTSIDE DIAMETER	TERR.	TERRAZZO
FOOT or FEET	PTD.	PAINTED	THK.	THICK(NESS)
FOOTING	PNL.	PANEL	TH.	THRESHOLD
FOUNDATION	P.T.D.	PAPER TOWEL DISPENSER	TLT.	TOILET
FREEZER	PART.	PARTITION	T.P.H.	TOILET PAPER HOLDER
GAUGE	PED.	PEDESTRIAN	T.O.M.	TOP OF MASONRY
GENERAL CONTRACTOR	PERP	PERPENDICULAR	T.O.S.	TOP OF STEEL
GLASS	P.LAM.	PLASTIC LAMINATE	TRTD.	TREATED
GRAB BAR	PL.	PLATE	TYP.	TYPICAL
GRADE	+/-	PLUS OR MINUS	U.C.	UNDER COUNTER
GROUND FACE	PLYWD.	PLYWOOD	UND.	UNDERLAYMENT
GYPSUM	PSF	POUNDS PER SQUARE FOOT	U.N.O.	UNLESS NOTED OTHERWISE
GYPSUM WALLBOARD	PSI	POUNDS PER SQUARE INCH	V.T.R.	VENT THROUGH ROOF
HARDWARE	P.S.	PROJECTOR SCREEN	VER.	VERIFY
HEATING, VENTILATING & AIR	Q.T.	QUARRY TILE	V.I.F.	VERIFY IN FIELD
CONDITIONING	RAD.	RADIUS	V.O.J.	VERIFY ON JOBSITE
HEIGHT	R.W.C.	RAIN WATER CONDUCTOR	VERT.	VERTICAL
HIGH	REC.		V.B.	VINYL BASE
HIGH PERFORMANCE		RECESSED	V.C.T.	VINYL COMPOSITION TILE
HOLLOW CORE	RE:	REFERENCE (REFER TO)	W.C.	WATER CLOSET
HOLLOW METAL	REFL.	REFLECTED	W.W.M./F.	WELDED WIRE MESH/ FABRIC
HORIZONTAL	R.F.	REFLECTIVE FACE	W.	WIDE
HOT WATER	REF.	REFRIGERATOR	WDW.	WINDOW
	RCP	REINFORCED CONCRETE PIPE		
INSIDE DIAMETER	REINF.	REINFORCED or REINFORCING	W.G.	WIRE GLASS
INSULATION	REQ'D.	REQUIRED	W/	WITH
INTERIOR	REQ'TS.	REQUIREMENTS	W/O	WITHOUT
INVERT	R.A.	RETURN AIR	WD.	WOOD
JOINT	DD	DOOF DOAIN		

R.D. ROOF DRAIN



FINISH KEY SCHEDULE					FLO	OR FINISH LEGEND
KEY NAME	FLOOR FINISH	BASE FINISH	WALL FINISH	COMMENTS	NOTE: REFER TO FINISH LEG	END & SCHEDULE FOR FURTHER INFORMATION
GALLERY	TERRAZZO	TERRAZZO	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS		1
ITORIUM	CARPET TILE	RUBBER BASE	PTD, GYP, BOARD		TZ-1	TERAZZO
ETERIA	VCT	RUBBER BASE	PTD. GYP. BOARD		1 1 1	
PUS MINISTRY	CARPET TILE	RUBBER BASE	PTD, GYP, BOARD			
PEL	PORCELAIN TILE	PORCELAIN TILE	PTD. GYP. BOARD		CDT 1	
IR/BAND	CARPET TILE	RUBBER BASE	PTD. GYP. BOARD		CPT-1	CARPET TILE
SSROOM	VCT	RUBBER BASE	PTD. GYP. BOARD		E	
SET/STORAGE	VCT	RUBBER BASE	PAINTED			
MMONS	VCT/CARPET TILE	RUBBER BASE	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS	LVT-1	LUXURY VINYL TILE
ICESSIONS	VCT	RUBBER BASE	PAINT			
FERENCE	LVT	RUBBER BASE	PAINTED			
RIDOR	VCT	RUBBER BASE	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS	OT 1	011/07/2015
HER/CORRIDOR	TERRAZZO	TERRAZZO	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS	QT-1	QUARRY TILE
I & AUX. GYM	HARDWOOD	RUBBER BASE	PTD. CMU/PTD. GYP. BD.			
BOOSTER	TERRAZZO	TERRAZZO	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS	T-1	12 X 12 PORECLAIN
CORRIDOR	VCT	RUBBER BASE	PTD CMU			OR CERAMIC TILE
DANCE	LVT?????	RUBBER BASE	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS		
ILEVEL 1	SEALED CONCRETE	RUBBER BASE	PTD CMU		NOT 1	
LEVEL 2	SEALED CONCRETE	RUBBER BASE	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS	VCT-1	VINYL COMPOSITION TILE
ILOBBY	TERRAZZO	TERRAZZO	PTD. CMU/PTD. GYP. BD.			
RESTROOMS	PORCELAIN TILE	PORCELAIN TILE	PTD CMU	15- P4	WD-1	WOOD FLOOR
TOR	SEALED CONCRETE	RUBBER BASE	PAINTED			
HEN	QUARRY TILE	QUARRY TILE	PTD. GYP. BOARD			
ARY	CARPET TILE	CARPET TILE	PTD. GYP. BOARD	PROVIDE CORNER GUARD AT OUTSIDE GYP. CORNERS	WD 1	
H/ELEC/DATA	SEALED CONCRETE	RUBBER BASE	PAINTED		WD-1	ATHELTIC WOOD FLOOR
CE	LVT	RUBBER BASE	PAINTED			
TROOM (GANG)	PORCELAIN TILE	RUBBER BASE	PORCELAIN TILE		1.27.2	
TROOM (SINGLE)	PORCELAIN TILE	RUBBER BASE	PORCELAIN TILE		AR-1	ATHLETIC RUBBER FLOOR
INCE LAB	VCT	RUBBER BASE	PTD. GYP. BOARD			
R	VCT/CONCRETE TREADS & LANDINGS	RUBBER BASE	PAINTED			
H	VCT	RUBBER BASE	PAINTED	P.1	SC 1	STALED CONCRETE
GHT ROOM	ATHLETIC RUBBER FLOORING	RUBBER BASE	PTD CMU		SC-1	SEALED CONCRETE
RKROOM	VCT	RUBBER BASE	PAINTED			
					EP-1	EPOXY





9.11 WALL BASE; RE: FINISH SCHEDULE 9.14 CEILING; RE: REFLECTED CEILING PLAN 9.16 STUCCO CASING BEAD, TYPICAL AT PERIMETER OF DOORS, WINDOWS, & 9.17 BRACE TO STRUCTURE @ 48" O.C. MAX







A0.06









STOREFRONT FRAMING

- ALUM. ENTRANCE





- 1/4" TEMPERED GLAZING

- STOREFRONT FRAMING -june 22 DETAIL 3" = 1'-0" 6" STOREFRONT HORIZONTAL - CENTER



- INSULATED GLAZING - STOREFRONT FRAMING - ALUM. ENTRANCE - 1/4" TEMPERED GLAZING































1" = 1'-O"







N N DIO ST. CEH PROJECT #: 2106 RHH PROJECT #: 42-01-21 4/22/2022 DATE: REVIEW FOR: © 2022 RHH ARCHITECTS, APAC REVISION DATE QUAD SITE PLAN & ROOF PLAN A1.20

NORTH



















QUAD - TOWER SOUTH ELEVATION 5 3/32" = 1'-0"

MATERIALS LEGEND:

4" NOMINAL BRICK VENEER

3/4" PORTLAND CEMENT PLASTER or CAST STONE

ARCHITECTURAL COMPOSITE SHINGLE ROOFING



Æ









BUILDING A- LEVEL 2 LIFE SAFETY PLAN



 \bigoplus NORTH

CODE SUMMARY	S
- 2015 DDE (IBC] - 2015 ACT GUIDELINES (ADAAG] - 2010 N	ARCHITECTS
I: RE: CIVIL RE: CIVIL	ARO
ATION OF THE STRUCTURE: TIONAL (CHAPTER 14] SILY (CHAPTER 12] SORY BUSINESS TION GROUP E (SECTION 305] SILY GROUP A-3 (SECTION 303] SORY BUSINESS GROUP B (SECTION 304]	CHAMPEAUX EVANS HOTARD A R C H I T E C T S
D FIRE-RESISTANCE RATINGS ABLE A.8.2.1.2, COMMENTARY 8.1] EXCEPT AT ROOF STRUCTURE 20' AFF BLE 503]	
AREA GHTS AND FLOOR AREAS FOR TYPES OF CUPANCY CLASSIFICATIONS: 5.2 FOR TYPE II-B, SPRINKLERED : 2 STORIES, 58,000 SF PER STORY $-3:$ 2 STORIES, 38,000 SF PER STORY $-3:$ 2 STORIES, 28,000 F PER STORY $-3:$ 2 STORIES, 28,000 F PER STORY $-3:$ 2 STORIES, 28,000 F PER STORY $-3:$ 2 STORI	CONSULTANTS: CONSULTANTS: DUHON PLEASANT ENCINEERS CIVIL/STRUCTURAL ADG ENCINEERING MEP MEP LANDSCAPE FOOD SERVICE TBA
AND FIRE ALARM REQUIREMENTS SPRINKLER FION – YES [14.3.5.1] LY – YES [12.3.5.1] IRE AREA EXCEEDS 12,000 SF [903.2.3] FIRE AREA EXCEEDS 12,000 SF OR O.L. EXCEEDS .3] JIREMENT: TONAL – YES [SEC. 14.3.4.1]	
[SEC. 12.3.4.1] E: YES [SEC. 907.2.3] A3: YES, AS REQUIRED BY GROUP E OCC. [SEC.] DRS	
IBC [TABLE 1004.1.2]: IBC [TABLE 1004.1.2]: SEATS) 15 NET SF/OCCUPANT 50 NET SF/OCCUPANT 100 NET SF/OCCUPANT 18 LINEAR INCHES/OCCUPANT 18 LINEAR INCHES/OCCUPANT 100 NET SF/OCCUPANT 100 NET SF/OCCUPANT 15 NET SF/OCCUPANT 15 NET SF/OCCUPANT 19): 50 NET SF/OCCUPANT 300 NET SF/OCCUPANT	
5: 3.1]: STAIRWAYS – O.L. X 0.3"/OCCUPANT (44" LEVEL – O.L. X 0.2"/OCCUPANT (44" MIN. EACH) AYS – O.L. X 0.3"/OCCUPANT (44" MIN. EACH); (0.2"/OCCUPANT (44" MIN. EACH) DF EXITS:	Ъ
2]: <500 OCCUPANTS: 2 EXITS -1000 OCCUPANTS: 3 EXITS 000 OCCUPANTS: 4 EXITS <500 OCCUPANTS: 2 EXITS	SCHOO
7.4] 26.2]	- ES -
5.2]	CHARLES C HIGH S
GS: APTERS 11 THROUGH 43, UNENCLOSED EALED WITHIN THE BUILDING ITED AS FOLLOWS: CONNECT NOT MORE THAN TWO DOR PIERCED ONLY). BE SEPARATED FROM UNPROTECTED GOTHER FLOORS BY A BARRIER	for LAKE THOLI Charles, LA
E SEPARATED FROM CORRIDORS. QUIREMENTS FOR NFPA 101: DRRIDOR OR PASSAGEWAY SHALL NOT WIDTH. [14.2.3.2]. KITS SHALL BE PROVIDED ON EACH IBLE FROM EVERY PART OF EVERY STORY . NOT EXCEED 50 FT IF SPRINKLED	of OF OF OF OF OF OF
SHALL NOT EXCEED 100' IF SPRINKLED 1,000 S.F. OR WITH AN OCCUPANT ALL HAVE A MIN. OF TWO EXIST ACCESS ACCESS TO SEPARATE EXITS, AND SHALL O A COMMON CORRIDOR, PROVIDED S TO SEPARATE EXITS LOCATED IN .5.4] HALL NOT EXCEED 200 FT. IF SPRINKLED.	Construction Doc DIOCESE ST. LOUIS 4220 Corbina Roa
E REQUIRED. [7.5.4.7] D: YES [7.2.12]	CEH PROJECT #: 2106 RHH PROJECT #: 42-01-21
REQUIREMENTS FOR IBC: 1007.2.1] D: NO [1007.3.3] EL SHALL NOT EXCEED 75' FOR GROUP E A [1006.2.1]. EXITS SHALL BE PROVIDED ON EACH ACE WITH MORE THAN 49 OCCUPANTS	DATE: 4/22/2022 FOR: REVIEW © 2022 RHH ARCHITECTS, APAC
S SHALL NOT EXCEED 250 FT [TABLE 1017.2]. WIDTH SHALL NOT BE LESS THAN 72 IN. LOAD OF 100 OR MORE. HALL NOT EXCEED 50 FT [1020.4.2].	REVISION DATE
E SAFETY LEGEND	
50 ALONG PATH OF EGRESS	
OCCUPANT LOAD	
NUMBER OF OCCUPANTS EXITING REQUIRED OPENING RATING (min.)	
- EXIT SIGN (DIRECTION & ILLUMINATION SIDE) 	
IRE EXTINGUISHER: SURFACE MOUNTED CABINET	
- FIRE EXTINGUISHER: FULLY RECESSED CABINET RE EXTINGUISHER: SURFACE MOUNTED BRACKET	
EXTINGUISHER: UNDER COUNTER WITH BRACKET	
ROL TIED TO SHARED CARD READER, RE: ELEC.	
ACCESS CONTROL PUSH BUTTON, RE: ELEC.	BUILDING A LIFE
SMOKE PARTITION	SAFETY PLANS & CODE SUMMARY
STORAGE AREAS REQUIRE SMOKE PARTITION TO CEILING WITH SELF CLOSING DOORS	A2.00
RATED FLOOR ASSEMBLY AS NOTED	



1/16" = 1'-0"

1/16" = 1'-0"





1/8" = 1'-0"



KEYNOTES	ř.
10.9	4' MARKER STRIP
12.3	MAIL PASS

FLOOR PLAN LEGEND RE: SHEET A3.01 RE: SHEETS A7.01-A7.02 INTERIOR ELEVATION EXTERIOR ELEVATION TBA CAPE TBA MEP BUILDING SECTION PLAN DETAIL TAG U.N.O., WALLS ARE CENTERED ON COLUMN CENTER LINE DISTANCE FROM WALL FACE TO EDGE OF DOOR RECESSED FIRE EXTINGUISHER CABINET AND EXTINGUISHER SHEET METAL DOWNSPOUT/BOOT TIED INTO PAINTED DOWNSPOUT BOOT U SS C U T R BOARD W/ 4' x 1' TACK C THROUGH DROP BOX 0 S 0 -O S CEH PROJECT #: 2106 RHH PROJECT #: 42-01-21 4/22/2022 DATE: REVIEW FOR: © 2022 RHH ARCHITECTS, APAC REVISION DATE **BUILDING A** LEVEL 1 PLAN -NORTH A2.11



1/8" = 1'-0"







BUILDING A - LEVEL 2 FLOOR PLAN - NORTH

1/8" = 1'-0"



10.9 4' MARKER BOARD W/ 4' x 1' TACK STRIP







BUILDING A - LEVEL 2 FLOOR PLAN - SOUTH

1/8" = 1'-0"



KEYNOTES

4' MARKER BOARD W/ 4' x 1' TACK STRIP 10.9







2 BUILDING A - ROOF PLAN 1/16" = 1'-0"



APPENDIX 2. DOLC New SLCHS Property Geo Tech Report



Geotechnical Engineering Report

New St. Louis Catholic High School Campus Lake Charles, Louisiana

Geotechnical

September 1, 2023 Terracon Project No. EU235053

Prepared for: Champeaux Evans Hotard APAC Lake Charles, LA

> Prepared by: Terracon Consultants, Inc. Baton Rouge, Louisiana

Materials

Facilities

September 1, 2023



Champeaux Evans Hotard APAC 702 Dr. Michael Debakey Drive Lake Charles, LA 70601

- Attn: Mr. Stephen Hotard, AIA P: (337) 439-8871 E: stephen@champeaux.biz
- Re: Geotechnical Engineering Report New St. Louis Catholic High School Campus Corbina Road and James Court Lake Charles, Louisiana Terracon Project No. EU235053

Dear Mr. Hotard:

We have completed the Geotechnical Engineering services for the above referenced project. This study was performed in general accordance with Terracon Proposal No. PEU235053_Rev. 1 dated July 28, 2023. This report presents the findings of the subsurface exploration and provides geotechnical recommendations concerning earthwork and the design and construction of foundations, floor slabs, and pavements for the proposed project.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report or if we may be of further service, please contact us.

Sincerely, Terracon Consultants, Inc.

Trent A. Whitley, P.E. Senior Engineer

9/1/2023

Lynne E. Roussel, P.E. Principal | Office Manager

Terracon Consultants, Inc. 2822 O'Neal Lane Building B Baton Rouge, Louisiana 70816 P [225] 344 6052 F [225] 344 6346 terracon.com

REPORT TOPICS

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PROJECT DESCRIPTION	2
GEOTECHNICAL CHARACTERIZATION	4
GEOTECHNICAL OVERVIEW	5
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SHALLOW FOUNDATIONS	
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Note: This report was originally delivered in a web-based format. **Orange Bold** text in the report indicates a referenced section heading. The PDF version also includes hyperlinks which direct the reader to that section and clicking on the *GeoReport* logo will bring you back to this page. For more interactive features, please view your project online at <u>client.terracon.com</u>.

ATTACHMENTS

EXPLORATION AND TESTING PROCEDURES SITE LOCATION AND EXPLORATION PLANS EXPLORATION RESULTS SUPPORTING INFORMATION

Note: Refer to each individual Attachment for a listing of contents.

Geotechnical Engineering Report New St. Louis Catholic High School Campus Corbina Road and James Court Lake Charles, Louisiana Terracon Project No. EU235053 September 1, 2023

INTRODUCTION

This report presents the results of our subsurface exploration and geotechnical engineering services performed for the proposed new St. Louis Catholic High School campus to be located east of the intersection of Corbina Road and James Court in Lake Charles, Louisiana. The purpose of these services is to provide information and geotechnical engineering recommendations relative to:

- Subsurface soil conditions
- Groundwater conditions
- Site preparation and earthwork
- Excavation considerations
- Lateral earth pressure

- Foundation design and construction
- Floor slab design and construction
- Seismic site classification per IBC
- Pavement design and construction

The geotechnical exploration Scope of Services for this project included the advancement of 44 test borings to depths ranging from approximately 6 to 50 feet below existing site grades.

Maps showing the site and boring locations are shown in the **Site Location** and **Exploration Plan** sections, respectively. The results of the laboratory testing performed on soil samples obtained from the site during the field exploration are included on the boring logs and/or as separate graphs in the **Exploration Results** section.

SITE CONDITIONS

The following description of site conditions is derived from our site visit in association with the field exploration and our review of publicly available geologic and topographic maps.

Item	Description
Parcel Information See Site Location.	The project is located east of the intersection of Corbina Road and James Court in Lake Charles, Louisiana. Latitude/Longitude (approximate): 30.1817, -93.1586 (See Exhibit D)
Existing Improvements	No existing improvements appear to be present at the project site.

Geotechnical Engineering Report

New St. Louis Catholic High School Campus
Lake Charles, Louisiana September 1, 2023
Terracon Project No. EU235053



Item	Description			
Current Ground Cover	The field associated with the project site was lightly vegetated and very dry at the time of our exploration.			
Existing Topography	The site is relatively flat.			
	The property is located within an area of Beaumont Alloformation (Ppbe) of Prairie Terrace deposits of Pleistocene Age. Beaumont Alloformation consists of plain deposits of late to middle Pleistocene streams: the oldest alloformation and topographically highest surface or the Prairie Allogroup units of southwestern Louisiana. It exhibits the relict channels of the Red and Calcasieu rivers and includes deposits of the Ingleside barrier trend within the Lake Charles quadrangle. The Pleistocene Age deposits typically consist of medium stiff to very stiff tan and light gray silty clays and clays with silt and sand layering. The soils within the Prairie Terrace deposits typically provide good foundation support for relatively light to moderately loaded structures, are overconsolidated, and normally only marginally compressible. In some areas that are very dry and desiccated, the potential for expansive properties exists, but these conditions are not typical of the Prairie Terrace deposits.			
Geology	Pper Pper Pper			

PROJECT DESCRIPTION

Our initial understanding of the project was provided in our proposal and was discussed during project planning. A period of collaboration has transpired since the project was initiated, and our final understanding of the project conditions is as follows:

Geotechnical Engineering Report

New St. Louis Catholic High School Campus
Lake Charles, Louisiana September 1, 2023
Terracon Project No. EU235053



ltem	Description	
Information Provided	An email request for proposal was provided by Mr. Hotard, representing CEH, on July 9, 2023. The request included a Google Earth image of the site and conceptual plan drawings of the layout and elevations of the planned development.	
Project Description	The project includes the construction of a new campus for St. Louis Catholic High School, including new school buildings, a gymnasium, a courtyard, a central plant, a pavilion, six sports fields/courts (including a football field, baseball field, softball field, soccer field, practice field, and tennis courts), and associated parking and drives.	
Proposed Structures	Structures associated with the project include a two-story main classroom building, a two-story gymnasium, and 6 one-story buildings (including a science building, arts building, auditorium, chapel, field house, and baseball building).	
Building Construction	Not provided; we anticipate one-story buildings will be constructed using shallow foundations to support column loads in conjunction with a floor slab foundation system, and two-story buildings may be constructed with drilled shaft foundations to support column loads in conjunction with a floor slab foundation system.	
Finished Floor Elevation	Finished floor elevation for the structures were not provided. We have assumed finished floor elevation will not be more than 3 feet above existing grade.	
Maximum Loads	Anticipated structural loads were not provided. In the absence information provided by the design team, we will use the following loads estimating settlement based on our experience with similar projects. One-Story Building Columns: 50 kips Two-Story Building Columns: 150 kips Column Uplift Load: 30 kips Walls: 3 kips per linear foot (klf) Slabs: 150 pounds per square foot (psf)	
Pavements	 Paved driveway and parking will be constructed on the parcel. We assume rigid (concrete) pavement sections should be considered for all parking areas except the limestone parking area south of the proposed tennis courts. Please confirm this assumption. Anticipated traffic is as follows: Autos/light trucks: 500 vehicles per day Light delivery and trash collection vehicles: 10 vehicles per week Buses: 30 vehicles per day The pavement design period is 20 years. 	

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GEOTECHNICAL CHARACTERIZATION

We have developed a general characterization of the subsurface conditions based upon our review of the subsurface exploration, laboratory data, geologic setting and our understanding of the project. This characterization, termed GeoModel, forms the basis of our geotechnical calculations and evaluation of site preparation and foundation options. Conditions encountered at each exploration point are indicated on the individual logs. The individual logs can be found in the **Exploration Results** section and the GeoModel can be found in the **Figures** section of this report.

As part of our analyses, we identified the following model layers within the subsurface profile. For a more detailed view of the model layer depths at each boring location, refer to the GeoModel.

Model Layer	Layer Name	General Description
01	Silty Clay and Lean Clay	Brown, reddish brown, gray, and tan, very stiff to hard, silty clay and lean clay
02	Upper Fat Clay	Gray, reddish brown, and tan, stiff to hard, fat clay
03	Upper Lean Clay and Sandy Silty Clay	Reddish brown, gray, and tan, medium stiff to very stiff, sandy lean clay, sandy silty clay, and lean clay
04	Upper Clayey Sand	Reddish brown and gray, loose to medium dense, clayey sand
05	Lower Fat Clay	Brown and dark gray, stiff to very stiff, fat clay; B-02 contains lean clay from 32 feet to 40 feet
06	Lower Clayey Sand	Dark gray and light gray, dense, clayey sand
07	Lower Lean Clay	Light gray and tan, stiff to hard, lean clay and sandy lean clay

Groundwater was initially encountered in borings B-01 through B-18 (excluding B-17) during drilling at a depth of between approximately 13 and 16 feet below the existing ground surface. After 15 minutes, the water was measured at about 7 to 9 feet below existing grade. No groundwater was encountered in borings B-17 or in borings B-19 through B-44. This does not necessarily mean the borings terminated above groundwater, or that the water levels summarized above are stable groundwater levels. Due to the low permeability of the soils encountered in the borings, a relatively long period of time may be necessary for the groundwater level to develop and stabilize in a borehole in these materials. Long term observations in piezometers or observation wells sealed from the influence of surface water are often required to define the field or in-situ groundwater level in materials of this type.

Groundwater fluctuations occur due to seasonal variations in the amount of rainfall, runoff, site modification, and other factors not evident at the time the borings were performed. Therefore, groundwater levels during construction or at other times in the life of the structure may be higher or lower than the levels indicated on the boring logs. Perched water conditions, where groundwater is trapped above clays in an otherwise unsaturated zone are also common in this



region. The possibility of groundwater level fluctuations should be considered when developing the design and construction plans for the project.

GEOTECHNICAL OVERVIEW

In general, the near surface soils encountered at the project site below approximately 3 inches of topsoil consist of relatively dry silt and stiff to hard silty clay to a depth of about 1 foot below existing grade underlain by relatively dry, very stiff to hard lean clay to a depth of 2 feet below existing grade. Beneath the lean clay, the soils encountered generally included stiff to hard, slickensided fat clay to a depth of 8 feet below existing grade. The surface soils appeared relatively stable at the time of the exploration. However, these silty soils are expected to become unstable with typical earthwork and construction traffic, especially after precipitation events. To reduce potential for surface instability, effective drainage should be completed early in the construction sequence and maintained during and after construction. The construction phase drainage should be considered in the development of the project overall grading and drainage plan. The possible poor drainage conditions can lead to instability in the areas around the site and hamper construction progress. A temporary dewatering system of sumps and pumps could be necessary to remove ponding water where positive drainage is not feasible.

If possible, the grading should be performed during the warmer and drier time of the year. If grading is performed during the winter months or at times with persistent rain, an increased risk for possible undercutting and replacement of unstable subgrade or the need for other mitigation measures will persist. It should be budgeted to remove the upper 2 feet of silt, silty clay and dry fat clays.

The near surface soils at the site, to the depth of the approximate seasonal moisture change zone of about 8 feet, consists of low- to moderate-plasticity silt, silty clay, and lean clay to a depth of 2 feet underlain by high plasticity fat clay. In general, lean clays are considered to exhibit low to moderate potential while fat clays are considered to exhibit a high potential for shrink-swell movements. The Potential Vertical Rise (PVR) approach is a common method used to predict vertical movements in plastic clays. The methodology is based on a correlation between the plasticity index (PI) of the soil, moisture content, and the percent volumetric change. Considering the average conditions at the project site, a PVR at this site is predicted to be approximately 1.5 to 2 inches. The moisture conditions in the upper 8 feet were considered to be relatively dry with water content typically within 5 percent of the material plastic limits, especially within the fat clay encountered at about 2 feet below existing grade. Lab swell tests on two relatively dry samples of the fat clay indicated moderate shrink/swell potential. Reducing PVR can be accomplished by creating a buffer of low volume change low permeability material between the bottom of the slab or athletic field surfaces and the high-volume change fat clays. Based on our experience at nearby project sites, we recommend construction of a minimum 3 feet buffer of low volume change materials between the bottom of the structure or field surface and the underlying fat clays. This



buffer is usually created through a combination of undercut/removal and raising site grade. The buffer should extend a minimum of 5 feet from the perimeter of the structure or field footprint. The low volume change fill material meeting the soil property and compaction requirements for imported lean clay structural fill should be as specified in the Earthwork section. Details of moisture conditioning are included in the Earthwork section. A sand fill is not recommended due to the relative high permeability of this material which could allow surface water intrusion causing moisture change and related shrink/swell of the underlying fat clays.

Additional site preparation recommendations, including proof-rolling and fill placement, are provided in the **Earthwork** section.

The **Shallow Foundations** section addresses support of lightly to moderately loaded structures bearing on structural fill. The **Floor Slabs** section addresses slab-on-grade support of the buildings if site preparation recommendations in this report are followed.

Heavily loaded structures or structures potentially sensitive to shallow foundation settlement may be supported on deep foundations. The **Deep Foundations** section addresses support of the structures on drilled shafts.

Recommendations were requested for rigid pavements, flexible pavements, and aggregate surfacing. The **Pavements** section addresses the design of pavement systems.

The General Comments section provides an understanding of the report limitations.

EARTHWORK

Earthwork is anticipated to include grubbing, proof-rolling, excavations and fill placement. The following sections provide recommendations for use in the preparation of specifications for the work. Recommendations include critical quality criteria, as necessary, to render the site in the state considered in our geotechnical engineering evaluation for foundations, floor slabs, pavements, and athletic field surfaces.

Site Preparation

We anticipate construction will be initiated by stripping vegetation, desiccated silty soils, and loose, soft or otherwise unsuitable material. Complete stripping of the topsoil or root mat should be performed in the proposed building, pavement, and athletic field areas. Stripped materials consisting of vegetation and organic materials should be wasted off site or used to vegetate landscaped areas. Topsoil and underlying silty soil measurements were made at the boring locations; however, stripping depths at or between our boring locations and across the site could vary considerably. As such we recommend actual stripping depths be evaluated by a representative of Terracon during construction to aid in preventing removal of excess material.



For estimation purposes, we anticipate approximately 24 inches of soil removal should be anticipated for site preparation activities. Former utility lines and utility backfill, if present, should be removed from beneath the structures, and the resulting excavations should be properly backfilled as outlined herein. If roots are encountered, the entire root ball should be excavated such that the remaining roots measure 1 inch in diameter or less.

The exposed subgrade should be proof-rolled with heavy rubber tire construction equipment such as a loaded scraper or partially loaded tandem axle dump truck. The vehicle should weigh between 15 and 20 Tons (total vehicle weight). The proof-rolling should be performed under the direction of the Geotechnical Engineer. Proof-rolling should be performed after a suitable period of dry weather to avoid degrading an otherwise acceptable subgrade and to reduce the amount of undercutting/remedial work required. Areas excessively deflecting under the proof-roll should be delineated and subsequently addressed by the Geotechnical Engineer. The Geotechnical Engineer may require isolated areas to be undercut and replaced with structural fill and compacted. Widespread instability may require chemical treatment with lime or cement as specified by the Geotechnical Engineer at the time of construction. Excessively wet or dry material should either be removed or moisture conditioned and recompacted.

If the soils are deemed competent based on proof roll activities, the dry fat clay soil should be moisture conditioned. The exposed subgrade should be scarified, wetted to 2 to 3 percent above the optimum moisture, and compacted to a minimum of 95 percent of standard Proctor. The remaining fill placement can then be placed.

In addition to the above moisture conditioning, a minimum 3 feet buffer of low volume change materials should be placed between the bottom of the structure or field surface and the underlying fat clays to help mitigate potential shrink and swell.

Fill Material Types

Fill required to achieve design grade should be classified as structural fill and general fill. Structural fill is material used below, or within 10 feet of structures, pavements, constructed slopes, and other structural areas. General fill is material used to achieve grade outside of these areas, like landscaped areas. Earthen materials used for structural and general fill should meet the following material property requirements:

Soil Type ¹	USCS Classification	Acceptable Parameters (for Structural Fill)
Imported Lean Clay ²	CL	Liquid Limit less than 45, Plasticity index greater than 10 and less than 25.
Imported Sand	SP, SP-SM	Less than 10% Passing No. 200 sieve
Aggregate Base	GP	LADOTD 610 Crushed Limestone or similarly graded crushed recycled concrete.

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Soil Type ¹ USCS Classification		Acceptable Parameters (for Structural Fill)	
On-Site Soils	CL	The on-site lean clay soils appear suitable for use as fill; however, if they do not meet the low plasticity criteria, they should not be utilized within 3 feet of finished grade beneath building areas.	
On-Site Soils	ML	The silt materials are typically not considered ideal for use as structural fill due to difficult compaction characteristics and stability issues at higher moistures. Low plasticity silt may be used for establishing the subbase for parking/drives if cement treated (10 percent by volume).	
On-Site Soils ³	CH LL>50	The on-site soils from approximately 2 feet to 6 or 8 feet below existing grade consist of fat clay. This material is typically not recommended for use as structural fill without lime treatment due to difficult compaction characteristics, stability issues at higher moistures, and shrink/swell potential. It can be used as backfill in the landscape areas without lime treatment.	

1. Structural and general fill should consist of approved materials free of organic matter and debris. A sample of each material type should be submitted to the Geotechnical Engineer for evaluation prior to use on this site.

- 2. Delineation of fat clays and lean clays should be performed in the field by a qualified geotechnical engineer or their representative, and could require additional laboratory testing.
- 3. CH soils should not be used within structural fill areas.

Fill Compaction Requirements

Structural and general fill should meet the following compaction requirements.

ltem	Structural Fill	General Fill
Maximum Lift Thickness	9 inches or less in loose thickness when heavy, self-propelled compaction equipment is used.4 to 6 inches in loose thickness when hand-guided equipment (i.e. jumping jack or plate compactor) is used.	Same as Structural fill.

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ltem	Structural Fill	General Fill
Minimum Compaction Requirements ^{1, 2, 3}	 95% of standard Proctor (ASTM D698) maximum dry density for soil structural fill below foundations, floor slabs, pavement subgrade, and other structural areas. 95% of modified Proctor (ASTM D1557) maximum dry density for aggregate base beneath pavement or aggregate surfacing. 	92% of max.
Water Content Range ¹	Low plasticity cohesive: -2% to +3% of optimum Granular: -3% to +3% of optimum Aggregate Base: -2% to +2% of optimum	As required to achieve min. compaction requirements.

 Maximum density and optimum water content as determined by the standard Proctor test (ASTM D 698). The moisture content and compaction should be measured for each lift of engineered fill during placement. Should the results of the in-place density tests indicate the specified moisture or compaction limits have not been met, the area represented by the test should be reworked and retested as required until the specified moisture and compaction requirements are achieved.

2. For moisture levels of granular material, it is also appropriate to be conditioned at workable levels to allow for satisfactory compaction to be achieved without the cohesionless fill material pumping when proof-rolled.

Based on the results of borings B-16, B-17, and B-18 completed within the proposed detention pond areas, the surficial silt and silty clay (CL-ML and ML) and underlying fat clay (CH) encountered within the borings to a depth of 2 feet to 4 feet below existing grade appear to be generally not suitable for use as structural fill materials onsite. The lean clay (CL) soils encountered appear to be suitable and may be utilized as structural fill if they meet the requirements for structural fill stated herein.

Utility Trench Backfill

Utility trenches are a common source of water infiltration and migration. Utility trenches penetrating beneath the building should be effectively sealed to restrict water intrusion and flow through the trenches, which could migrate below the building. The trench should provide an effective trench plug that extends at least 5 feet from the face of the building exterior. The plug material should consist of cementitious flowable fill or low permeability clay. The trench plug material should be placed to surround the utility line. If used, the clay trench plug material should be placed to comply with the water content and compaction recommendations for structural fill stated previously in this report.

Grading and Drainage

All grades must provide effective drainage away from the building during and after construction and should be maintained throughout the life of the structure. Water retained next to the building can result in soil movements greater than those discussed in this report. Greater movements can result in unacceptable differential floor slab and/or foundation movements, cracked slabs and



walls, and roof leaks. The roof should have gutters/drains with downspouts that discharge onto splash blocks at a distance of at least 10 feet from the building.

At project sites with minimal grade change and with development and roads surrounding the construction area, it can be difficult to maintain positive drainage throughout the construction phase. The construction phase drainage should be considered in the development of the project overall grading and drainage plan. The possible poor drainage conditions can lead to instability in the areas around the buildings and hamper construction progress. The site grading and general contractor should consider their means and methods to maintain drainage during the construction phase.

Exposed ground should be sloped and maintained at a minimum 5 percent away from the building for at least 10 feet beyond the perimeter of the buildings. Locally, flatter grades may be necessary to transition ADA access requirements for flatwork. A minimum 12-inch thick layer of cohesive backfill should be placed against and 5 feet laterally from the exterior of foundation walls in unpaved/landscaped areas to reduce infiltration of surface water to underlying foundation support soils. After building construction and landscaping, final grades should be verified to document effective drainage has been achieved. Grades around the structures should also be periodically inspected and adjusted as necessary as part of the structure's maintenance program. Where paving or flatwork abuts the structures, a maintenance program should be established to effectively seal and maintain joints and prevent surface water infiltration.

Trees or other vegetation whose root systems can remove excessive moisture from the subgrade and foundation soils should not be planted next to the structure. Trees and shrubbery should be kept away from the exterior edges of the foundation element a distance at least equal to 1.5 times their expected mature height.

Earthwork Construction Considerations

Shallow excavations for the proposed structures and athletic field surfaces are anticipated to be accomplished with conventional construction equipment. Upon completion of filling and grading, care should be taken to maintain the subgrade water content prior to construction of floor slabs. Construction traffic over the completed subgrades should be avoided to the extent practical. The site should also be graded to prevent ponding of surface water on the prepared subgrades or in excavations. Water collecting over, or adjacent to, construction areas should be removed. If the subgrade desiccates, saturates, or is disturbed, the affected material should be removed, or the materials should be scarified, moisture conditioned, and recompacted, prior to floor slab construction.

Although the groundwater table was relatively low at the time of field exploration, the groundwater table could rise and affect excavations, especially for over-excavations and replacement of lower strength soils, where applicable. A temporary dewatering system consisting of sumps with pumps could be necessary to achieve some depths of excavation.


As a minimum, excavations should be performed in accordance with OSHA 29 CFR, Part 1926, Subpart P, "Excavations" and its appendices, and in accordance with any applicable local, and/or state regulations.

Construction site safety is the sole responsibility of the contractor who controls the means, methods, and sequencing of construction operations. Under no circumstances shall the information provided herein be interpreted to mean Terracon is assuming responsibility for construction site safety, shoring, dewatering, or any of the contractor's activities; such responsibility shall neither be implied nor inferred.

Construction Observation and Testing

The earthwork efforts should be monitored under the direction of the Geotechnical Engineer. Monitoring should include documentation of adequate removal of vegetation and topsoil, proofrolling and mitigation of areas delineated by the proof-roll to require mitigation.

Each lift of compacted fill should be tested, evaluated, and reworked as necessary until approved by the Geotechnical Engineer prior to placement of additional lifts. Each lift of fill should be tested for density and water content at a frequency of at least one test for every 2,500 square feet of compacted fill in the building areas and 5,000 square feet in pavement and field surfacing areas. One density and water content test should be performed for every 50 linear feet of compacted utility trench backfill.

In areas of foundation excavations, the bearing subgrade should be evaluated under the direction of the Geotechnical Engineer. If unanticipated conditions are encountered, the Geotechnical Engineer should prescribe mitigation options.

In addition to the documentation of the essential parameters necessary for construction, the continuation of the Geotechnical Engineer into the construction phase of the project provides the continuity to maintain the Geotechnical Engineer's evaluation of subsurface conditions, including assessing variations and associated design changes.

SHALLOW FOUNDATIONS

If the site has been prepared in accordance with the requirements noted in **Earthwork**, the following design parameters are applicable for shallow foundations.

Design Parameters – Compressive Loads

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Item	Description
Maximum Net Allowable Bearing Pressure ^{1, 2}	1,800 psf (Isolated columns and continuous footings).
Required Bearing Stratum ³	Structural fill.
Minimum Foundation Dimensions	Columns:24 inchesContinuous:16 inches
Ultimate Passive Resistance ⁴ (equivalent fluid pressures)	250 pcf (cohesive backfill) 350 pcf (granular backfill)
Ultimate Adhesion/Coefficient of Sliding Friction ⁵	400 psf (existing clay or cohesive backfill) 0.39 (granular material)
Minimum Embedment Below Finished Grade ⁶	Exterior footings:18 inchesInterior footings:12 inches
Estimated Total Settlement from Structural Loads ²	Less than about 1 inch.
Estimated Differential Settlement ²	About 1/2 of total settlement.

- The maximum net allowable bearing pressure is the pressure in excess of the minimum surrounding overburden pressure at the footing base elevation. An appropriate factor of safety has been applied. The allowable bearing pressure may be increased by one-third when considering the alternative load combinations of Section 1605.3.2 of the 2015 International Building Code, however, it should not be increased when loads are determined by the basic allowable stress design load combinations of Section 1605.3.1.
- 2. Values provided are for maximum loads noted in **Project Description**. Settlement is for structural loads and up to 3 feet of engineering fill. Differential settlements are as measured over a span of 40 feet.
- 3. Unsuitable or soft/unstable soils should be over-excavated and replaced per the recommendations in Earthwork.
- 4. Use of passive earth pressures require the sides of the excavation for the spread footing foundation to be nearly vertical and the concrete placed neat against these vertical faces or that the footing forms be removed and compacted structural fill be placed against the vertical footing face. Apply a factor of safety of at least 1.5 to this value when designing for lateral force resistance.
- 5. Can be used to compute sliding resistance where foundations are placed on suitable soil/materials. Should be neglected for foundations subject to net uplift conditions.
- 6. Embedment necessary to minimize the effects of seasonal water content variations. For sloping ground, maintain depth below the lowest adjacent exterior grade within 5 horizontal feet of the structure.

Design Parameters - Uplift Loads

Uplift resistance of spread footings can be developed from the effective weight of the footing and the overlying soils. As illustrated on the subsequent figure, the effective weight of the soil prism defined by diagonal planes extending up from the top of the perimeter of the foundation to the



ground surface at an angle, θ , of 20 degrees from the vertical can be included in uplift resistance. The maximum allowable uplift capacity should be taken as a sum of the effective weight of soil plus the dead weight of the foundation, divided by an appropriate factor of safety. A maximum total unit weight of 115 pcf should be used for the backfill. This unit weight should be reduced to 53 pcf for portions of the backfill or natural soils below the groundwater elevation.



Foundation Construction Considerations

As noted in **Earthwork**, the footing excavations should be evaluated under the direction of the Geotechnical Engineer. The base of all foundation excavations should be free of water and loose soil, prior to placing concrete. Concrete should be placed soon after excavating to reduce bearing soil disturbance. Care should be taken to prevent wetting or drying of the bearing materials during construction. Excessively wet or dry material or any loose/disturbed material in the bottom of the footing excavations should be removed/reconditioned before foundation concrete is placed.

If unsuitable bearing soils are encountered at the base of the planned footing excavation, the excavation should be extended deeper to suitable soils, and the footings could bear directly on these soils at the lower level or on lean concrete backfill placed in the excavations. This is illustrated on the sketch below.

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Over-excavation for structural fill placement below footings should be conducted as shown below. The over-excavation should be backfilled up to the footing base elevation, with structural soil fill or crushed stone wrapped in non-woven geotextile fabric, placed as recommended in the **Earthwork** section.



The following precautions are essential to the satisfactory performance of shallow foundations:

- Provide positive drainage away from the foundations, both during and after construction.
- Avoid excavations during inclement weather and place concrete within the excavations within 24 hours after completion of the excavations.
- Verify that the excavations are completely within the required bearing stratum or structural fill and remove and replace any unacceptable soils as discussed herein.
- Maintain adequate moisture levels in exposed excavation and slab subgrades, but do not allow the areas to become saturated.
- Place a "mudmat" of lean concrete to seal the bearing stratum in the event wet conditions are experienced or expected.
- Minimize traffic in excavations to only that necessary to place the steel and concrete for the footings.



Remove free water in the excavations prior to placing concrete.

DEEP FOUNDATIONS

Drilled Concrete Shafts

Drilled concrete shafts are a common foundation system for the planned construction, and when suitably reinforced, are particularly efficient in resisting uplift and horizontal forces. The following paragraphs provide design recommendations and construction considerations for a drilled concrete shaft supported foundation system.

Axial Resistance

We have predicted the nominal (ultimate) compression and tension geotechnical resistance for various drilled concrete shaft diameters and depths for static load conditions using contributions from skin friction and end bearing. The nominal side friction resistance of the drilled concrete shafts was predicted for uncased conditions using published design approaches for calculation of skin friction including the alpha (α) method for cohesive soils and the β -method for cohesionless soils, assuming uncased construction. The skin friction resistance from the upper 4 feet of the shaft was neglected. The nominal end bearing resistance for the drilled concrete shaft was estimated using classic bearing capacity theory for cohesive soils and empirical correlations between corrected Standard Penetration Test (SPT) N₆₀ values and the mobilized base resistance for cohesionless soils. If casing is used, the nominal compression and tension resistance in the tables below should be reduced by 10%.

The following table provides our recommendations for the nominal (ultimate) geotechnical resistance in kips for individual drilled shafts.

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Drilled Shaft Axial Resistance Summary ¹								
Drilled Shaft	Nominal (Ultimate) Compression Resistance			Nominal (Ultimate) Tension Resistance				
Depth		(kips) ³			(kips) ^{3, 4}			
(feet) ²	Shaft Diameter (inches)			Sł	haft Diamet	er (inches)		
	18	24	30	36	18	24	30	36
20	75	108	147	189	46	62	79	96
25		139	187	241		81	102	125
30		182	246	324		103	130	159
35		212	285	363		126	159	194
40		252	334	421		159	201	244

1. Design capacities are dependent upon the method of installation, and quality control during installation. The values provided are estimates and should be verified when installation protocols have been finalized.

2. Measured from the ground surface at the time of field exploration.

3. NR - Not Recommended. The depth of 18-inch diameter shafts is limited to not more than 20 feet due to anticipated installation difficulty below this depth.

4. Buoyant weight of shaft is included in nominal tension resistance.

The shaft resistances presented in the table above are the nominal (ultimate) geotechnical resistances and appropriate ASD factors of safety for the design should be established considering control methods specified to verify field capacity at the time of construction. Provided below are the recommended factors of safety that can be considered for this project:

Field Capacity Verification Method	ASD Factor of Safety
Static Load Test on minimum 1 test shaft per structure (after verification that concrete is at design strength). Full-time observation of production shaft installation	2
No static load test, but full-time observation of production shaft installation.	2.5

The allowable tension capacity should be determined using a factor of safety of 3 unless a static tension load test is performed. Design capacities can be increased by 33% for highly transient loads such as wind loads, unless the transient loads have already been included in the factored design load (subject to verification of allowable structural capacity).

The structural capacity of the shafts should be evaluated by the structural engineer to assure that they can safely accommodate the combined stresses that may be induced by axial and lateral



loads, drag loads, and overturning moments. The shaft should be adequately reinforced full depth to develop the full tension resistance.

Shaft top spacing is normally set to allow for typical construction tolerances in placement and vertical alignment. Drilled shafts should have a minimum (center-to-center) spacing of three diameters. For large shaft groups, the final design should be checked to evaluate potential for group settlement.

Lateral Capacity

The response of deep foundations to lateral loads is not only dependent upon the soil material's horizontal subgrade reaction, but also on the shaft actual cross-sectional features, effective length, stiffness, arrangement in the shaft cap with respect to direction of loading, and "fix-head" or "free-head" cap interaction conditions. The analysis is usually performed to provide a lateral load that result in some limiting amount of deflection or to a specified maximum yield moment capacity of the shaft. Shafts subjected to lateral and moment loading should be analyzed as part of the structural detailing. Tensile and lateral load resistance of deep foundation elements should be neglected unless the shafts are adequately reinforced.

We have not performed a lateral resistance analyses as part of this scope. However, we have included soil parameters below for a lateral analysis using LPILE[™] software. If lateral loads exceed approximately 10 kips/shaft, a detailed analysis of lateral load resistance should be performed after the actual loading conditions and shaft configurations have been determined considering reductions for shadowing in a shaft group.

The following table lists input values for use in LPILETM analyses. LPILETM estimates values of k_h and E_{50} based on undrained strength; however, non-default values of k_h should be used where provided. Since deflection or a service limit criterion will likely control lateral capacity design, no safety/resistance factor is included with the parameters.

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Approximate Depth Below the Existing Grade (ft) ¹	LPILE [™] Soil p-y Model	Effective Unit Weight (lb/ft ³)	Cohesion (lb/ft²)	Internal Angle of Friction (Degrees)	Strain ² ₈₅₀	Static Lateral Subgrade Modulus ² k (Ib/in ³)
Lean Clay/Silt ² 0 – 2	Stiff Clay w/o free water	115				
Lean Clay 2 – 4	Stiff Clay w/o free water	130	1,800		0.007	500
Fat Clay 4 – 8	Stiff Clay w/o free water	131	1,800		0.007	500
Lean Clay 8 – 11	Stiff Clay w/o free water	68	1,250		0.007	500
Clayey Sand 11 – 15	Sand (Reese)	58		30		60
Lean Clay/ Fat Clay 15 – 27	Stiff Clay w/o free water	59	1,250		0.007	500
Lean Clay/ Fat Clay 27 – 40	Stiff Clay w/o free water	56	1,600		0.007	500
Clayey Sand 40 – 45	Sand (Reese)	58		39		125
Lean Clay 45 – 50	Stiff Clay w/o free water	70	1,500		0.007	500

1. Minimum foundation depth of 16-ft. If the foundation length is less than 16 feet, analysis for fixity is warranted.

2. The upper 2-feet should not be considered to provide full passive resistance due to potential for disturbance and desiccation effects.

When shafts are used in groups, the lateral capacities of the shafts in the second, third, and subsequent rows of the group should be reduced as compared to the capacity of a single, independent shaft. Guidance for applying p-multiplier factors to the p values in the p-y curves for each row of shaft foundations within a shaft group are as follows:

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- Front row: P_m = 0.8
- Second row: P_m = 0.4
- Third and subsequent row: P_m = 0.3.

For the case of a single row of shafts supporting a laterally loaded grade beam, group action for lateral resistance of shafts would need to be considered when spacing is less than three shaft diameters (measured center-to-center). However, spacing closer than 3D (where D is the diameter of the shaft) is not recommended, due to potential for the installation of a new shaft disturbing an adjacent installed shaft, likely resulting in axial capacity reduction.

Tensile and lateral load resistance of deep foundation elements should be neglected unless the shafts are adequately reinforced. The installation of a long reinforcing cages can be problematic with small diameter shafts. Therefore, it may be appropriate in some cases to design the foundations with deeper foundation caps or grade beams or utilize other means of lateral support where high lateral loads occur.

Load Testing

If a factor of safety of 2 is used to establish the allowable shaft resistance, a static load test should be performed to validate the predicted axial resistance. The cost of the load test should be considered in the selection of the factor of safety/resistance factor for shaft design.

If a load test is planned, at least one shaft representing the predominant diameter and depth should be tested. However, if more than one depth will be used, additional load tests should be added. Alternatively, the shaft can be instrumented with strain gages to provide load distribution information during the testing of a single shaft to allow for estimating allowable loads for shorter shafts. The test shaft(s) should be installed using the installation methods planned for production foundation elements.

For a static load test, the shafts should be loaded to a minimum of 250% of its design capacity after confirming the concrete strength, but typically not sooner than 7 days after installation. Ideally the shafts should be loaded to produce top of shaft movement as provided below to allow for an accurate interpretation of the ultimate resistance.



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Shaft Diameter (inches)	Minimum Top of Shaft Movement For Load Test Interpretation (inches)
18	1-1/4
24	1-1/2
30	1-3/4
36	2

The load test including design of the reaction beam and shafts should be provided by the foundation contractor. However, we should oversee the load testing program and validate our capacity predictions based upon the test results.

Shaft Settlement, Drag Load and Down Drag

Shafts installed into the stiff to very stiff, overconsolidated clays below approximately 25 feet from existing grade at the site should experience minimal settlements. Top of shaft movement of less than 1 inch is expected for the allowable design loads. These movements are associated with the loading from the structure and would be in addition to any fill-induced or down-drag settlement, where applicable.

If more than three feet of fill will be placed at this site to achieve final grade, fill induced settlement will create drag load on the shafts which may result in excessive shaft movement from down-drag effects. Drilled shafts typically have sufficient structural capacity to account for drag loads that may develop. Our office should be notified if fill heights exceeding three feet are planned so that we can evaluate the expected top of shaft movement and other potential settlement related development issues.

Drilled Shaft Construction Considerations

The drilling contractor should be experienced in the subsurface conditions observed at the boring locations, and the shaft excavations should be performed with equipment capable of efficiently advancing through the soil and providing a clean bearing area. The straight–shaft foundations should be installed in general accordance with the procedures presented in "Drilled Shafts: Construction Procedure and Design Methods," Publication No. FHWA-NHI-18-024, FHWA GEC 010, September 2018 by the U.S. Department of Transportation Federal Highway Administration, and "Standard Specification for the Construction of Drilled Piers," ACI Publication No. 336.1-01, 2011.

Because the subsurface conditions could vary away from the boring locations, we recommend that the Geotechnical Engineer or his representative observe the shaft installations to evaluate that the intended bearing material is encountered and sufficiently penetrated, and to provide recommendations should conditions vary from those encountered at our borings.



The subsurface conditions predominantly consist of medium stiff to stiff, lean to fat clays. The clay soils should be relatively easy to drill through using conventional auger drilling equipment. However, the shaft contractor should consider utilizing mud slurry or temporary steel casing to maintain stability of the upper portions of the excavation, particularly at depths of about 11 feet where groundwater and clayey sand were encountered. Prediction of excavation cave-in and the need for casing or mud slurry methods is not exact and depends on many factors including but not limited to: soil strength, sand/silt content, excavation and drilling methods, planned diameter and depth of the excavation, water table at time of construction, amount of time shaft excavation will be open, etc. The need for casing/mud slurry is best evaluated at the time of actual construction. As stated previously, the occurrence of sand and silt layering below a depth of 11 feet and related groundwater may cause difficulties with shaft excavation stability.

The concrete for the drilled shafts should be a flowable mix that can achieve the required compressive strength with a slump of 7 to 9 inches. If open excavation techniques are planned the concrete should be on-site near the end of the shaft excavation process and placed immediately after final excavation of the shaft. Free-fall concrete placement in dry drilled shafts is acceptable, provided care is taken to avoid striking the concrete on the sides of the excavation or the reinforcing steel. A bottom-dump hopper or a tremie, discharging near the bottom of the excavation, could be used to place concrete and reduce concrete segregation. If the mud slurry method is used, the discharge hose end should be placed at the base of the excavation prior to pumping the concrete. A "pig" should be used to reduce the mixing of drill mud and concrete in the discharge hose, and the discharge hose should be continuously raised during the placement with at least five feet of concrete head maintained over the discharge end of the hose. Proper construction techniques and quality control are important for the integrity of the deep foundation system. The drilled shaft installation process should be performed under the observation of the Geotechnical Engineer. The Geotechnical Engineer should document the shaft installation process including soil and groundwater conditions encountered, consistency with expected conditions, and details of the installed shaft.

SEISMIC CONSIDERATIONS

The seismic design requirements for buildings and other structures are based on Seismic Design Category. Site Classification is required to determine the Seismic Design Category for a structure. The Site Classification is based on the upper 100 feet of the site profile defined by a weighted average value of either shear wave velocity, standard penetration resistance, or undrained shear strength in accordance with Section 20.4 of ASCE 7 and the International Building Code (IBC). Based on the soil properties encountered at the site and as described on the exploration logs and results, it is our professional opinion that the **Seismic Site Classification is D**. Subsurface explorations at this site were extended to a maximum depth of 50 feet. The site properties below the boring depth to 100 feet were estimated based on our experience and knowledge of geologic



conditions of the general area. Although not considered necessary, additional deeper borings or geophysical testing may be performed to confirm the conditions below the current boring depth.

FLOOR SLABS

The subgrade soils below a depth of 2 feet are comprised of high plasticity clays exhibiting the potential to swell with increased water content. Construction of the floor slab, combined with the revising site drainage creates the potential for gradual increased water contents within the clays. Increases in water content will cause the clays to swell and damage the floor slab. To reduce the swell potential to less than about 1 inch, at least the upper 3 feet of subgrade soils below the floor slab (excluding the floor slab support course) should be an approved Low Volume Change (LVC) buffer consisting of lean clays as specified in the Earthwork section. This buffer can be comprised of undercutting the existing soils onsite and replacing with structural lean clay fill or increasing the grade of the site with lean clay above the site grade, or a combination of both.

This report provides recommendations to help mitigate the effects of soil shrinkage and expansion. However, even if these procedures are followed, some movement and (at least minor) cracking in the structure should be anticipated. The severity of cracking and other damage such as uneven floor slabs will probably increase if modification of the site results in excessive wetting or drying of the expansive soils. Eliminating the risk of movement and distress may not be feasible, but it may be possible to further reduce the risk of movement if significantly more expensive measures are used during construction. Some of these options are discussed in this report such as additional undercut and replacement of expansive soils or a structural slab.

Design parameters for floor slabs assume the requirements for **Earthwork** have been followed. Specific attention should be given to positive drainage away from the structure and positive drainage of the granular base beneath the floor slab.

Item	Description		
	A leveling course of 4-6 inches of free-draining (less than 10% passing the U.S.		
Floor Slab Support ¹	No. 200 sieve) sand compacted to at least 95% of ASTM D 698 ² over		
	compacted structural fill and/or stable subgrade.		
Estimated Modulus of			
Subgrade Reaction ² 100 pounds per square inch per inch (psi/in) for point loads.			
 Free-draining granular material should have less than 10 percent fines (material passing the No. 200 sieve Other design considerations such as cold temperatures and condensation development could warrant mor extensive design provisions. 			

Floor Slab Design Parameters

2. Modulus of subgrade reaction is an estimated value based upon our experience with the subgrade condition, the requirements noted in Earthwork, and the floor slab support as noted in this table. It is

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Item	Description
provided for point lo	ads. For large area loads the modulus of subgrade reaction would be substantially
lower.	

The use of a vapor retarder should be considered beneath concrete slabs on grade covered with wood, tile, carpet, or other moisture sensitive or impervious coverings, or when the slab will support equipment sensitive to moisture. When conditions warrant the use of a vapor retarder, the slab designer should refer to ACI 302 and/or ACI 360 for procedures and cautions regarding the use and placement of a vapor retarder.

Saw-cut control joints should be placed in the slab to help control the location and extent of cracking. For additional recommendations refer to the ACI Design Manual. Joints or cracks should be sealed with a water-proof, non-extruding compressible compound specifically recommended for heavy duty concrete pavement and wet environments.

Where floor slabs are tied to perimeter walls or monolithic turn-down slabs are designed to meet structural or other construction objectives, our experience indicates differential movement between the walls and slabs will likely be observed in adjacent slab expansion joints or floor slab cracks beyond the length of the structural dowels. The Structural Engineer should account for potential differential settlement through use of sufficient control joints, appropriate reinforcing or other means.

Settlement of floor slabs supported on existing fill materials cannot be accurately predicted, but could be larger than normal and result in some cracking. Mitigation measures as noted in **Existing Fill** within **Earthwork** are critical to the performance of floor slabs. In addition to the mitigation measures, the floor slab can be stiffened by adding steel reinforcement, grade beams and/or posttensioned elements.

Floor Slab Construction Considerations

Finished subgrade within and for at least 10 feet beyond the floor slab should be protected from traffic, rutting, or other disturbance and maintained in a relatively moist condition until floor slabs are constructed. If the subgrade should become damaged or desiccated prior to construction of floor slabs, the affected material should be removed and structural fill should be added to replace the resulting excavation. Final conditioning of the finished subgrade should be performed immediately prior to placement of the floor slab support course.

The Geotechnical Engineer should approve the condition of the floor slab subgrades immediately prior to placement of the floor slab support course, reinforcing steel and concrete. Attention should be paid to high traffic areas that were rutted and disturbed earlier, and to areas where backfilled trenches are located.

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POST TENSION SLAB DESIGN PARAMETERS

Post Tension (PT) slabs are common in this type of construction and can be effective in reducing slab cracking and effects from unanticipated differential movement from settlement and shrink/swell of underlying soils. We understand a PT slab will be utilized for the tennis courts associated with this project. The soil parameters provided below are based on the Post Tensioning Institute (PTI) method which is outlined in the "PTI Design of Post-Tensioned Slabs-on-Ground, 3rd Edition (2008)". The design parameters provided correspond with a post-tensioned slab-on-grade foundation that is placed on approximately 3 feet of compacted lean clay soils over the native lean/fat clays with the exterior grade beams placed at least 18 inches below the final grade on compacted structural fill as specified herein. Foundations placed at least 12 inches below finished grade can be designed for a net allowable bearing pressure of 2,000 psf. The continuous grade beams should experience a total settlement of less than 1 inch with differential of about ½ inch over 30 feet. If any changes are anticipated in the subgrade or fill conditions, Terracon should be notified in order to verify the recommendations provided.

Post-Tensioned Slab Design Parameters				
ltem	Parameter			
Estimated Edge Meisture Variation	Edge Lift: 5.1 feet			
Estimated Edge Moisture Variation, e _m	Center Lift: 9 feet			
Estimated Differential Soil Movement, ym	Edge Lift: 1.38 inches			
Estimated Differential Soft Movement, ym	Center Lift: 0.79 inches			
Friction Coefficient	0.35			
Potential Vertical Rise, PVR	~ 1 inch			

It should be noted that the differential soil movements of the project site in-situ material do not account of the influence of vegetation located near the proposed building footprint, which can impact the foundation's performance. The design of the exterior grade beam to a depth of 18 inches feet below finished grade should aid in reducing some of these effects, but deeper embedment may be necessary to account for effects of trees. Planting of large landscaping next to the tennis court should be minimized to the extent practical.

The foundation excavations should be inspected by a representative of Terracon before placement of steel or concrete to assess the that the excavation can support the design loads and are consistent with the materials discussed in the report. Soft or loose areas encountered



within the bottom of the footing excavation should be removed and replaced with properly compacted structural fill material as described in the **Earthwork** section of the report.

Once the footing excavations have been opened and inspected, the concrete should be promptly placed to avoid the excavation bottoms being exposed to weather. Surface runoff should be diverted away from the foundation excavations and should not be permitted to pond before or during construction. If the excavations must be left open for an extended period (over 1 day), then they should be covered and protected to prevent evaporation and any introduction of moisture.

ARTIFICIAL TURF RECOMMENDATIONS

Subgrade Conditions

Surficial material at the existing football field consists of low to medium plasticity silt, silty clay, and lean clay to a depth of 2 feet and fat clay below a depth of 2 feet. It is our understanding that the proposed football field elevation will be established within a few inches of the existing grades. The exposed subgrade soils will be conducive for the support of the proposed artificial turf either on 12 inches of lime-treated fill cap or on 12 inches of aggregate base. Since turf systems were not specified prior to report completion, we have provided two typical turf system construction methods below.

Prior to placement of the lime-treated fill or aggregate base, site preparation should be completed in accordance with the **Earthwork** section, and low-volume change fill should be placed to the base of the lime-treated fill or aggregate base.

"FieldTurf" artificial turf system can be established over a 12-inch layer of permeable aggregate (#57 stone or similar) over filter fabric placed over the stable/proof-rolled subgrade.

"Geo-Surfaces" turf system consisting of drainage underlayment and turf cover can be supported on a minimum 12 inches of lime-treated fill which should meet the requirements of imported lean clay specified in the **Earthwork** section.

Design Considerations

Artificial turf performance is affected by its surroundings, especially by presence of water. Turf subgrade should be sloped to provide rapid drainage of surface water. Water allowed to pond on or adjacent to the pavements could saturate the subgrade and contribute to premature turf deterioration. The civil engineer should consider the following drainage recommendations in the design and layout of pavements:

- Final grade adjacent to field areas should slope down from the edges;
- The subgrade surface should be sloped to promote proper subsurface drainage;
- Perimeter drain systems should be properly installed;



It is our understanding that a 'French Drain', or similar perimeter drain system, will be installed at the site. To prevent migration/transport of fines through the drain system a perforated drain pipe with filter fabric sock should be placed within a permeable aggregate which also should be encased in filter fabric.

DETENTION PONDS

We understand a detention pond will be constructed in the northeast corner of the project site. Beneath the silty clay (CL-ML), silt (ML), and lean clay (CL) soils encountered to a depth of about 2 foot below existing grade, the underlying soils generally consisted of fat clay (CH) soils ranging from a depth of about 2 feet to 8 feet below existing grade.

For construction of detention ponds, site preparation should include removal of existing vegetation, topsoil, root mats, unstable silty soils, and loose, soft or otherwise unsuitable material in accordance with the **Earthwork** section prior to pond excavation activities. Pond side slopes should be constructed no deeper than 3-horizontal to 1-vertical to prevent side slope failure. Surface instability is not expected on the slopes of the proposed improvements for a pond up to about 9 feet deep, especially after site preparation operations. However, surficial slope instability typically impacts the upper 3 to 5 feet of the subsurface profile, predominantly during extended wet and dry periods. The contractor should check for the occurrence of tension cracks along the banks during construction and after construction is completed. The banks should also be visually inspected periodically during routine maintenance. Tension cracks are initial signs of the soil sliding off the pond bank. The contractor should stop work and move equipment and stockpiles away from the top of the bank immediately if cracks or other signs of slope movement are identified.

If future surficial slope erosion occurs near the crest of slopes, we recommend the slope face be restored as soon as practical. We recommend irrigated landscaping be setback a minimum of 30 feet from the crest of the slopes.

If the pond is expected to extend deeper than 9 feet below existing grade, the base of the pond may extend into sandy lean clay (CL) or clayey sand (SC) soils. If these soils are anticipated, we should be contacted to provide recommendations on clay liner soil characteristics and general construction considerations associated with encountering groundwater.



PAVEMENTS

General Pavement Comments

Pavement designs are provided for the traffic conditions and pavement life conditions as noted in **Project Description** and in the following sections of this report. A critical aspect of pavement performance is site preparation. Pavement designs noted in this section must be applied to the site which has been prepared as recommended in the **Earthwork** section.

Support characteristics of subgrade for pavement design do not account for shrink/swell movements of an expansive clay subgrade. Thus, the pavement may be adequate from a structural standpoint, yet still experience cracking and deformation due to shrink/swell related movement of the subgrade.

Pavement Design Parameters

Design of Asphaltic Concrete (AC) pavements are based on the procedures outlined in the National Asphalt Pavement Association (NAPA) Information Series 109 (IS-109). Design of Portland Cement Concrete (PCC) pavements are based upon American Concrete Institute (ACI) 330; Guide for Design and Construction of Concrete Parking Lots.

A subgrade CBR of 4 was used for the AC pavement designs, and a modulus of subgrade reaction of 130 pci was used for the PCC pavement designs. The values were empirically derived based upon our experience with the lean clay and fat clay subgrade soils and our understanding of the quality of the subgrade as prescribed by the **Site Preparation** conditions as outlined in **Earthwork**. A modulus of rupture of 600 psi, corresponding to a 4,000 psi compressive strength, was used for concrete pavement.

Pavement Section Thicknesses

The following table provides options for AC and PCC Sections:

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Asphaltic Concrete Design					
	Minimum Thickness (inches)				
Layer	Parkir	ig Stalls	Drive	ways	Entrances, Exits ⁴
Asphalt Surface and Binder ¹		3	2	Ļ	Concrete Only
Aggregate Base ^{2,3}	6		6		4

1. Design and construction of asphaltic or bituminous concrete should be in accordance with Louisiana Department of Transportation Specifications for Roads and Bridges 2016 (LSSRB).

- The aggregate base should be a No. 610 limestone or similarly graded recycled crushed concrete compacted to 100% of its max dry density as determined by ASTM D-698, Standard Proctor Test with stability present.
- 3. Alternatively, a minimum 9-inches of soil-cement base should be constructed in general accordance with Section 305 of the 2016 LSSRB. The lime and/or cement addition rates should be based upon classification testing performed on the actual proposed soils at the time of construction in accordance with Section 305.04. Based on soil conditions observed in the upper 2 feet at the soil boring locations the cement addition rate should be 10% Type I Cement by volume. Initial lime treatment with 6% hydrated lime by volume may be necessary depending on soils present at the finished subgrade at the time of construction to reduce PI to less than 15 prior to cement treatment.
- 4. A minimum 7-inch concrete pavement is recommended at entrances to provide increased resistance to turning forces and rutting. PCC pavements are recommended for trash container pads and in any other areas subjected to heavy wheel loads and/or turning traffic.

Portland Cement Concrete Design				
	Thickness (inches)			
Layer	Parking Stalls Driveways Entrances, Exits Dumpster Pac			
PCC ^{1, 2}	5	6	7	8
Aggregate Base ^{3, 4}	4	4	4	4

1. 4,000 psi at 28 days, 4-inch maximum slump and 3 to 5 percent air entrained. PCC pavements are recommended for trash container pads and in any other areas subjected to heavy wheel loads and/or turning traffic.

Standard design and construction details for rigid pavements are contained in ACI330R-21. It is
recommended that the design engineer refer to this document for more detailed information. A critical
aspect of concrete pavements for facilities of this nature is joint spacing and related details. ACI330R-21
addresses these important details.

- 3. Aggregate base course should be a No. 610 limestone or similarly graded recycled concrete compacted to 100% of its max dry density as determined by ASTM D-698, Standard Proctor Test with stability present.
- 4. The aggregate base will serve to protect the subgrade, reduce pumping of fines, and reduce shrink/swell affects for the concrete pavement applications. Alternatively, a minimum 9 inches of compacted select low plasticity structural fill (compacted to a minimum 95% of the standard proctor maximum dry density) could

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	Portland Cement Concrete Design					
		Thickness (inches)				
		Parking Stalls				
5.	be placed across the site under the planned PCC pavements incorporating minimum 2-ft strips of geotextile fabric at each planned control joint locations.					

The estimated pavement sections provided in this report are minimums for the assumed design criteria, and as such, periodic maintenance should be expected. Areas for parking of heavy vehicles, concentrated turn areas, and start/stop maneuvers could require thicker pavement sections. Edge restraints (i.e. concrete curbs or aggregate shoulders) should be planned along curves and areas of maneuvering vehicles. A maintenance program including surface sealing, joint cleaning and sealing, and timely repair of cracks and deteriorated areas will increase the pavement's service life. As an option, thicker sections could be constructed to decrease future maintenance.

Although not required for structural support of PCC pavements, a minimum 4-inch thick dense graded aggregate base course layer is recommended to help reduce potential for slab curl, shrinkage cracking, and subgrade pumping through joints. Proper joint spacing will also be required to prevent excessive slab curling and shrinkage cracking. Joints should be sealed to prevent entry of foreign material and dowelled where necessary for load transfer.

Timing of saw-cutting is also very important to reduce formation of shrinkage cracking. Where practical, we recommend early-entry cutting of crack-control joints in PCC pavements. Cutting of the concrete in its "green" state typically reduces the potential for micro-cracking of the pavements prior to the crack control joints being formed, compared to cutting the joints after the concrete has fully set. Micro-cracking of pavements may lead to crack formation in locations other than the sawed joints, and/or reduction of fatigue life of the pavement.

Openings in pavements, such as decorative landscaped areas, are sources for water infiltration into surrounding pavement systems. Water can collect in the islands and migrate into the surrounding subgrade soils thereby degrading support of the pavement. This is especially applicable for islands with raised concrete curbs, irrigated foliage, and low permeability near-surface soils. The civil design for the pavements with these conditions should include features to restrict or to collect and discharge excess water from the islands. Examples of features are edge drains connected to the storm water collection system, longitudinal subdrains, or other suitable outlet and impermeable barriers preventing lateral migration of water such as a cutoff wall installed to a depth below the pavement structure.



Dishing in parking lots surfaced with ACC is usually observed in frequently used parking stalls (such as near the front of buildings), and occurs under the wheel footprint in these stalls. The use of higher-grade asphaltic cement, or surfacing these areas with PCC, should be considered. The dishing is exacerbated by factors such as irrigated islands or planter areas, sheet surface drainage to the front of structures, and placing the ACC directly on a compacted clay subgrade.

Pavement Drainage

Pavements should be sloped to provide rapid drainage of surface water. Water allowed to pond on or adjacent to the pavements could saturate the subgrade and contribute to premature pavement deterioration. In addition, the pavement subgrade should be graded to provide positive drainage within the granular base section.

Pavement Maintenance

The pavement sections represent minimum recommended thicknesses and, as such, periodic maintenance should be anticipated. Therefore, preventive maintenance should be planned and provided for through an on-going pavement management program. Maintenance activities are intended to slow the rate of pavement deterioration and to preserve the pavement investment. Maintenance consists of both localized maintenance (e.g. crack and joint sealing and patching) and global maintenance (e.g. surface sealing). Preventive maintenance is usually the priority when implementing a pavement maintenance program. Additional engineering observation is recommended to determine the type and extent of a cost-effective program. Even with periodic maintenance, some movements and related cracking may still occur, and repairs may be required.

Pavement performance is affected by its surroundings. In addition to providing preventive maintenance, the civil engineer should consider the following recommendations in the design and layout of pavements:

- Final grade adjacent to paved areas should slope down from the edges at a minimum 2%.
- Subgrade and pavement surfaces should have a minimum 2% slope to promote proper surface drainage.
- Install below pavement drainage systems surrounding areas anticipated for frequent wetting.
- Place 8 inches of compacted dense graded crushed stone around drop inlet basins extending at least 8 inches from the perimeter to reduce settlement at pavement interface.
- Install joint sealant and seal cracks immediately.
- Seal all landscaped areas in or adjacent to pavements to reduce moisture migration to subgrade soils.
- Place compacted, low permeability backfill against the exterior side of curb and gutter.
- Place curb, gutter and/or sidewalk directly on clay subgrade soils rather than on unbound granular base course materials.



Aggregate Pavement Thickness

Aggregate pavements designed in accordance with the following table may be implemented for drives and parking areas onsite.

Typical Pavement Section Thickness (inches)						
Traffic Area Aggregate Base Course ^{1,2} Woven Geotextile						
Limestone Aggregate Paving	12	Mirafi HP370 or equivalent				
 Aggregate base course should be a No. 610 limestone or similarly graded recycled concrete compacted to 95% of its max dry density as determined by ASTM D-1557, Modified Proctor Test with stability present over high- performance geotextile. 						
2. The aggregate paving should be placed over stable subgrade prepared as recommended in the Earthwork section.						

Aggregate Pavement Maintenance

The pavement sections represent minimum recommended thicknesses and, as such, periodic maintenance should be anticipated. We recommend that preventive maintenance should be planned and provided for through an on-going pavement management program to slow the rate of pavement deterioration, and to preserve the pavement investment. Preventive maintenance is usually the first priority when implementing a planned pavement maintenance program and provides the highest return on investment for pavements. Over time the placement of additional limestone material will likely be required within aggregate paved areas that exhibit depressions. These areas should be filled with additional limestone rather than scalping of material from adjacent areas. Prior to implementing any maintenance, additional engineering observation is recommended to determine the type and extent of preventive maintenance. Even with periodic maintenance, some movements may still occur, and repairs may be required.

GENERAL COMMENTS

Our analysis and opinions are based upon our understanding of the project, the geotechnical conditions in the area, and the data obtained from our site exploration. Natural variations will occur between exploration point locations or due to the modifying effects of construction or weather. The nature and extent of such variations may not become evident until during or after construction. Terracon should be retained as the Geotechnical Engineer, where noted in this report, to provide observation and testing services during pertinent construction phases. If variations appear, we can provide further evaluation and supplemental recommendations. If variations are noted in the absence of our observation and testing services on-site, we should be immediately notified so that we can provide evaluation and supplemental recommendations.

Our Scope of Services does not include either specifically or by implication any environmental or biological (e.g., mold, fungi, bacteria) assessment of the site or identification or prevention of



pollutants, hazardous materials or conditions. If the owner is concerned about the potential for such contamination or pollution, other studies should be undertaken.

Our services and any correspondence or collaboration through this system are intended for the sole benefit and exclusive use of our client for specific application to the project discussed and are accomplished in accordance with generally accepted geotechnical engineering practices with no third-party beneficiaries intended. Any third-party access to services or correspondence is solely for information purposes to support the services provided by Terracon to our client. Reliance upon the services and any work product is limited to our client, and is not intended for third parties. Any use or reliance of the provided information by third parties is done solely at their own risk. No warranties, either express or implied, are intended or made.

Site characteristics as provided are for design purposes and not to estimate excavation cost. Any use of our report in that regard is done at the sole risk of the excavating cost estimator as there may be variations on the site that are not apparent in the data that could significantly impact excavation cost. Any parties charged with estimating excavation costs should seek their own site characterization for specific purposes to obtain the specific level of detail necessary for costing. Site safety, and cost estimating including, excavation support, and dewatering requirements/design are the responsibility of others. If changes in the nature, design, or location of the project are planned, our conclusions and recommendations shall not be considered valid unless we review the changes and either verify or modify our conclusions in writing.

FIGURES

Contents:

GeoModel (2 Pages) Swell Test Results (3 Pages)





GeoModel



This is not a cross section. This is intended to display the Geotechnical Model only. See individual logs for more detailed conditions.

Model Layer	Layer Name	General Description	Topsoil	Silty Clay
1	Silty Clay and Lean Clay	Brown, reddish brown, gray, and tan, very stiff to hard, silty clay and lean clay	Lean Clay	Fat Clay
2	Upper Fat Clay	Gray, reddish brown, and tan, stiff to hard, fat clay	Sandy Lean Clay	💋 Clayey Sand
3	Upper Lean Clay and Sandy Silty Clay	Reddish brown, gray, and tan, medium stiff to very stiff, sandy lean clay, sandy silty clay, and lean clay	Poorly-graded Sand with Clay	
4	Upper Clayey Sand	Reddish brown and gray, loose to medium dense, clayey sand	Sandy Silty Clay	Poorly-graded Sand with Silt
5	Lower Fat Clay	Brown and dark gray, stiff to very stiff, fat clay; B-02 contains lean clay from 32 feet to 40 feet	Lean Olay with Gand	
6	Lower Clayey Sand	Dark gray and light gray, dense, clayey sand		
7	Lower Lean Clay	Light gray and tan, stiff to hard, lean clay and sandy lean clay		

LEGEND

NOTES:

Layering shown on this figure has been developed by the geotechnical engineer for purposes of modeling the subsurface conditions as required for the subsequent geotechnical engineering for this project.

IN First Water Observation

V Second Water Observation

The groundwater levels shown are representative of the date and time of our exploration. Significant changes are possible over time. Water levels shown are as measured during and/or after drilling. In some cases, boring advancement methods mask the presence/absence of groundwater. See individual logs for details.



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GeoModel



This is not a cross section. This is intended to display the Geotechnical Model only. See individual logs for more detailed conditions.

Model Layer	Layer Name	General Description
1	Silty Clay and Lean Clay	Brown, reddish brown, gray, and tan, very stiff to hard, silty clay and lean clay
2	Upper Fat Clay	Gray, reddish brown, and tan, stiff to hard, fat clay
3	Upper Lean Clay and Sandy Silty Clay	Reddish brown, gray, and tan, medium stiff to very stiff, sandy lean clay, sandy silty clay, and lean clay
4	Upper Clayey Sand	Reddish brown and gray, loose to medium dense, clayey sand
5	Lower Fat Clay	Brown and dark gray, stiff to very stiff, fat clay; B-02 contains lean clay from 32 feet to 40 feet
6	Lower Clayey Sand	Dark gray and light gray, dense, clayey sand
7	Lower Lean Clay	Light gray and tan, stiff to hard, lean clay and sandy lean clay

LEGEND



NOTES:

Layering shown on this figure has been developed by the geotechnical engineer for purposes of modeling the subsurface conditions as required for the subsequent geotechnical engineering for this project.

V First Water Observation

V Second Water Observation

The groundwater levels shown are representative of the date and time of our exploration. Significant changes are possible over time. Water levels shown are as measured during and/or after drilling. In some cases, boring advancement methods mask the presence/absence of groundwater. See individual logs for details. ATTACHMENTS



EXPLORATION AND TESTING PROCEDURES

Field Exploration

Number of Locations	Type of Exploration	Boring Depth (feet)	Drilled Location
2	Soil Borings	50	Two-story building areas
3	Soil Borings	30	Stadium seats / press box
9	Soil Borings	24	Building areas
4	Soil Borings	15	Detention pond / central plant
15	Soil Borings	10	Fields / courts
11	Soil Borings	6	Parking areas

Boring Layout and Elevations: Unless otherwise noted, Terracon personnel provided the boring layout. Coordinates were obtained with a handheld GPS unit (estimated horizontal accuracy of about ± 10 feet) and approximate elevations were estimated from the provided survey information. If elevations and a more precise boring layout are desired, we recommend borings be surveyed following completion of fieldwork.

Subsurface Exploration Procedures: We advanced the borings with a ATV-mounted rotary drill rig using continuous flight augers (solid stem) followed by rotary wash techniques. Samples were continuously obtained in the upper 10 feet of each boring and at maximum intervals of 5 feet thereafter. In the thin-walled tube sampling procedure, a seamless steel tube with a sharp cutting edge was pushed hydraulically into the soil to obtain a relatively undisturbed sample. In the split-barrel sampling procedure, a standard 2-inch outer diameter split-barrel sampling spoon was driven into the ground by a 140-pound automatic hammer falling 30 inches. The number of blows required to advance the sampling spoon the last 12 inches of a normal 18-inch penetration is recorded as the Standard Penetration Test (SPT) resistance value. The SPT resistance values, also referred to as N-values, are indicated on the boring logs at the test depths. We observed and recorded groundwater levels during drilling and sampling. For safety purposes, all borings were backfilled with auger cuttings or cement-bentonite grout, consistent with state regulations, upon completion. Pavements were patched with cold-mix asphalt and/or pre-mixed concrete, as appropriate.

The sampling depths, penetration distances, and other sampling information was recorded on the field boring logs. The samples were placed in appropriate containers and taken to our soil laboratory for testing and classification by a Geotechnical Engineer. Our exploration team prepared field boring logs as part of the drilling operations. These field logs included visual classifications of the materials encountered during drilling and our interpretation of the subsurface conditions between samples. Final boring logs were prepared from the field logs. The final boring logs represent the



Geotechnical Engineer's interpretation of the field logs and include modifications based on observations and tests of the samples in our laboratory.

Laboratory Testing

The project engineer reviewed the field data and assigned laboratory tests to understand the engineering properties of the various soil strata, as necessary, for this project. Procedural standards noted below are for reference to methodology in general. In some cases, variations to methods were applied because of local practice or professional judgment. Standards noted below include reference to other, related standards. Such references are not necessarily applicable to describe the specific test performed.

- ASTM D2216 Standard Test Methods for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass
- ASTM D4318 Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils
- ASTM D6913/D6913M Standard Test Methods for Particle-Size Distribution (Gradation) of Soils Using Sieve Analysis
- ASTM D2166/D2166M Standard Test Method for Unconfined Compressive Strength of Cohesive Soil
- ASTM D7263 Standard Test Methods for Laboratory Determination of Density (Unit Weight) of Soil Specimens
- ASTM D4546 Standard Test Methods for One-Dimensional Swell or Collapse of Soils The laboratory testing program often included examination of soil samples by an engineer. Based on the material's texture and plasticity, we described and classified the soil samples in accordance with the Unified Soil Classification System.

SITE LOCATION AND EXPLORATION PLANS

Contents:

Site Location Plan Exploration Plan

Note: All attachments are one page unless noted above.





GeoModel



This is not a cross section. This is intended to display the Geotechnical Model only. See individual logs for more detailed conditions.

Model Layer	Layer Name	General Description	Topsoil	Silty Clay
1	Silty Clay and Lean Clay	Brown, reddish brown, gray, and tan, very stiff to hard, silty clay and lean clay	Lean Clay	Fat Clay
2	Upper Fat Clay	Gray, reddish brown, and tan, stiff to hard, fat clay	Sandy Lean Clay	💋 Clayey Sand
3	Upper Lean Clay and Sandy Silty Clay	Reddish brown, gray, and tan, medium stiff to very stiff, sandy lean clay, sandy silty clay, and lean clay	Poorly-graded Sand with Clay	
4	Upper Clayey Sand	Reddish brown and gray, loose to medium dense, clayey sand	Sandy Silty Clay	Poorly-graded Sand with Silt
5	Lower Fat Clay	Brown and dark gray, stiff to very stiff, fat clay; B-02 contains lean clay from 32 feet to 40 feet	Lean Olay with Gand	
6	Lower Clayey Sand	Dark gray and light gray, dense, clayey sand		
7	Lower Lean Clay	Light gray and tan, stiff to hard, lean clay and sandy lean clay		

LEGEND

NOTES:

Layering shown on this figure has been developed by the geotechnical engineer for purposes of modeling the subsurface conditions as required for the subsequent geotechnical engineering for this project.

IN First Water Observation

V Second Water Observation

The groundwater levels shown are representative of the date and time of our exploration. Significant changes are possible over time. Water levels shown are as measured during and/or after drilling. In some cases, boring advancement methods mask the presence/absence of groundwater. See individual logs for details.



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GeoModel



This is not a cross section. This is intended to display the Geotechnical Model only. See individual logs for more detailed conditions.

Model Layer	Layer Name	General Description
1	Silty Clay and Lean Clay	Brown, reddish brown, gray, and tan, very stiff to hard, silty clay and lean clay
2	Upper Fat Clay	Gray, reddish brown, and tan, stiff to hard, fat clay
3	Upper Lean Clay and Sandy Silty Clay	Reddish brown, gray, and tan, medium stiff to very stiff, sandy lean clay, sandy silty clay, and lean clay
4	Upper Clayey Sand	Reddish brown and gray, loose to medium dense, clayey sand
5	Lower Fat Clay	Brown and dark gray, stiff to very stiff, fat clay; B-02 contains lean clay from 32 feet to 40 feet
6	Lower Clayey Sand	Dark gray and light gray, dense, clayey sand
7	Lower Lean Clay	Light gray and tan, stiff to hard, lean clay and sandy lean clay

LEGEND



NOTES:

Layering shown on this figure has been developed by the geotechnical engineer for purposes of modeling the subsurface conditions as required for the subsequent geotechnical engineering for this project.

V First Water Observation

V Second Water Observation

The groundwater levels shown are representative of the date and time of our exploration. Significant changes are possible over time. Water levels shown are as measured during and/or after drilling. In some cases, boring advancement methods mask the presence/absence of groundwater. See individual logs for details.

EXPLORATION RESULTS

Contents:

Boring Logs, B-01 through B-44 (49 pages)

Note: All attachments are one page unless noted above.

St. Louis Catholic High School Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan		el ns	edu	Ħ.c.	St	rength 1	Test	(%)	it G	Atterberg Limits	
Latitude: 30.1820° Longitude: -93.1564°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) <u>FAT CLAY (CH)</u> , brown, stiff to very stiff (continued)	-			-		90					-
-gray, stiff to very stiff below 28 feet				2.25 (HP)	UC	1.58	6.5	37.1	86		
	30-			2.25 (HP)		1.30	0.5	57.1	00		
	-										
	-										
				2.00 (HP)							
	35-										
	-										
38.0	1										
CLAYEY SAND (SC), dark gray, dense	-			0.25 (HP)				24.7			
	40-							-			-
-dense below 43 feet											
			X	6-15-19 N=34							
45.0 <u>SANDY LEAN CLAY (CL)</u> , light gray and tan, stiff to very stiff	45_		\wedge								
	-			_					_		
50.0	-			4.50 (HP)	UC	1.48	6	18.8	111		
Boring Terminated at 50 Feet	- 50-			_	T						1
											-
xploration and Testing Procedures for a description of field and laboratory	6	w	ater	Level Observatio	ons		-	-		Drill Rig	1
dures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.		7	-	irst encountered After 15 minutes						ATV Hammer Typ Rope and Cat	
				ement Method						Driller M.Billiot	
ion Reference: Elevations based on Google Earth		0'-	13'C	ontinuous Flight A Rotary Wash	luger					Logged by B. Alexander	
		At	ando	nment Method ackfilled with ber				100-00		Boring Start 08-04-2023	ed

Boring Completed 08-04-2023

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220 Prater Rd Sulphur, LA

St. Louis Catholic High School Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053





Location: See Exploration Plan Latitude: 30.1813° Longitude: -93.1581°	2	la IS	be	н.	St	rength 1	Test	(9)	£.	Atterberg Limits	
atitude: 30.1813° Longitude: -93.1581° epth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (H.) 			T								-
SILTY CLAY (CL), brown and light gray, very stiff to hard	-				-						
				4.50 (HP)	_	_					
FAT CLAY (CH), brown and gray, very stiff to hard				4.00 (HP)	uc	1.97	10	25.2	98	87-22-65	
	5-			3.25 (HP)							
-with trace silt below 6 feet	-	∇		4.25 (HP)							
8.0 <u>LEAN CLAY (CL)</u> , tan and light gray, stiff to very stiff, with trace silt				3.00 (HP)	UC	1.66	9.3	18.7	108	45-13-32	
11.0	10-					-				1000	
<u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, stiff				1.00 (HP)							
13.0 CLAYEY SAND (SC), reddish brown and light gray, medium dense											
16.0	15-		X	7-8-9 N=17				21.5			3
LEAN CLAY (CL), brown, medium stiff -with sand layers to 20 feet	-										
	1		\bigvee	3-4-3 N=7				28.8			-
	20-		\wedge	N=7	-						
22.0 FAT CLAY (CH), dark gray, stiff to very stiff	-										
-with trace sand to 25 feet				2 50 (110)							
	25-			2.50 (HP)	_						
Exploration and Testing Procedures for a description of field and laboratory				Level Observatio	ons					Drill Rig	
adures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		7	-	irst encountered After 15 minutes						ATV Hammer Typ Rope and Catl Driller	e heac
es ation Reference: Elevations based on Google Earth		0'-	-16' C	cement Method ontinuous Flight A Rotary Wash	uger					M.Billiot Logged by B. Alexander	

B. Alexander

Boring Started 08-01-2023

Boring Completed 08-01-2023

St. Louis Catholic High School Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Boring Log No. B-02

Location: See Exploration Plan		in s	e	2	St	rength T	est	(9)	÷,	Atterberg Limits	
Location: See Exploration Plan Latitude: 30.1813° Longitude: -93.1581°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) FAT CLAY (CH), dark gray, stiff to very stiff (continued)			-		-	20	01	-	-		-
	-		-								
	-			2.00 (HP)							
	30-										
	-										
32.0 LEAN CLAY (CL), dark gray, stiff											
	-	1.5									-
	+			1.75 (HP)	UC	1.69	5.5	35.7	88	49-18-31	
	35-										-
	-										
	-										
	-			1							
	-			1.50 (HP)							
40.0 CLAYEY SAND (SC), light gray, dense	- 40-										
	-										
	-			-							
45.0	45		Х	8-16-20 N=36							
LEAN CLAY (CL), light gray and tan, very stiff to hard, with sand seams and pockets	45_										
	-										
		1		1 50 (110)							
-low strain failure at 48 feet 50.0				4.50 (HP)	UC	3.21	4	19.1	114	-	97
Boring Terminated at 50 Feet	- 50-										
Exploration and Testing Procedures for a description of field and laboratory redures used and additional data (If any).	¢	w	and a	Level Observatio	ons					Drill Rig ATV	
Supporting Information for explanation of symbols and abbreviations.		A	-	fter 15 minutes						Hammer Typ Rope and Cath	e nead
			harris	om out Marker J						Driller M.Billiot	
0.2		Ad	16'Co	ement Method	uger					Logged by	
es ation Reference: Elevations based on Google Earth		16	-50'	ontinuous Flight A Rotary Wash	-					B. Alexander	
				Rotary Wash						B. Alexander Boring Starte 08-01-2023	ed

St. Louis Catholic High School Corbina Road and James Court | Lake Charles, LA

Terracon Project No. EU235053

Boring Log No. B-03



60	Location: See Exploration Plan	Depth (Ft.)	In st	be	¥.	Strength Test					Atterberg Limits	4
Graphic Log	Latitude: 30.1819° Longitude: -93.1581° Depth (Ft.)		Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
X	0.3 Approximately 3-inches of topsoil	1		T	44				6.0			1
	SILTY CLAY (CL-ML), brown -brown and light gray, very stiff to hard below 1 foot 2.0				4.00 (HP)				0.0			
	FAT CLAY (CH), tan and light gray, very stiff				2.25 (HP)	UC	2.35	15	18.4	118	65-13-52	
		5-			2.50 (HP)							
	8.0		V		2.50 (HP)							
	<u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, very stiff	10-			2.50 (HP)							
	11.0 SAND WITH CLAY (SP-SC), reddish brown, medium dense		V	X	6-8-9 N=17	-			26.4			11
	14.0				_							
	FAT CLAY (CH), brown, very stiff -with sand seams from 14 feet to 20 feet	15-			1.75 (HP)	UC	0.89	5.8	26.2	97		
		20-			2.50 (HP)							
		115										
					2.25 (HP)							
	24.0 Boring Terminated at 24 Feet											
roce	xploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any).		2	ZF	Level Observatio	ons					Drill Rig ATV	
lote				dvanc	ofter 15 minutes						Hammer Typ Rope and Cat Driller M. Billiot	head
leva	tion Reference: Elevations based on Google Earth		13	3'-24'	ontinuous Flight A Rotary Wash	luger					Logged by B. Alexander Boring Start 08-07-2023	ed
					ackfilled with aug	ger cutti	ngs upor	n comp	letion.		Boring Comp	olete

Boring Completed 08-07-2023
n	Location: See Exploration Plan		- 0	e		St	rength 1	Test		¢	Atterberg Limits	
	Latitude: 30.1820° Longitude: -93.1576°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
15	Depth (Ft.) 0.3 Approximately 3-inches of topsoil			Т			-					-
	1.0 SILTY CLAY (CL) , brown, very stiff to hard FAT CLAY (CH) , brown and light gray, stiff to very stiff			ż	4.50 (HP)				15.4	93	60-18-42	
		-				-			1			
					3.50 (HP)							
		5 -			2.25 (HP)	υc	3.05	13.3	16.3	114	53-16-37	
			V		2.00 (HP)							
		10			2.00 (HP)							
	11.0	10-										
	CLAYEY SAND (SC), reddish brown, medium dense				5-7-10	-						
			∇	A	N=17							
	14.0											
	FAT CLAY (CH), brown, stiff to very stiff, -with sand seams from 18 to 20 feet	15-			2.50 (HP)							
					2.50 (HP)							
	-gray and brown below 20 feet	20-										
					2.75 (HP)	UC	1.29	6	31.5	91		
	24.0 Boring Terminated at 24 Feet									-		1
ce	xploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.	6	N Z Z	ZF	Level Observation irst encountered After 15 minutes	ons					Drill Rig ATV Hammer Typ	e
											Rope and Catl	nea
	ion Reference: Elevations based on Google Earth		0'	-13'C	ement Method ontinuous Flight A Rotary Wash	uger					M. Billiot	
					the mart in a more that						B. Alexander	

Abandonment Method Boring backfilled with auger cuttings upon completion.

Boring Started 08-07-2023

Boring Completed 08-07-2023





Location: See Exploration Plan	1	/el	vpe	s st	_	rength '	_	(%)	it ocf)	Atterberg Limits	+
Location: See Exploration Plan Latitude: 30.1819° Longitude: -93.1571°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) T ³ 0.3 Approximately 3-inches of topsoil			\mathbf{T}		-	0.0		4.2		ND	-
1.0 SILT (ML), brown, with clay seams	-				_			4.2		NP	
SILTY CLAY (CL-ML), brown and light gray, hard 2.0				4.50 (HP)				1			
FAT CLAY (CH), gray and tan, very stiff -with ferrous nodules to 6 feet				3.75 (HP)	UC	3.41	7.8	15.8	117	52-15-37	
	5-			2.50 (HP)							
8.0	-	\mathbb{V}		2.25 (HP)	uc	2.55	7.3	19.6	111		
SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff	10-			2.50 (HP)							
11.0 CLAYEY SAND (SC), reddish brown, loose											
	1	V	Ą	4-5-5 N=10	-						
14.0 FAT CLAY (CH), brown, very stiff -with sand layers from 14 feet to 16 feet	15-		I	3.25 (HP)							
				2.75 (HP)	υc	2.21	5.2	27.5	95	70-22-48	
24.0	1 1			3.00 (HP)							
Boring Terminated at 24 Feet											
Exploration and Testing Procedures for a description of field and laboratory cedures used and additional data (If any).		w	Z F	Level Observatio	ons					Drill Rig ATV	
Supporting Information for explanation of symbols and abbreviations. tes vation Reference: Elevations based on Google Earth		0'-	Ivano	After 15 minutes Cement Method Continuous Flight A Rotary Wash	uger					Hammer Typ Rope and Catl Driller M.Billiot Logged by B. Alexander	head
		At	ando	onment Method backfilled with aug	ger cutti	ngs upoi	n comp	letion.		Boring Start 08-07-2023 Boring Comp 08-07-2023	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053

Boring Log No. B-06

Location: See Exploration Plan	~	el ns	be	Ħ.e	St	rength T	est	(%	e,	Atterberg Limits	
Latitude: 30.1826° Longitude: -93.1578°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3_Approximately 4-inches of topsoil			T			-	-				+
1.0 SILTY CLAY (CL), brown	-				-			-		A	
FAT CLAY (CH), brown and tan, stiff to very stiff	-			4.50 (HP)	-		_	18.0	_	68-19-49	
				2.00 (HP)	UC	1.87	6.7	19.0	105	62-19-43	
-with ferrous nodules from 4 feet to 6 feet	5-			2.00 (HP)							
8.0				2.50 (HP)							
SANDY LEAN CLAY (CL), reddish brown and light gray, medium stiff to stiff -low strain failure at 8 feet	10-			1.75 (HP)	UC	0.97	3.3	20.0	109		
11.0 CLAYEY SAND (SC), reddish brown, medium dense		V	X	5-5-8 N=13							
14.0 LEAN CLAY (CL), brown, very stiff, with sand seams 16.0	15			3.00 (HP)							
<u>FAT CLAY (CH)</u> , brown, very stiff				2.75 (HP)							
-brown and gray below 22 feet 24.0				3.00 (HP)							
Boring Terminated at 24 Feet											
xploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any).	-	w		Level Observatio	ons					Drill Rig	-
dures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.		7	-	irst encountered After 15 minutes						ATV Hammer Typ Rope and Cat Driller	be head
s ion Reference: Elevations based on Google Earth		0'-	13'C	ement Method ontinuous Flight A Rotary Wash	uger					M. Billiot Logged by B. Alexander Boring Start	ed

Abandonment Method Boring backfilled with auger cuttings upon completion.



Boring Completed 08-07-2023

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220 Prater Rd Sulphur, LA



бо	Location: See Exploration Plan		la si	be	÷	St	rength ⁻	Test	(9)	t cJ	Atterberg Limits	1
Graphic Log	Latitude: 30.1814° Longitude: -93.1572°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines
11. 3	Depth (Ft.) 0.3_Approximately 4-inches topsoil		-	Т			0.4					
	LEAN CLAY (CL), brown and light gray, stiff to very stiff	-				-		1	1	_	2.00 - 0.00	
	and the second				4.50 (HP)	UC	1.72	2	7.7	103	30-10-20	
	-with silt seams to 2 feet				4.50 (HP)							
	4.0											
	FAT CLAY (CH), tan and gray, medium stiff to stiff, slickensided	5-			1.25 (HP)	UC	0.86	7.5	20.6	105		
	-very stiff below 6 feet				2.75 (HP)							
	8.0											
	SANDY LEAN CLAY (CL), tan and light gray, stiff	1	V		1.75 (HP)							
aa		10-			1							
	11.0 <u>SANDY SILTY CLAY (CL-ML)</u> , reddish brown and light gray, medium stiff to stiff -low strain failure at 11 feet	1			1.00 (HP)	UC	0.79	3.7	17.9	115	22-16-6	
		-	V							-		
ų,	14.0 <u>CLAYEY SAND (SC)</u> , reddish brown and light gray,	-										
Ŋ	medium dense	15_		M	5-7-9 N=16				21.5			18
1	16.0 LEAN CLAY (CL), brown, stiff											-
	20.0 FAT CLAY (CH), brown, stiff to very stiff, with sand seams	20			1.75 (HP)							
					-							
		-			2.00 (HP)							
	24.0 Boring Terminated at 24 Feet							-		-		
ļ												
proce	xploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.		2	ZI	Level Observation First encountered After 15 minutes	ons					Drill Rig ATV Hammer Typ	
Notes	ion Reference: Elevations based on Google Earth		A. 0'	dvan	cement Method	uger					Rope and Cat Driller M. Billiot Logged by	head
	ACTIVITY OF A CONTRACT OF A				Rotary Wash						B. Alexander Boring Start 08-02-2023	ed
					backfilled with aug	er cutti	ngs upor	n comp	letion.		Boring Comp 08-02-2023	leted

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220 Prater Rd Sulphur, LA



6c	Location: See Exploration Plan		IS OF	be		St	rength 1	Test	(9)	-£	Atterberg Limits	
Graphic Log	Latitude: 30.1824° Longitude: -93.1565°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines
1/2 31	Depth (Ft.) 0.4 Approximately 5-inches of topsoil		-	Т			0.0	177				-
Ц	1.0 SILTY CLAY (CL-ML), brown					-						
	LEAN CLAY (CL), brown and light gray, hard 2.0				4.50 (HP)							
	FAT CLAY (CH), tan and light gray, stiff to very stiff, slickensided	-			1.75 (HP)	UC	1.50	13.6	21.5	106	63-18-45	
		5-			2.00 (HP)							
	8.0		V		1.50 (HP)							
Ø	SANDY LEAN CLAY (CL), reddish brown and light gray, stiff		-		1. 100 10.000							1
	-low strain failure at 8 feet	10-			1.75 (HP)	UC	1.24	3.5	15.8	114	29-14-15	
#	11.0 POORLY GRADED SAND WITH SILT (SP-SM), reddish	-										
	brown, medium dense		V	X	7-7-8 N=15				23.5			9
	14.0 <u>FAT CLAY (CH)</u> , brown, medium stiff to stiff, with sand layers	15-		T	1.00 (HP)				29.5			99
		- 1 - 1										-
	-very stiff below 18 feet	20-			2.00 (HP)							
	24.0	-			2.50 (HP)							
	Boring Terminated at 24 Feet											
oce	xploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.		N N	ZF	Level Observation irst encountered After 15 minutes	ons					Drill Rig ATV Hammer Typ Rope and Cat	ie head
otes evat	s ion Reference: Elevations based on Google Earth		0'-	13'C	ement Method ontinuous Flight A Rotary Wash	uger					Driller M. Billiot Logged by B. Alexander	
			At	ando	onment Method backfilled with aug	jer cutti	ngs upor	n comp	letion.		B. Alexander Boring Start 08-04-2023 Boring Comp	

Facilities | Environmental | Geotechnical | Materials

Boring Completed 08-04-2023





-	Location: See Exploration Plan				A	St	rength ⁻	Test		_	Atterberg	
Graphic Log	Latitude: 30.1814° Longitude: -93.1560°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)		Water Content (%)	Dry Unit Weight (pcf)	Limits LL-PL-PI	Percent Fines
1. 3	Depth (Ft.) 0.4 Approximately 5-inches of topsoil	-	-	T		-			-			-
	1.0 SILTY CLAY (CL-ML), brown	1										
	LEAN CLAY (CL) , brown and light gray, hard, with silt 2.0 seams and pockets	1			4.50 (HP)							
	FAT CLAY (CH), gray and tan, very stiff, slickensided				2.00 (HP)	UC	3.22	14.6	18.8	109	68-14-54	
	-with ferrous nodules below 4 feet.	5-			2.00 (HP)							
	LEAN CLAY WITH SAND (CL), light gray and tan, very stiff 8.0	-			2.50 (HP)							
	SANDY LEAN CLAY (CL), reddish brown and light gray, stiff	10-			1.25 (HP)	UC	1.64	5.5	17.5	111		
	13.0	1 1		I	1.25 (HP)							
Ï	CLAYEY SAND (SC), reddish brown and light gray, medium dense				1610							
U	16.0	15-		Х	8-7-8 N=15							
	FAT CLAY (CH), brown, stiff to very stiff, with sand seams											
	-low strain failure at 18 feet				2.00 (HP)	uc	1.22	3	25.2	96	53-19-34	
		20-										
	24.0	-			1.75 (HP)		_					
	Boring Terminated at 24 Feet		1									
	xploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.		22	ZF	Level Observation First encountered After 15 minutes	ons					Drill Rig ATV Hammer Typ Rope and Cat Driller	be head
Note Eleva	s tion Reference: Elevations based on Google Earth		A 0' 1:	dvanc -13' C 3'-24'	cement Method continuous Flight A Rotary Wash	uger					M.Billiot Logged by B. Alexander	

Abandonment Method Boring backfilled with auger cuttings upon completion.

Boring Started 08-02-2023

Boring Completed 08-02-2023





Location: See Exploration Plan	3	/el	/be	tt u	St	rength 7	Test	(%)	it cf	Atterberg Limits	4
Latitude: 30.1808° Longitude: -93.1558°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil			\mathbf{T}			0.4					-
1.0 SILTY CLAY (CL-ML), brown, hard	-										
FAT CLAY (CH), light gray and brown, very stiff to hard -slickensided below 2 feet				4.50 (HP)						74-18-56	
	-			3.75 (HP)							
	5-			3.25 (HP)	UC	2.44	15	15.9	115	50-13-37	
		V		3.50 (HP)							
	10-			2.50 (HP)							
11.0	10										
CLAYEY SAND (SC), tan and light gray, loose		∇	X	3-4-5 N=9				16.7			41
-medium dense below 14.5 feet	15-			5-8-12	_			T			
	-		Ą	N=20							
18.0		1									
SANDY LEAN CLAY (CL), brown, stiff, with sand seams				1.75 (HP)							
	20-		1								
22.0 <u>LEAN CLAY (CL)</u> , brown, medium stiff to stiff, -with sand seams -low strain failure at 22 feet		Ì.		3.00 (HP)	UC	0.67	4.4	24.4	100		
24.0 Boring Terminated at 24 Feet											
Exploration and Testing Procedures for a description of field and laboratory		v	ater	Level Observatio	ons					Drill Rig	
edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		2		irst encountered After 15 minutes						ATV Hammer Typ Rope and Catl	
es ation Reference: Elevations based on Google Earth		0'-	13'C	ement Method ontinuous Flight A Rotary Wash	uger					Driller M. Billiot Logged by B. Alexander	
				onment Method backfilled with aug	er cutti	ngs upor	n comp	letion.		Boring Start 08-02-2023 Boring Comp 08-02-2023	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053

Location: See Exploration Plan	-	- 0	g		St	rength 1	Test		G	Atterberg Limits	
Latitude: 30.1824° Longitude: -93.1560°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3_ Approximately 4-inches of topsoil		-	T				-	-			+
1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), tan and light gray, hard, with silt seams	÷	19	-	4.50 (HP)	-						
2.0 and pockets FAT CLAY (CH), tan and light gray, stiff to very stiff	4			4.50 (HP)	-	_	-				
				2.00 (HP)	uc	1.81	15	19.8	113	53-15-38	
	5-			2.50 (HP)							
-with trace sand below 6 feet		∇		2.00 (HP)							
8.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, stiff to very stiff	1			2.25 (HP)	uc	0.99	8.5	20.4	106		
11.0 CLAYEY SAND (SC), reddish brown, medium dense	10-		1								
13.0		∇	X	6-7-6 N=13							
FAT CLAY (CH), reddish brown, stiff, with sand layers											
16.0	15-			1.75 (HP)							
LEAN CLAY (CL), brown, stiff to very stiff, with silt seams				lan di							
		Ĩ		2.00 (HP)	UC	1.04	7.8	28.4	94	40-19-21	1
	20-										
22.0 FAT CLAY (CH), brown and gray, stiff				1							
				1,75 (HP)							
-dark gray below 25 feet	25-										
ploration and Testing Procedures for a description of field and laboratory lures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.		w V	Z F	Level Observation irst encountered After 15 minutes	ons	1.				Drill Rig ATV Hammer Typ Rope and Cath	le
										Driller	led
ion Reference: Elevations based on Google Earth				ement Method	uger					M. Billiot	

Abandonment Method Boring backfilled with bentonite grout upon completion

Boring Started 08-04-2023

Boring Completed 08-04-2023

erracon

220 Prater Rd

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



бо	Location: See Exploration Plan	0	el 1s	be	Ħ	St	rength T	est	(%	t cf)	Atterberg Limits	
Graphic Log	Latitude: 30.1824° Longitude: -93.1560°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
	Depth (Ft.) <u>FAT CLAY (CH)</u> , brown and gray, stiff (continued)					-	30	ŝ		-	_	
		-		-								
		1			1.50 (HP)							
	30.0 Boring Terminated at 30 Feet	- 30-				1			-		-	
e Er	ploration and Testing Procedures for a description of field and laborate	ory			Level Observatio	ons					Drill Rig	
	xploration and Testing Procedures for a description of field and laborate lures used and additional data (If any). upporting Information for explanation of symbols and abbreviations.	סרע		ZF	Level Observatio First encountered After 15 minutes	ins					ATV	e
ee Si	upporting Information for explanation of symbols and abbreviations.	Dry	Z	Z F Z	First encountered After 15 minutes	ons					ATV Hammer Typ Rope and Cath Driller	e read
otes	upporting Information for explanation of symbols and abbreviations.	עזק	Ac 0':-	Z F	First encountered						ATV Hammer Typ Rope and Cath Driller M. Billiot	e head
otes	upporting Information for explanation of symbols and abbreviations.	עזק	Ac 0'- 13	Z F Z -13' C 3'-30'	First encountered After 15 minutes Cement Method Continuous Flight A						ATV Hammer Typ Rope and Cath Driller	

Terracon Project No. EU235053

ierracon 220 Prater Rd Sulphur, LA

Location: See Exploration Plan	2	el ns	ed	ti	St	rength T	Test	(%)	c) t	Atterberg Limits	
Latitude: 30.1824° Longitude: -93.1550°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 4-inches of topsoil		-	+	_		0.0		-			-
1.0 SILTY CLAY (CL-ML), brown, hard											
LEAN CLAY (CL), brown and light gray, very stiff to hard, 2.0 with silt seams				4.50 (HP)	UC	2.05	3.5	12.6	107	40-15-25	
FAT CLAY (CH), tan and light gray, very stiff			Ī	3.75 (HP)							
	_			5.15 ()							
	5-			2.50 (HP)							
-with trace sand below 6 feet	-	V		3.00 (HP)	υc	2.16	14.8	20.0	110		
8.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, very stiff	-	Ì		2.25 (HP)							
11.0 CLAYEY SAND (SC), reddish brown, medium dense	10-										
<u>CLATET SALE (SC)</u> , reduisi brown, median dense	-		X	7-7-9 N=16				20.7			3
14.0											
FAT CLAY (CH), brown, stiff -with sand layers to 16 feet	15-			1.25 (HP)							
-with silt seams from 18 feet to 20 feet	1 1 1	1		1.50 (HP)							
	20-										
-brown and gray from 23 feet to 28 feet											
25.0	-			2.25 (HP)							
LEAN CLAY (CL), dark gray, stiff	25-										
Exploration and Testing Procedures for a description of field and laboratory	_	w	ater	Level Observatio	ons					Drill Rig	
edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		V	-	irst encountered After 15 minutes						ATV Hammer Typ Rope and Cat	head
										Driller	
s tion Reference: Elevations based on Google Earth		0'-	13'C	ement Method ontinuous Flight A Rotary Wash	uger					M. Billiot Logged by B. Alexander	
				nment Method backfilled with ben	itonite ç	prout upo	on com	detion		Boring Start 08-04-2023 Boring Comp	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



In Cocation: See Exploration Plan Streng Latitude: 30.1824° Longitude: -93.1550° (1) Depth (Ft.) Image: Streng of the streng of	Strength Ital (tsf) Strain (%) Mater Content (%)	Dry Unit Weight (pcf)	tterberg Limits	Percent
Depth (Ft.) 8 LEAN CLAY (CL), dark gray, stiff (continued) 1.25 (HP) -dark gray below 28 feet 1.25 (HP) 30.0 30	<u>v</u> <u>v</u>			
-dark gray below 28 feet				
30.0 - 1.25 (HP) 30.0 - 30				
See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any). See Supporting Information for explanation of symbols and abbreviations. See Supporting Information for explanation of symbols and abbreviations.		ATV	ill Rig √ mmer Type	
		Rop	pe and Cathe	ad
Iotes Advancement Method Nevation Reference: Elevations based on Google Earth 0 ¹ -13 ¹ Continuous Flight Auger 13 ¹ -30 ¹ Rotary Wash		М.	Billiot	
levation kererence: Elevations based on Google Earth 13'-30' Rotary Wash			gged by Alexander ring Started	d
Abandonment Method Boring backfilled with bentonite grout		1	ring Started -04-2023 ring Comple	



Location: See Exploration Plan	4 1	-	ls l	be	Ħ.,	St	rength 7	Test	(%)	£t	Atterberg Limits	
Latitude: 30.1810° Longitude: -93.1540°		Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.)			-	-	_	-	90	N.	-	_		-
1.0 SILTY CLAY (CL-ML), brown, hard		1			+							
LEAN CLAY (CL), brown and light gray, 2.0	with silt layers	1			4.50 (HP)							
FAT CLAY (CH), reddish brown and tan -with ferrous nodules to 4 feet	, stiff to very stiff	-			1.75 (HP)	UC	2.08	15	18.6	109	56-17-39	
-tan and light gray, slickensided below 4	feet				1.75 (HP)							
					3.50 (HP)	υc	2.31	13.3	18.9	112		
8.0 SANDY LEAN CLAY (CL), reddish brow	n and light gray.	-	V			-				_		
stiff					1.75 (HP)							
11.0		10										
CLAYEY SAND (SC), gray and tan, loos	e	ĩ										
		1 . 1	V	X	3-4-4 N=8							
and the barrier of the state of the state of the	6-14	4										
-reddish brown, medium dense below 14		15-		X	5-7-10 N=17							
		1										
18.0 FAT CLAY (CH), brown, stiff to very stif	f	-		-								-
		-			1.50 (HP)				25.8			8
-with sand seams to 25 feet		20-										
		20-			_				1			
		1.7										
		-	- 1									
		-			3.00 (HP)							
-dark gray below 25 feet	13	25-	1			-						
-dark gray below 25 feet												
		1	0.1									
4		-				_						
Exploration and Testing Procedures for a description educes used and additional data (If any).	of field and laboratory		W		Level Observation	ons					Drill Rig	
Supporting Information for explanation of symbols an			T T	-	After 15 minutes						Hammer Typ	e
			1								Rope and Cath	head
es			Ad	vanc	ement Method						Driller M. Billiot	
			0'-	13'C	ontinuous Flight A Rotary Wash	uger					Logged by	
ation Reference: Elevations based on Google Earth				50	THE TYPE						B. Alexander	
ation Reference: Elevations based on Google Earth					and the second							
ation Reference: Elevations based on Google Earth			Ab	ando	onment Method backfilled with ben						Boring Starte 08-03-2023	ed

Terracon Project No. EU235053



50	Location: See Exploration Plan	0	el 1s	be	#	St	rength T	est	(%	÷t	Atterberg Limits	
Graphic Log	Latitude: 30.1810° Longitude: -93.1540°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
77	Depth (Ft.) FAT CLAY (CH), brown, stiff to very stiff (continued)					-	Sø	ŝ	-			-
		-		_								
		-			3.75 (HP)							
	30.0 Boring Terminated at 30 Feet	- 30-	-			-		-	-	_		-
e Ex	ploration and Testing Procedures for a description of field and laborator ures used and additional data (If any).				Level Observatio	ns					Drill Rig ATV	
	pporting Information for explanation of symbols and abbreviations.			-	After 15 minutes						Hammer Typ Rope and Catl	e lead
			-								Driller M. Billiot	
					cement Method Continuous Flight A	Inor						
otes evati	on Reference: Elevations based on Google Earth		13	3'-30'	Rotary Wash	uge					Logged by B. Alexander	

Terracon Project No. EU235053

Boring Log No. B-14

bo	Location: See Exploration Plan		la st	be	Ŧ	St	rength ⁻	Test	(9)	÷,	Atterberg Limits	
Graphic Log	Latitude: 30.1820° Longitude: -93.1546°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines
NIX 5	Depth (Ft.) 0.3_Approximately 4-inches of topsoil			Т		-	0.0	01				-
	1.0 SILTY CLAY (CL-ML), brown	1 -			**				9.3	_		
	SANDY LEAN CLAY (CL), brown and light gray, medium 2.0 stiff to stiff				2.25 (HP)	UC	0.87	5.7	19.7	108	37-18-19	
	FAT CLAY (CH), reddish brown and light gray, stiff to very stiff				2.50 (HP)							
	-tan and light gray with trace sand below 4 feet	5-			2.50 (HP)	UC	1.68	14.3	18.7	111		
	-with ferrous nodules from 6 feet to 8 feet				2.00 (HP)							
	8.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, medium stiff to stiff	10-	V		1.00 (HP)							
	11.0 <u>CLAYEY SAND (SC)</u> , reddish brown and light gray, medium dense	10-										
Ű			V	Х	4-5-6 N=11							
	14.0 <u>SANDY LEAN CLAY (CL)</u> , brown, very stiff	15-			2.50 (HP)							
	18.0 LEAN CLAY (CL), brown, stiff				1.50 (HP)	υc	1.16	7.8	26.1	97		
	22.0 FAT CLAY (CH), brown, very stiff, -with sand seams				2.25 (HP)							
	24.0 Boring Terminated at 24 Feet											
proce	Exploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		м 44 М	Z	FLevel Observation First encountered After 15 minutes	ons					Drill Rig ATV Hammer Typ Rope and Cat Driller	
Note: Eleva	s tion Reference: Elevations based on Google Earth		0'- 13 Al	-13' (3'-24'	cement Method Continuous Flight A Rotary Wash						M. Billiot Logged by B. Alexander Boring Start 08-03-2023	ed
					backfilled with aug	ler cutt	ngs upor	n compl	letion.		Boring Comp 08-03-2023	leted

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220 Prater Rd Sulphur, LA

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



	ation: See Exploration Plan	ţ.	vel	ype	s st	St	rength ⁻		(%)	it of	Atterberg Limits	t.
Lati	itude: 30.1809° Longitude: -93.1562°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Dep	oth (Ft.) _ Approximately 4-inches of topsoil						90	01				-
	SILTY CLAY (CL-ML), brown, hard	-				-						
2.0	LEAN CLAY (CL), brown and light gray, very stiff				4.50 (HP)	UC	3.51	2.6	8.0	109	28-17-11	
	FAT CLAY (CH), brown and gray, stiff to very stiff, slickensided	-			2.00 (HP)							
		5-			1.50 (HP)	υc	1.79	13.3	18.0	109		
8.0		-			2.25 (HP)							
0,0	SANDY LEAN CLAY (CL), tan and light gray, medium stiff to stiff	10-	V		1.00 (HP)							
11.0	CLAYEY SAND (SC), reddish brown and gray, loose			\vee	3-4-4	-						
8	-medium dense below 13 feet	-	V	\wedge	N=8							
		-		X	7-7-10 N=17							
15.0	Boring Terminated at 15 Feet	15-	-			-	-					-
			1 I I			1						1
Explor	ration and Testing Procedures for a description of field and laboratory s used and additional data (If any).				Level Observatio	DRS					Drill Rig ATV	
edures	ration and Testing Procedures for a description of field and laboratory s used and additional data (If any). rting Information for explanation of symbols and abbreviations.			ZF	and the second second second second	ons						
cedures Suppo	s used and additional data (If any).		Z Z Ad	Z F Z	First encountered						ATV Hammer Typ	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	0	el	/pe	¥.,	St	rength T	est	(%)	"F	Limits	
Location: See Exploration Plan Latitude: 30.1832° Longitude: -93.1545°	Depth (Ft.)	Water Level Observations	Sample Type	Field Text Results	Test Type	Compressive Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (cf)	LL-PL-PI	Percent
Depth (Ft.)			-		1	8"	S		_		-
1.0 SILTY CLAY (CL-ML), brown and light gray, hard	1 -							7.9			
2.0				4.50 (HP)				14.3			
FAT CLAY (CH), brown, hard				4.50 (HP)				20.5		65-15-50	
4.0				3.00 (HP)				18.9			
LEAN CLAY (CL), tan and light gray, very stiff				2.25 (HP)				17.8		48-14-34	1
	5-			2.50 (HP)				18.4			1
	1			2.50 (HP)				21.7			
	1	V		2.25 (HP)				23.3		46-16-30	1
8.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, medium stiff to very stiff				1.00 (HP)				21.8			1
				1.00 (HP)				22.3		27-14-13	
	10-			4.00 (HP)				19.5			1
11.0 CLAYEY SAND (SC), reddish brown and light gray, loose			X	4-5-4 N=9				19.7			4
-medium dense below 12.5 feet	-	V	$\left< \right>$	7-9-9 N=18							-
	-		$\left(\right)$	6-8-9							-
15.5	15-		\wedge	N=17			-	21.1			2
I Exploration and Testing Procedures for a description of field and laboratory redures used and additional data (If any).	6			Level Observatio	ns					Drill Rig	1
Supporting Information for explanation of symbols and abbreviations. es ation Reference: Elevations based on Google Earth			Z	First encountered After 15 minutes cement Method Continuous Flight A	uger					Hammer Typ Rope and Cath Driller M. Billiot Logged by B. Alexander	ie head
				onment Method backfilled with aug	er cutti	ngs Upon	comp	letion.		Boring Starts 08-02-2023 Boring Comp 08-02-2023	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Boring Log No. B-17

Location: See Exploration Plan	G	/el	Ape	ti n	St	rength 1	est	(%)	£	Limits	+
Latitude: 30.1831° Longitude: -93.1534°	Depth (Ft.)	Water Level Observations	Sample Type	Field Text Results	Test Type	Compressive Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (cf)	LL-PL-PI	Percent
Depth (Ft.) 0.3_Approximately 4-inches	-		-		15	8"	Ś		_		-
1.0 SILTY CLAY (CL-ML), brown, hard				*				3.8			
LEAN CLAY (CL), brown and light gray, hard 2.0				4.50 (HP)				8.2		34-14-20	
FAT CLAY (CH), tan and light gray, very stiff, slickensided				3.00 (HP)				16.8			
4.0				2.50 (HP)				17.0			
LEAN CLAY (CL), tan and light gray, stiff to very stiff				1.50 (HP)				20.1		46-16-30	1
	5 -			1.25 (HP)				20.6			1
	1			2.25 (HP)				22.7			
8.0				2.00 (HP)				19.4		47-15-32	1
SANDY SILTY CLAY (CL-ML), reddish brown and tan, soft to medium stiff		1		1.50 (T)				23.8			1
				1.60 (T)				25.5			
11.0	10-			1.00 (HP)				18.7		23-17-6	1
<u>CLAYEY SAND (SC)</u> , tan and light gray, loose to medium dense	1		X	4-4-4 N=8				18.7			3
14.0			X	5-7-8 N=15				23.6			2
FAT CLAY (CH), brown, very stiff	15-			2.75 (HP)				26.5			

Boring Completed 08-03-2023

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



	2	vel	ype	ti s	St	rength T		(%)	<u>≞</u> €	Limits	-
Latitude: 30.1826° Longitude: -93.1533°	Depth (Ft.)	Water Level Observations	Sample Type	Field Text Results	Test Type	Compressive Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (cf)	LL-PL-PI	Percent
Depth (Ft.)				_	5	8"	ŝ		1		
0.3 Approximately 4-inches of topsoil 1.0 SILTY CLAY (CL-ML), brown, hard	1							11.4			
SANDY LEAN CLAY (CL), brown, stiff, with silt seams	1 -	1	Ż	1.50 (HP)				12.7		25-16-9	1
2.0 FAT CLAY (CH), brown and tan, stiff	-			1.50 (HP)				21.1			1
-tan and light gray below 3 feet 4.0	-			1.75 (HP)				17.2			
LEAN CLAY (CL), tan and light gray, stiff to very stiff				2.00 (HP)				16.7			
	5-			2.25 (HP)				18.8		47-15-32	Ľ
				1.75 (HP)				19.5			ħ
		577		2.50 (HP)				16.2			
9.0	-	V		1.25 (HP)				17.1		40-17-23	1
SANDY LEAN CLAY (CL), reddish brown and light gray, stiff to very stiff				2.00 (HP)				18.5			
11.0	10-	i		1.00 (HP)				18.4			5
CLAYEY SAND (SC), reddish brown, medium dense			X	4-5-6 N=11				1			
			()	3-6-5							
			A	N=11				21,4			2
	15-	∇	X	6-9-9 N=18							
15.5 Boring Terminated at 15.5 Feet		1	$\langle \cdot \rangle$	2.32	-		-				+
Exploration and Testing Procedures for a description of field and laboratory adures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		ZZ	Z F	Level Observatio First encountered After 15 minutes						Drill Rig ATV Hammer Typ Rope and Cat Driller M. Billiot Logged by B. Alexander	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan		le lus	ed/	tt u	St	rength T	est	(%)	ef.	Atterberg Limits	4
Location: See Exploration Plan Latitude: 30.1829° Longitude: -93.1555°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil		-	\mathbf{T}			0.0	17				-
1.0 SILTY CLAY (CL-ML), brown and light gray	-		1	-7				6.2		-	
LEAN CLAY (CL), brown and light gray, hard				4.50 (HP)				9.4		46-15-31	
FAT CLAY (CH), gray and tan, very stiff	-			2.75 (HP)				18.6			
-slickensided below 4 feet	5-			2.00 (HP)							
6.0 <u>SANDY LEAN CLAY (CL)</u> , tan and light gray, stiff to very stiff	-			2.75 (HP)							
10.0	1-1-			1.50 (HP)							
Exploration and Testing Procedures for a description of field and laboratory adures used and additional data (If any).				Level Observatio	0.5					Drill Rig ATV	
				Level Observatio	ns					ATV Hammer Typ	e
					0.5					ATV	head
Exploration and Testing Procedures for a description of field and laboratory edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		No	vanc							ATV Hammer Typ Rope and Cath Driller M. Billiot	ee mead
Supporting Information for explanation of symbols and abbreviations.		No	vanc	water observed						ATV Hammer Typ Rope and Cath Driller	head

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	2	le lus	/be	ti u	St	rength T	est	(%)	it cf)	Atterberg Limits	+
Latitude: 30.1824° Longitude: -93.1555°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil			\mathbf{T}			Q.e		15.0			-
SILTY CLAY (CL-ML), brown, very stiff	-							1			
2.0 FAT CLAY (CH) tap and gray stiff to very stiff	-			2.50 (HP)				18.8		-	
FAT CLAY (CH), tan and gray, stiff to very stiff, slickensided				1.75 (HP)				19.3		50-18-32	
	5-			2.00 (HP)							
8.0				2.50 (HP)							
8.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, medium stiff	-			0.75 (HP)							
Evaluation and Testing Procedures for a description of field and lot states			ater	Level Observation	DS					Drill Big	
				Level Observatio water observed	ns					Drill Rig ATV Hammer Typ Rope and Cath	e nead
Exploration and Testing Procedures for a description of field and laboratory edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		N	o free							ATV Hammer Typ	e

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	2	lei ns	/be	tt u	_	rength T	est	(%)	e,	Atterberg Limits	+
Location: See Exploration Plan Latitude: 30.1819° Longitude: -93.1555°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) ³⁰ 0.3 Approximately 4-inches of topsoil			-		-	90	•,				-
1.0 SILTY CLAY (CL-ML), brown, hard	1 _							51.6			
LEAN CLAY (CL), brown and light gray, stiff 2.0				1.50 (HP)				19.6			
FAT CLAY (CH), reddish brown and gray, very stiff				3.00 (HP)				26.4		67-18-49	
6.0	5-			3.50 (HP)				18.3		52-18-34	
5.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, stiff to very stiff	-			2.50 (HP)							
10.0	- 10-			1.75 (HP)							
									1		
e Exploration and Testing Procedures for a description of field and laboratory cedures used and additional data (If any). a Supporting Information for explanation of symbols and abbreviations. tes vation Reference: Elevations based on Google Earth		No	o free	Level Observation water observed coment Method continuous Flight A						Drill Rig ATV Hammer Typ Rope and Cath Driller M. Billiot Logged by B. Alexander Boring Starte	iead

Terracon Project No. EU235053

Boring Log No. B-22

Location: See Exploration Plan Latitude: 30.1813° Longtude: -93.1553° Depth (ft.) 0.2.Approximately 3-inches of topsoil 1. SLITY CLAY (CL,L), brown and light gray, hard -gray and tan, with ferrous nodules below 4 feet 5- 1.00 (HP) 1.00 (HP) 1.0	Location: See Exploration Plan	0	le su	edu	ti	St	rength T	est	(%)	Ð,	Atterberg Limits	
Depth (Ft.) 0.3 _ Approximately 3-inches of topsoil 0.3 _ Approximately 3-inches of topsoil - 1.0 SILTY CLAY (CL-ML), brown - LEAN CLAY (CL), brown and light gray, hard - 2.0 4.50 (HP) FAT CLAY (CH), brown and light gray, hard - -gray and tan, with ferrous nodules below 4 feet 5- 5- 1.75 (HP) 1.00 (HP) 19.4 8.0 - SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff - 10.0 -	Latitude: 30.1813º Longitude: -93.1553º	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Fest Type	ompressiv Strength (tsf)	strain (%)	Water Content (Dry Unit Weight (pcf)	1960	Percent
1.0 SILTY CLAY (CL-ML), brown LEAN CLAY (CL), brown and light gray, hard 2.0 FAT CLAY (CH), brown and light gray, hard -gray and tan, with ferrous nodules below 4 feet 5 1.75 (HP) 8.0 SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff 10.0	Depth (Ft.)		-	-	_		90	w.	1	_	_	
LEAN CLAY (CL), brown and light gray, hard 4.50 (HP) FAT CLAY (CH), brown and light gray, hard 4.50 (HP) -gray and tan, with ferrous nodules below 4 feet 4.50 (HP) 5 1.75 (HP) 8.0 1.00 (HP) 8.0 2.25 (HP)		1							6.0			
FAT CLAY (CH), brown and light gray, hard 4.50 (HP) -gray and tan, with ferrous nodules below 4 feet 5 5 1.75 (HP) 8.0 1.00 (HP) SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff 2.25 (HP)	LEAN CLAY (CL), brown and light gray, hard				4.50 (HP)				11.4			
-gray and tan, with ferrous nodules below 4 feet 5 - 1.75 (HP) 8.0 SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff 10.0		-										
8.0 1.75 (HP) SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff 1.00 (HP) 10.0 2.25 (HP)		-			4.50 (HP)				14.9			
8.0 SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff 2.25 (HP)	-gray and tan, with ferrous nodules below 4 feet	5-			1.75 (HP)				19.4	107	56-15-41	
SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff 2.25 (HP)	8.0	-			1.00 (HP)							
	SANDY LEAN CLAY (CL), reddish brown and light gray, very stiff	-			2.25 (HP)							
		1-									-	
0'-10' Continuous Flight Auger	Exploration and Testing Procedures for a description of field and laboratory sources used and additional data (If any).		No	vand	Level Observation water observed						Drill Rig ATV Hammer Typ Rope and Cath Driller M. Billiot	e

Facilities | Environmental | Geotechnical | Materials

Boring Completed 08-03-2023

Boring backfilled with auger cuttings upon completion.

erracon

220 Prater Rd Sulphur, LA

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan		lei ns	ed/	tt in	St	rength T	Test	(%)	it cf)	Atterberg Limits	-+-
Latitude: 30.1806° Longitude: -93.1552°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 10.3 Approximately 4-inches of topsoil						Q.¢	51	_	-		-
1.0 SILTY CLAY (CL-ML), brown, hard	1 -			-7				4.8			
LEAN CLAY (CL), brown, hard, with ferrous nodules 2.0				4.50 (HP)				16.5			
FAT CLAY (CH), tan and light gray, hard	-			4.50 (HP)				20.1		75-14-61	
-light gray and tan, slickensided below 4 feet	5-			3.25 (HP)				18.4			
	-			2.25 (HP)				18.8			
10.0	- 10-			2.75 (HP)							
Exploration and Tasting Procedures for a description of field and laborato dures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.	γ			Level Observatio	ns					Drill Rig ATV Hammer Typ Rope and Cath Driller	ie Teac

Terracon Project No. EU235053

Boring Log No. B-24

50	Location: See Exploration Plan	0	la IS	be	e.	St	rength T	est	(9)	e,	Atterberg Limits	
Graphic Log	Latitude: 30.1828° Longitude: -93.1541°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines
	Depth (Ft.) 0.3 Approximately 3-inches of topsoil			T			0.4	1.1.2	4.9		22-15-7	
	1.0 SILTY CLAY (CL-ML), brown, hard SANDY LEAN CLAY (CL), brown and light gray, hard	-		4							22-13-7	
	2.0 LEAN CLAY (CL), tan and light gray, stiff to very stiff	-		_	4.50 (HP)				9.9			
					2.00 (HP)				17.5			
	6.0	5-			2.25 (HP)							
	FAT CLAY (CH), tan and light gray, very stiff, with trace sand	-			2.50 (HP)							
	8.0 SANDY LEAN CLAY (CL), reddish brown, medium stiff to stiff				1.00 (HP)							
(11)	10.0 Boring Terminated at 10 Feet	1 -				-	_	-	-			-

Boring Completed 08-03-2023

Ierracon

220 Prater Rd Sulphur, LA

Terracon Project No. EU235053

Boring Log No. B-25

Cocation: See Exploration Plan	~	el	ed	ti	St	rength T	est	(%)	÷t	Atterberg Limits	
Location: See Exploration Plan Latitude: 30.1824° Longitude: -93.1537° E	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.)	-		Т			0.0	118	1.1.2			-
1.0 SILTY CLAY (CL-ML), brown, hard				-7				11.2			
LEAN CLAY (CL), brown and tan, stiff 2.0				1.50 (HP)				18.6			
FAT CLAY (CH), light gray and tan, stiff to very stiff, slickensided				2.25 (HP)				18.5		51-15-36	
6.0	5-			1.75 (HP)	1			18.0			
SANDY LEAN CLAY (CL), light gray and tan, very stiff	-			2.25 (HP)							
				1.50 (HP)							
10.0 Boring Terminated at 10 Feet	- 10-	-						-			
Purplements and Testing Procedures for a description of field and laboration		w	ater	Level Observatio	15		lł,			Drill Rig	
e Exploration and Testing Procedures for a description of field and laboraton ocedures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.				a water observed						ATV Hammer Typ Rope and Catl Driller	e
											head
otes evation Reference: Elevations based on Google Earth				cement. Method Continuous Flight Ai	uger					M.Billiot Logged by B. Alexander Boring Starte	

Boring Completed 08-03-2023





Location: See Exploration Plan	3	le us	ed/	tt	St	rength T	est	(%)	it C	Atterberg Limits	+
Location: See Exploration Plan Latitude: 30.1824° Longitude: -93.1542°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 30.3 Approximately 4-inches of topsoil			-		1	90	Ś			-	-
1.0 SILTY CLAY (CL-ML), brown, hard								10.6			
LEAN CLAY (CL), brown, stiff to very stiff, with silt seams 2.0				2.00 (HP)				18.8			
FAT CLAY (CH), light gray and tan, stiff, slickensided with ferrous nodules	1			1.75 (HP)				18.5		60-16-44	
gray and tan from 4 feet to 6 feet	- 5-			1.50 (HP)							
tan and gray from 6 feet to 8 feet	-			3 F0 (HD)							
8.0 SANDY LEAN CLAY (CL), brown and reddish brown, stiff				2.50 (HP)							
SANDY LEAN CLAY (CL), brown and reddish brown, stiff to very stiff	-			2.00 (HP)							
Boring Terminated at 10 Feet	1 -									-	
Exploration and Testing Procedures for a description of field and laboratory edures used and additional data (If any).				Level Observatio	ns					Drill Rig ATV	
edures used and additional data (If any).					ns					ATV Hammer Typ	e gead
edures used and additional data (If any).					ns					ATV	e head
adures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		No	vanc	water observed						ATV Hammer Typ Rope and Catl Driller M. Billiot	e
edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations. as		No	vanc	water observed						ATV Hammer Typ Rope and Catl Driller	e
edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations. as		Nc Ad 0'-	vanc 10' C	ewater observed Sement Method Continuous Flight A						ATV Hammer Typ Rope and Catl Driller M. Billiot Logged by B. Alexander Boring Start	head
Exploration and Testing Procedures for a description of field and laboratory edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		Nd Ad 0'-	vanc 10°C	water observed	uger	ngs Upon	compl	letion.		ATV Hammer Typ Rope and Cati Driller M. Billiot Logged by B. Alexander	ed



Location: See Exploration Plan	0	el ns	edu	ti	St	rength T	est	(%)	£	Atterberg Limits	4
Latitude: 30.1817° Longitude: -93.1537°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil		-	\mathbf{T}			00				-	-
1.0 SILTY CLAY (CL-ML), brown, hard								12.5			
LEAN CLAY (CL), gray and tan, stiff, with silt seams and 2.0 pockets				1.25 (HP)				20.8			
FAT CLAY (CH), light gray and tan, medium stiff to stiff	-			1.00 (HP)				20.8			
-with trace sand below 4 feet	5-			2.50 (HP)	1						
-with ferrous nodules below 6 feet				3.50 (HP)							
8.0 SANDY LEAN CLAY (CL), light gray and tan, very stiff	4										
10.0	-			3.75 (HP)							
Boring Terminated at 10 Feet	1 -				-			-			-
Exploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any).				Level Observatio	ns					Drill Rig ATV	
Exploration and Tasting Procedures for a description of field and laboratory dures used and additional data (If any).					ns					ATV Hammer Typ	e
dures used and additional data (If any).					ns					ATV Hammer Typ Rope and Catl Driller	e
dures used and additional data (If any). supporting Information for explanation of symbols and abbreviations. s		No	o free							ATV Hammer Typ Rope and Cath Driller M. Billiot	e
dures used and additional data (If any). supporting Information for explanation of symbols and abbreviations.		No	o free	e water observed						ATV Hammer Typ Rope and Cati Driller M. Billiot Logged by B. Alexander	head
dures used and additional data (If any). supporting Information for explanation of symbols and abbreviations. s		Nd 0'- At	vanc 10°C	e water observed	uger					ATV Hammer Typ Rope and Catl Driller M. Billiot Logged by	head

Terracon Project No. EU235053

Location: See Exploration Plan	0	el 1s	be	H	St	rength T	Test	(9)	÷¢	Atterberg Limits	
Location: See Exploration Plan Latitude: 30.1813° Longitude: -93.1535°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.)				_	1	90		-		-	
1.0 SILTY CLAY (CL-ML), brown, hard	-			-7				6.8			
LEAN CLAY (CL), gray and tan, hard, with calcareous 2.0 nodules and silt seams				4.50 (HP)				20.1			
FAT CLAY (CH), tan and gray, stiff to very stiff	1			1.75 (HP)				18.8			
	5-			2.25 (HP)							
	-			1.50 (HP)							
8.0 <u>SANDY LEAN CLAY (CL)</u> , tan and light gray, medium stiff 10.0				0.75 (HP)							
ee Exploration and Testing Procedures for a description of field and laboratory ocedures used and additional data (If any). ee Supporting Information for explanation of symbols and abbreviations.		No	o free	Level Observation water observed						Drill Rig ATV Hammer Typ Rope and Catl Driller M. Billiot	e head
evation Reference: Elevations based on Google Earth		0'-	10' 0	Continuous Flight A	uger					Logged by B. Alexander	





Location: See Exploration Plan	0	el	be	Ħ.,,	St	rength T	est	(%)	Ð.	Atterberg Limits	
Latitude: 30.1816° Longitude: -93.1532°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3_ Approximately 4-inches of topsoil						00					-
1.0 SILTY CLAY (CL-ML), brown, hard	1 -			1				11.3			
LEAN CLAY (CL), brown, very stiff				3.00 (HP)				20.3			
-tan and light gray below 2 feet		-		1.50 (HP)				17.3	109	43-14-29	
4.0 FAT CLAY (CH), tan and light gray, stiff to very stiff	5-			2.00 (HP)							
6.0 SANDY LEAN CLAY (CL), tan and light gray, very stiff	-										
	t			2.50 (HP)							
-reddish brown and light gray below 8 feet				1.00 (HP)							
10.0 Boring Terminated at 10 Feet	- 10-	1							-		+
Exploration and Testing Procedures for a description of field and laborator edures used and additional data (If any).	Y			Level Observatio	ns					Drill Rig ATV	
Exploration and Testing Procedures for a description of field and laborator edures used and additional data (If any).	Y				as					ATV Hammer Typ Rope and Cat	e thead
edures used and additional data (If any).	у	N	lo free dvanc							ATV Hammer Typ	e head

Terracon Project No. EU235053

Boring Log No. B-30

Location: See Exploration Plan	0	la st	be	Ħ.,	St	rength T	est	(%	÷.	Atterberg Limits	
Location: See Exploration Plan Latitude: 30.1813° Longitude: -93.1442°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil			T	_		90			-		-
1.0 SILTY CLAY (CL-ML), brown, hard	1 -							7.3			
LEAN CLAY (CL), brown and light gray, hard, with silt 2.0 seams and pockets and ferrous nodules				4.50 (HP)				15.2			
FAT CLAY (CH), gray and tan, stiff to very stiff				1.75 (HP)				18.7		62-15-47	
	5-	-		2.00 (HP)							
6.0 <u>LEAN CLAY (CL)</u> , reddish brown and gray, medium stiff to stiff	-			1.00 (HP)							
8.0 LEAN CLAY WITH SAND (CL), reddish brown and gray, stiff to very stiff				2.00 (HP)							
10.0 Boring Terminated at 10 Feet	1 -	-		_	-		_	-			-

Boring Completed 08-03-2023

erracon

220 Prater Rd Sulphur, LA

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	3	lei ns	ed/	ts .	St	rength T	est	(%)	c) it	Atterberg Limits	4
Latitude: 30.1806° Longitude: -93.1544°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) ¹⁰ .3_ Approximately 4-inches of topsoil			T			00			-		
1.0 SILTY CLAY (CL-ML), brown, hard	1 -			-7				7.4			
LEAN CLAY (CL), brown and light gray, hard 2.0				4.50 (HP)				17.7		34-14-20	
FAT CLAY (CH), reddish brown and light gray, stiff to very stiff	-			2.75 (HP)				19.0			
-slickensided below 4 feet	5-			1.75 (HP)							
	_			2.75 (HP)							
8.0 <u>SANDY LEAN CLAY (CL)</u> , reddish brown and light gray, medium stiff				0.75 (HP)				23.6			
10.0 Boring Terminated at 10 Feet	1 -					-					
Exploration and Testing Procedures for a description of field and laboratory adures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.				Level Observation a water observed	ns					Drill Rig ATV Hammer Typ	-
										Rope and Cat	
es ation Reference: Elevations based on Google Earth				cement Method Continuous Flight A	uger					M. Billiot Logged by B. Alexander Boring Start	iead

Terracon Project No. EU235053



Location: See Exploration Plan	0	el	be	t	St	rength T	est	(%)	it C	Atterberg Limits	4
Latitude: 30.1809° Longitude: -93.1537°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 4-inches of topsoil		-				0.4		4.5			-
1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), brown and light gray, hard								1			
2.0				4.50 (HP)				12.9			
FAT CLAY (CH), tan and gray, stiff to very stiff, slickensided				2.50 (HP)				20.3	103	57-12-45	
6.0	5-			1.50 (HP)				20.0			
LEAN CLAY (CL), light gray and tan, stiff				1.75 (HP)				16.7			
SANDY LEAN CLAY (CL), reddish brown and gray, medium stiff				0.75 (HP)				18.6			
Boring Terminated at 10 Feet	- 1 -			-							
Exploration and Testing Procedures for a description of field and laboration	Y				ns					Drill Rig ATV	
Exploration and Testing Procedures for a description of field and laborator redures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.	Y			Level Observatio	0.5					ATV Hammer Typ	
	у				0.5					ATV Hammer Typ Rope and Catl	head
	у	N	o free							ATV Hammer Typ	e head

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Cocation: See Exploration Plan	0	el ns	be	ti	St	rength T	est	(%)	e)	Atterberg Limits	4
Location: See Exploration Plan Latitude: 30.1809° Longitude: -93.1533°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil		-	П			90					
1.0 SILTY CLAY (CL-ML), brown				-7				10.3		-	
FAT CLAY (CH), tan and light gray, stiff to very stiff	-			2.50 (HP)				24.5		76-22-54	
	-			1.25 (HP)				18.1			
-with ferrous nodules below 4 feet	5-			2.00 (HP)				18.3			
6.0 SANDY LEAN CLAY (CL), reddish brown and light gray,											
stiff -with ferrous nodules to 8 feet	÷			1.50 (HP)				19.4			
	1			0.50 (HP)							
10.0 Boring Terminated at 10 Feet	10-				-		-	-			
			ater	Level Observatio	ns					Drill Rig ATV	
Exploration and Testing Procedures for a description of field and laboratory cedures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations. tes vation Reference: Elevations based on Google Earth		No Ac	o free	e water observed cement Method Continuous Flight A	uger					Hammer Typ Rope and Cath Driller M. Billiot Logged by B. Alexander Boring Starts	iead

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	0	el ns	edu	ti	St	rength T	est	(%)	£	Atterberg Limits	
Latitude: 30.1825° Longitude: -93.1584°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil	5		Т					3.7			1
1.0 SILTY CLAY (CL-ML), brown LEAN CLAY (CL), brown and light gray, hard	-		ż	4.50 (HP)				6.7		39-24-15	
2.0 FAT CLAY (CH), reddish brown and light gray, very stiff	-										
				3.00 (HP)				22.1	;		
6.0	5-			2.75 (HP)							
xploration and Tasting Procedures for a description of field and laboratory dures used and additional data (If any).				Level Observatio	ns					Drill Rig	
supporting Information for explanation of symbols and abbreviations.		Ad	Ivanc	water observed	ger					ATV Hammer Typ Rope and Cat Driller M. Billiot Logged by	be head
tion Reference: Elevations based on Google Earth		Ab	ando	onment Method backfilled with aug		ings upon	comp	letion.		Boring Start 08-07-2023 Boring Comp 08-07-2023	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



60	Location: See Exploration Plan	0	el ns	be	Ħ.e.	St	rength T	est	(%)	e,	Atterberg Limits	
orapn	Latitude: 30.1830° Longitude: -93.1579°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
	Depth (Ft.) D.3_Approximately 3-inches of topsoil			Т			0.0		9.7			-
	L.0 SILTY CLAY (CL-ML), brown LEAN CLAY (CL), brown and light gray, hard			-	4.50 (HP)				9.6		28-15-13	
	FAT CLAY (CH), tan and light gray, very stiff				4.30 (HP)				9.0		28-13-13	
					2.50 (HP)							
	5.0	5 -			2.25 (HP)							
	Boring Terminated at 6 Feet											
	ploration and Testing Procedures for a description of field and laborator ures used and additional data (If any). pporting Information for explanation of symbols and abbreviations.	y			Level Observatio	ns					Drill Rig ATV Hammer Typ Rope and Catl Driller	ne tieac
			Ac	Ivan	cement Method	oor					Driller M. Billiot Logged by B. Alexander	

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	0	el Is	be	Ħ.,	St	rength T	est	(9)	£t	Atterberg Limits	
Latitude: 30.1827º Longitude: -93.1571º	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 4-inches of topsoil			T					6.8			+
1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), reddish brown and light gray, hard	-				-			-			
2.0 FAT CLAY (CH), reddish brown and light gray, very stiff				4.50 (HP)				18.0			
				2.50 (HP)							
6.0	5-			2.25 (HP)							
Boring Terminated at 6 Feet											
Exploration and Testing Procedures for a description of field and laboratory				Level Observatio	ns					Drill Rig	
Exploration and Testing Procedures for a description of field and laboratory idures used and additional data (If any).				Level Observation	ns					ATV Hammer Typ	De
					ns					ATV Hammer Typ Rope and Cat	be
		No Ac	o free	water observed						ATV Hammer Typ	De
upporting Information for explanation of symbols and abbreviations.		No Ac	o free	water observed						ATV Hammer Typ Rope and Cat Driller	De
supporting Information for explanation of symbols and abbreviations.		No Ac 0'-	lvanc 6' Co	water observed	ger		000000	letion		ATV Hammer Typ Rope and Cat Driller M. Billiot Logged by	head
St. Louis Catholic High School

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053





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220 Prater Rd Sulphur, LA

St. Louis Catholic High School Corbina Road and James Court | Lake Charles, LA

Terracon Project No. EU235053



Location: See Exploration Plan	0	el ns	ed,	ti	St	rength T	est	(%)	÷t	Atterberg Limits	
Latitude: 30.1810° Longitude: -93.1582°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 10.3 Approximately 4-inches of topsoil			П			0.0	1.176	7.7			-
1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), brown and tan, hard				4.50 (HP)				17.2			
2.0 FAT CLAY (CH), gray and tan, stiff to very stiff, slickensided				4.50 (117)						-	
	-			2.00 (HP)				21.1		54-13-41	
-tan and reddish brown below 4 feet	5-			3.00 (HP)				1			
Boring Terminated at 6 Feet											
Exploration and Testing Procedures for a description of field and laborator edures used and additional data (If any).	γ			Level Observatio	ns					Drill Rig ATV	
Exploration and Testing Procedures for a description of field and laborator adures used and additional data (If any).	γ				ns						e head
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Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



6c	Location: See Exploration Plan	0	in s	ype	2 H		s st	St	rength T	est	(9)	÷,	Atterberg Limits	
Graphic Log	Latitude: 30.1804° Longitude: -93.1582°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines		
Ť	Depth (Ft.) 0.3 Approximately 3-inches of topsoil			\mathbf{T}				1.12	5.6		-			
	1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), brown and light gray, hard			÷	4.50 (HP)				13.9					
	2.0 FAT CLAY (CH), tan and light gray, hard, slickensided				4.50 (HP)									
		5-			2.75 (HP)									
	Boring Terminated at 6 Feet													
proce See S	Exploration and Testing Procedures for a description of field and laboratory adures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations. Is is	4	No Ac	o free	Level Observatio water observed sement Method ntinuous Flight Au						Drill Rig ATV Hammer Typ Rope and Cath Driller M. Billiot Logged by B. Alexander			
					onment Method backfilled with aug	er cutt	ngs upon	comp	letion.		Boring Starte 08-02-2023 Boring Comp 08-02-2023			

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Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053

Boring Log No. B-40

Decation: See Exploration Plan	0	10 5	ge		St	rength T	est	(9)	÷.	Atterberg Limits	
Location: See Exploration Pair Latitude: 30.1807° Longitude: -93.1575°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines
Depth (Ft.) 0.3 Approximately 3-inches of topsoil	_	-	Т			0.4		4.0			
1.0 SILTY CLAY (CL-ML), brown LEAN CLAY (CL), tan and brown, hard	-			4.50 (HP)				9.2		32-16-16	
2.0 FAT CLAY (CH), tan and reddish brown, very stiff to hard	-			4.50 (112)				9.2		52-10-10	
				4.50 (HP)							
6.0	5-			3.50 (HP)							
See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any). See Supporting Information for explanation of symbols and abbreviations.				Level Observatio	ns					Drill Rig ATV Hammer Typ Rope and Catt	

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220 Prater Rd Sulphur, LA

St. Louis Catholic High School Corbina Road and James Court | Lake Charles, LA

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Location: See Exploration Plan	~	el	be	Ħ.,,	St	rength T	est	(%)	Ð,t	Atterberg Limits	
Latitude: 30.1810° Longitude: -93.1567°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) <u>0.4</u> Approximately 5-inches of topsoil		-	Т		-	90				-	-
1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), brown and tan, medium stiff to stiff			-					12.0			
2.0 FAT CLAY (CH), tan and gray, medium stiff to stiff, slickensided	-			1.00 (HP)							
slickensided				1.00 (HP)				18.9			
6.0	5-			1.50 (HP)							
Exploration and Testing Procedures for a description of field and laboratory edures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.		No	o free	Level Observatio a water observed						Drill Rig ATV Hammer Typ Rope and Cati Driller M. Billiot Logged by	hear
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Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



бо	Location: See Exploration Plan	0	el 1s	be	H	St	Strength Te		(0)	÷,	Atterberg Limits	t.
Graphic Log	Latitude: 30.1804° Longitude: -93.1567° Depth (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent Fines
Ť	0.3 Approximately 3-inches of topsoil 1.0 SILTY CLAY (CL-ML), brown, hard			Т					10.3		27-17-10	
	LEAN CLAY (CL), brown and light gray, stiff			Ż	1.50 (HP)				17.5			
	2.0 <u>FAT CLAY (CH)</u> , tan and light gray, stiff to very stiff, slickensided				2.25 (HP)				-			
	6.0	5-			1.75 (HP)	1						
	Boring Terminated at 6 Feet											
proce	Exploration and Testing Procedures for a description of field and laboratory adures used and additional data (If any). Supporting Information for explanation of symbols and abbreviations.				Level Observation water observed	ns					Drill Rig ATV Hammer Typ Rope and Cath Driller	e tead
Note	is Ition Reference: Elevations based on Google Earth				ement Method ntinuous Flight Au	ger					M. Billiot Logged by B. Alexander	
					onment Method backfilled with aug	er cutti	ngs upor	o comp	letion.		Boring Starte 08-02-2023 Boring Comp 08-02-2023	

St. Louis Catholic High School

Corbina Road and James Court | Lake Charles, LA Terracon Project No. EU235053



Location: See Exploration Plan	0	le su	be	ti .c	St	rength T	est	(%)	£	Atterberg Limits	4
Latitude: 30.1806° Longitude: -93.1537°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Test Type	Compressiv e Strength (tsf)	Strain (%)	Water Content (%)	Dry Unit Weight (pcf)	LL-PL-PI	Percent
Depth (Ft.) 0.3 Approximately 3-inches of topsoil			Т			-		5.9			
1.0 SILTY CLAY (CL-ML), brown, hard LEAN CLAY (CL), brown and tan, hard			÷	4.50 (HP)				8.7		40-15-25	-
2.0 FAT CLAY (CH), tan and light gray, hard, with trace silt	1			1.55 (11)				0.7		10 15 15	
				4.50 (HP)							
-with ferrous nodules below 4 feet	5-			1.00 (HP)							
Boring Terminated at 6 Feet											
Exploration and Testing Procedures for a description of field and laboratory dures used and additional data (If any).			C	Level Observatio	ns					Drill Rig ATV	
Exploration and Testing Procedures for a description of field and laboratory edures used and additional data (If any).			C		ns					Drill Rig ATV Hammer Typ Rope and Cati	e
		N	o free							ATV Hammer Typ	e

APPENDIX 3. NRCS USDA Soil Map



Conservation Service

USDA

Web Soil Survey National Cooperative Soil Survey

8/23/2023 Page 1 of 3 Soil Map-Calcasieu Parish, Louisiana



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Calcasieu Parish, Louisiana Survey Area Data: Version 18, Sep 1, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Nov 13, 2022—Nov 27, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Cr	Crowley-Vidrine complex, 0 to 1 percent slopes	30.4	74.9%
Mn	Midland silty clay loam, 0 to 1 percent slopes, rarely flooded	1.6	4.0%
Mt	Mowata-Vidrine complex, 0 to 1 percent slopes, rarely flooded	8.6	21.2%
Totals for Area of Interest		40.6	100.0%

Map Unit Legend

USDA

APPENDIX 4. Wetland Delineation



SENT VIA EMAIL

October 23, 2023

Mr. Stephen C. Hotard Champeaux, Evans, Hotard 720 Dr. Michael Debakey Drive Lake Charles, LA 70601

RE: Wetland Delineation 47-Acre Tract- Corbina Road Calcasieu Parish, Louisiana

Dear Mr. Hotard,

Southland Environmental, LLC is pleased to provide this electronic copy of the Wetland Delineation Report for the referenced property. A copy of this Delineation Report can be submitted to the Corps of Engineers with a request for a preliminary wetland determination upon your review and approval.

If you have any questions or need a bound copy of the report, please do not hesitate to contact us. We appreciate the opportunity to provide this service for you. Sincerely,

C. Blaine Johnson, P.E. Owner/Sr. Engineer

Attachment

WETLAND DELINEATION

47-ACRE TRACT CORBINA ROAD CALCASIEU PARISH, LOIIISIANA

Prepared for:

Champeaux Evans Hotard 702 Dr. Michael Debakey Drive Lake Charles, Louisiana 70601

October 23, 2023

C. Blaine Johnson, P.E. Owner/Sr. Engineer

Jared K

Owner/Sr. Environmental Scientist

Prepared by:



510 Clarence Street Lake Charles, Louisiana 70601 (337) 436-3248

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3.0	SITE	E DESCRIPTION	2
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Infrared Aerial Photograph and Soils Maps	B
Wetland Data Forms	
Site Photographs	
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#### SUMMARY

An approximate 47-acre tract located east of Corbina Road in Lake Charles, Calcasieu Parish, Louisiana was evaluated for the presence of jurisdictional wetlands. The property is undeveloped and is comprised of pastured land. The site has been historically used for agricultural purposes. A series of roads and small drainage swales are located on the tract to promote drainage to aide with hay production and cattle grazing.

The dominant grass vegetation consisted of Yellow Bluestem and Bahia grass. Soils present on the property, as mapped by the United States Department of Agriculture-Natural Resources Conservation Service (USDA-NRCS) include Mowata-Vidrine and Crowley-Vidrine silt loams. The property has a relatively flat topography which is not typical of the listed soil types. Typical Mowata-Vidrine and Crowley-Vidrine silt loams are typically "pimple mounded". The mounds were likely leveled as a result of historical agriculture activities on the property.

The wetland delineation was performed in accordance with the procedures and methods as described in the U.S. Department of the Army Corps of Engineers (COE) 1987 Manual for Wetland Delineations and the Atlantic and Gulf Coastal Plain Regional Supplement 2010.

Based on the results of this delineation, 6.1 acres of wetlands are present within the tract boundary.

#### **1.0 INTRODUCTION**

Southland Environmental, LLC (Southland Environmental) was retained to conduct a wetland delineation on property that is located east of Corbina Road in Lake Charles, Calcasieu Parish. The property is located in Section 23, Township 10 South, Range 08 West. The center of the property is located at Latitude 30° 10' 54.1" North, Longitude 93° 9' 21.1" West. The purpose of the delineation was to evaluate the tract for the potential presence of wetlands. A site location map is included as **Figure 1** and a site diagram is included as **Figure 2**. LIDAR imagery was also reviewed and is included as **Figure 3**. LIDAR is a remote sensing method that uses a near-infrared laser to map changes in elevation of the surface of the Earth. Also included as **Figure 4** is a Flagging Key.

Jared King of Southland Environmental was involved with the field evaluation on October 5, 2023. Mr. King has a Bachelor's of Science Degree in Environmental Science and has experience in wetland ecosystem evaluation and wetland vegetation identification, in addition to specialized training in performing wetland delineations. Mr. King has been performing wetland delineations for over ten years. Blaine Johnson managed the project. Mr. Johnson has over thirty years' experience in environmental investigation and permitting, with over twenty years' experience in wetland permitting. Copies of the applicable Certificates of Training are included as Attachment A.

#### 2.0 METHODOLOGY

The wetland delineation performed by Southland Environmental was conducted in accordance with technical guidelines and methods for wetland delineations set forth by the COE in the 1987

Manual for Wetland Delineations and the Atlantic and Gulf Coastal Plains Regional Supplement 2010. These technical guidelines and methods utilize a multi-parameter approach to identify and delineate wetlands for the purposes of Section 404 of the Clean Water Act.

According to the COE 1987 Manual for Wetland Delineations, a site must have hydrophytic vegetation, hydric soils, and wetland hydrology in order for it to be classified as a wetland. The following definitions are from the COE 1987 Manual for Wetland Determinations:

**Hydrophytic vegetation** – the sum total of macrophytic plant life growing in water or on a substrate that is at least periodically deficient in oxygen as a result of excessive water content. When hydrophytic vegetation comprises a community where indicators of hydric soils and wetland hydrology also occur, the area has wetland vegetation.

Wetland soils – a soil that is saturated, flooded, ponded long enough during the growing season to develop anaerobic conditions that favor the growth and regeneration of hydrophytic vegetation (US Department of Agriculture – Soil Conservation Service 1985). Hydric soils that occur in areas having positive indicators of hydrophytic vegetation and wetland hydrology are wetland soils.

**Wetland hydrology** – the sum total of wetness characteristics in areas that are inundated or have saturated soils for sufficient duration to support hydrophytic vegetation.

Prior to the site visit, the Calcasieu Parish Soil Survey prepared by the USDA-NRCS was reviewed. The purpose of that review was to determine the soil types as mapped by USDA. As indicated by the Soil Survey, the delineated site includes two soil types: Mowata-Vidrine silt loams (Mt) and Crowley-Vidrine silt loams (Cr). Mt soils are listed as a partially hydric soil and Cr soils are listed as a predominantly nonhydric soil in Calcasieu Parish. In addition to the soils map, infrared aerial photographs from 1998, 2004, and 2008 were reviewed. The soil maps and infrared photographs are included as **Attachment B**.

The delineation was begun by traversing the site and making a general evaluation of the topography and drainage features. Sample points were selected at appropriate locations to properly characterize the soil, vegetation, and hydrology on the investigated property. Five representative sample points were selected and a detailed evaluation was conducted at these locations. The data collected at these sample points were recorded on Wetland Data Forms and the location of the sample plots were marked with a Trimble Global Positioning Unit (GPS). The Wetland Data Forms are included as **Attachment C**.

After a general evaluation of the tract and conducting data points, a Trimble GPS was utilized to map the wetland areas. Once GPS mapping was completed, geospatial data was imported into ArcView GIS for graphical display and land cover analysis.

#### **3.0 SITE DESCRIPTION**

The delineated property is located east of Corbina Road and north of East McNeese Street in Lake Charles, Calcasieu Parish. The tract is rectangular in shape and encompasses approximately 47

acres. Based on aerial photography review and the site investigation, the property is currently undeveloped and consists of pasture land. The dominant vegetation on the site is listed within Section 4.1 of this report. As noted earlier, the USDA-NRCS soil maps indicate that soils on the property consist of two soil types: Mt and Cr. Mt soils are listed as partially hydric in Calcasieu Parish. Cr soils are listed as predominantly nonhydric soil.

Photographs of the sample locations were taken and are included as Attachment D.

#### 4.0 FINDINGS

The tract of land was inspected with respect to the potential presence of wetlands. Five sample points were selected to characterize the site. At these sample points, the soils, hydrology, and vegetation were characterized and the information was recorded on Wetland Data Forms. The findings of the delineation are described in the following sections.

#### 4.1 VEGETATION

The typical dominant plant species that were encountered at the site included the following:

#### UPLAND

Brothriochloa ischaemum (King Ranch Bluestem) Croton Capitatus (Hogwort)

FACULTATIVE UPLAND

Paspalum notatum (Bahia grass)

FACULTATIVE

Stenotaphrum secundatum (St. Augustine Grass) Triadica sebifera (Chinese Tallow) Morella cerifera (Southern Bayberry)

FACULTATIVE WETLAND

Saccharum giganteum (Plume Grass) Bidens aristosa (Breaded Beggarticks)

OBLIGATE WETLAND

Juncus effusus (Lamp Rush)

Two of the sample points had a dominance of hydrophytic vegetation.

#### 4.2 SOILS

The review of the Soil Survey indicated that the delineated tract was located on two soil types. Below is a brief description of the soils from the Soil Survey of Calcasieu Parish.

- Mt soils are level and gently sloping, poorly drained and moderately well drained. They are on the Gulf Coast Prairies. The landscape consists of broad flats that have many low mounds. The mounds are circular and range from 30 to 150 feet in diameter and from 1 to 6 feet in height. Individual areas of this complex range from 30 to 1,500 acres and contain about 60 percent Mowata soils and about 30 percent Vidrine soils. The poorly drained Mowata soil is in the intermound areas and the moderately well drained Vidrine soil is on the mounds. Slopes range from about 0 to 1 percent on the intermound areas and from about 1 to 5 percent on the mounds. The investigated property did not exhibit the typical "pimple mounded" topography associated with Mt soils. The soils were likely leveled as a result of the historical agriculture practices that may have occurred on the site. Mt soils are listed as partially hydric in Calcasieu Parish.
- Cr soils are level and somewhat poorly drained. They are on broad convex ridges on the Gulf Coast Prairies. This complex consists of small areas of Crowley and Vidrine soils that are so intermingled that they cannot be mapped separately at the scale selected. Areas are irregular in shape and range from 20 to 1,000 acres. The landscape consists of broad, convex ridges that contain many small convex mounds. The mounds are circular and range from 50 to 150 feet in diameter and 1 foot to 6 feet in height. Cr soils are listed as predominantly nonhydric in Calcasieu Parish however, during the site inspection hydric soil indicators were present in areas of the site mapped Cr.

#### 4.3 HYDROLOGY

General observations and inspections of the soil samples were performed to evaluate for wetland hydrology. One primary indicator or two secondary indicators must be present for an area to have wetland hydrology.

- Sample Plot 1 exhibited no primary or secondary indicators of wetland hydrology. One primary indicator or two secondary indicators must be present for an area to have wetland hydrology.
- Sample Plot 2 exhibited oxidized rhizospheres on living roots, which is primary wetland hydrology indicators. This plot also included secondary hydrology indicators crawfish burrows and geomorphic position.
- Sample Plot 3 exhibited no primary or secondary indicators of wetland hydrology. One primary indicator or two secondary indicators must be present for an area to have wetland hydrology.

- Sample Plot 4 exhibited oxidized rhizospheres on living roots, which is primary wetland hydrology indicators. This plot also included secondary hydrology indicators crawfish burrows and geomorphic position.
- Sample Plot 5 exhibited no primary or secondary indicators of wetland hydrology. One primary indicator or two secondary indicators must be present for an area to have wetland hydrology.

#### 5.0 CONCLUSIONS

An approximate 47-acre tract located adjacent east of Corbina Road in eastern Lake Charles, Louisiana was evaluated for the presence of jurisdictional wetlands. The wetland delineation was performed in accordance with the procedures and methods as described in the COE 1987 Manual for Wetland Delineations.

The investigated property consists of agricultural or pasture land. Due to agricultural practices, the site has been manipulated to promote drainage. Field roads and small drainage swales have been installed on the tract. The eastern section of the property is at a lower elevation and shows evidence of wetland characteristics. A small depression area in the center of the tract that is poorly drained also showed evidence of wetland characteristics. The western portion of the land showed the highest elevations and no evidence of wetland hydrology.

Based on the results of this delineation, approximately 6.1 acres of herbaceous wetlands and 40.9 acres of uplands are present on the investigated property. The wetlands identified on the tract appeared to be isolated in nature and not directly connected or adjacent to a navigable water way.

Site Location Map



Site Diagram



Lidar Imagery



Flagging Key



## ATTACHMENT A

Certificates of Training

# Richard Chinn Environmental Training, Inc.

certifies that

# Jared King

has successfully completed a

# 38 Hour Army Corps of Engineers Wetland Delineation Training Program

Issued Certificate No. 9362 and 3.8 CEUs, September 25 - 28, 2023, in Baton Rouge, Louisiana This course is pre-approved by the Society of Wetland Scientists Professional Certification Program to provide 2.5 Training Credits and/or Points



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This training has been based in part on the U.S. Army Corps of Engineers Wellands Delineation Manual Technical Report Y-87-1 (1987 manual), as provided for in the training materials developed in conjunction with Section 307(e) of the Water Resources Development Act of 1990 for the Wetland Delineator Certification Program.



### ATTACHMENT B

Infrared and Soil Maps







## ATTACHMENT C

Wetland Data Forms

U.S. Army Corps of Engineers WETLAND DETERMINATION DATA SHEET – Atlantic and Gulf Coastal Plain Reg See ERDC/EL TR-10-20; the proponent agency is CECW-CO-R	OMB Control #: 0710-0024, Exp: 11/30/2024 gion Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)
Project/Site: Champeaux Evans Hotard - St. Louis High City/County: Lake Ch	arles/Calcasieu Sampling Date: 10/9/23
Applicant/Owner: Lake Charles Diocese	State: LA Sampling Point: 1
Investigator(s): J.King/L. Demary Section, Township, Range	
Landform (hillside, terrace, etc.): Slight Ridge Local relief (concave, convex	
	3339002 Datum: UTM NAD 83
Soil Map Unit Name: Crowley-Vidrine (Cr)	NWI classification: None
Are climatic / hydrologic conditions on the site typical for this time of year? Yes	No X (If no, explain in Remarks.)
	Circumstances" present? Yes X No
Are Vegetation <u>No</u> , Soil <u>No</u> , or Hydrology <u>No</u> naturally problematic? (If needed, e	xplain any answers in Remarks.)
SUMMARY OF FINDINGS – Attach site map showing sampling point loca	tions, transects, important features, etc.
Hydrophytic Vegetation Present? Yes No X Is the Sampled Area   Hydric Soil Present? Yes X No within a Wetland?   Wetland Hydrology Present? Yes No X	Yes NoX
Remarks: Drier than normal site conditions	
L HYDROLOGY	
Wetland Hydrology Indicators:   Primary Indicators (minimum of one is required; check all that apply)   Surface Water (A1) Aquatic Fauna (B13)   High Water Table (A2) Marl Deposits (B15) (LRR U)   Saturation (A3) Hydrogen Sulfide Odor (C1)   Water Marks (B1) Oxidized Rhizospheres on Living Roots (C3)   Sediment Deposits (B2) Presence of Reduced Iron (C4)   Drift Deposits (B3) Recent Iron Reduction in Tilled Soils (C6)   Algal Mat or Crust (B4) Thin Muck Surface (C7)   Iron Deposits (B5) Other (Explain in Remarks)   Inundation Visible on Aerial Imagery (B7) Water-Stained Leaves (B9)   Field Observations: No X Depth (inches):   Saturation Present? Yes No X Depth (inches):   Saturation Present? Yes No X Depth (inches): Wetland   Uncludes capillary fringe) Describe Recorded Data (stream gauge, monitoring well, aerial photos, previous inspections), if Describe Recorded Data (stream gauge, monitoring well, aerial photos, previous inspections), if	Secondary Indicators (minimum of two required)   Surface Soil Cracks (B6)   Sparsely Vegetated Concave Surface (B8)   Drainage Patterns (B10)   Moss Trim Lines (B16)   Dry-Season Water Table (C2)   Crayfish Burrows (C8)   Saturation Visible on Aerial Imagery (C9)   Geomorphic Position (D2)   Shallow Aquitard (D3)   FAC-Neutral Test (D5)   Sphagnum Moss (D8) (LRR T, U)
Remarks:	
Sampling Point: 1

<u>Tree Stratum</u> (Plot size: <u>30</u> )	Absolute % Cover	Dominant Species?	Indicator Status	Dominance Test worksheet:
1	J.			Number of Dominant Species
2		,		That Are OBL, FACW, or FAC:(A)
3	j.			Total Number of Dominant Species Across All Strata: 3 (B)
5.				Percent of Dominant Species
6.				That Are OBL, FACW, or FAC: <u>33.3%</u> (A/B)
7				Prevalence Index worksheet:
8	J.	and a the same		Total % Cover of: Multiply by:
		=Total Cover		OBL species 0 x 1 = 0
50% of total cover:	20%	of total cover:		FACW species $0 \times 2 = 0$
Sapling/Shrub Stratum (Plot size: 30)		Ver		FAC species $42 \times 3 = 126$
Croton capitatus     Triadica sebifera	20	Yes	UPL FAC	FACU species         6         x 4 =         24           UPL species         72         x 5 =         360
2. <u>Triadica sebifera</u> 3.	2	No	FAC	
3	J.			Column Totals: 120 (A) 510 (B) Prevalence Index = $B/A =$ 4.25
4. 5.	U.			Hydrophytic Vegetation Indicators:
6	î			1 - Rapid Test for Hydrophytic Vegetation
7.				2 - Dominance Test is >50%
8.	c			$3 - Prevalence Index is \leq 3.0^{1}$
	22	=Total Cover		Problematic Hydrophytic Vegetation ¹ (Explain)
50% of total cover: 11		of total cover:	5	
Herb Stratum (Plot size: 30 )				
1. Bothriochloa ischaemum	50	Yes	UPL	
2. Stenotaphrum secundatum	40	Yes	FAC	¹ Indicators of hydric soil and wetland hydrology must be present, unless disturbed or problematic.
3. Kummerowia striata	5	No	FACU	Definitions of Four Vegetation Strata:
4. Iva angustifolia	2	No	UPL	<b>Tree</b> – Woody plants, excluding vines, 3 in. (7.6 cm) or
5. Erigeron annuus	1	No	FACU	more in diameter at breast height (DBH), regardless of
6.				height.
7.	I			
8.	L.			<b>Sapling/Shrub</b> – Woody plants, excluding vines, less than 3 in. DBH and greater than 3.28 ft (1 m) tall.
9.	J.			
10.				
11.				<b>Herb</b> – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall.
12.				
	98	=Total Cover		Woody Vine - All woody vines greater than 3.28 ft in
50% of total cover: 49	20%	of total cover:	20	height.
Woody Vine Stratum (Plot size: 30)				
1			,	
2	L.			
3	J.			
4				
5				Hydrophytic
		=Total Cover		Vegetation
50% of total cover:	20%	of total cover:	,	Present?         Yes         No         X
Remarks: (If observed, list morphological adaptations	s below.)			

Depth	Matrix		Redo	x Featur	es			- Protocomoustreasesureccubescute 1
inches)	Color (moist)	%	Color (moist)	%	Type ¹	Loc ²	Texture	Remarks
0-16	10YR 4/2	95	7.5YR 5/6	5	С	PL/M	Loamy/Clayey	Prominent redox concentrations
Hydric Soil Histosol Histic Ep Black Hi Hydroge Stratified Organic 5 cm Mu Muck Pr 1 cm Mu Depleted Thick Da Coast Pi	oncentration, D=Depl Indicators: (Applicat (A1) bipedon (A2) stic (A3) in Sulfide (A4) d Layers (A5) Bodies (A6) (LRR P, icky Mineral (A7) (LR esence (A8) (LRR U) ick (A9) (LRR P, T) d Below Dark Surface ark Surface (A12) rairie Redox (A16) (M fucky Mineral (S1) (L	ble to all T, U) R P, T, U) (A11) LRA 1504	LRRs, unless othe Thin Dark Si Barrier Islan (MLRA 15 Loamy Muck Loamy Gley X Depleted Ma Redox Dark Depleted Da Redox Depre Marl (F10) (I Depleted Oc	erwise n urface (S ds 1 cm <b>3B, 153</b> dy Minerri ed Matrit trix (F3) Surface rk Surfa essions <b>.RR U)</b> thric (F1 esse Mat	oted.) 69) (LRR Muck (S D) al (F1) (L x (F2) (F6) ce (F7) (F8) 1) (MLRA sses (F1)	S, T, U) 12) RR O) A 151) 2) (LRR O	Indicators 1 cm   2 cm   2 coast (out Reduc Reduc Red Red P Red P Red P Very S Very S	PL=Pore Lining, M=Matrix. s for Problematic Hydric Soils ³ : Muck (A9) (LRR O) Muck (A10) (LRR S) Prairie Redox (A16) sside MLRA 150A) ced Vertic (F18) sside MLRA 150A, 150B) nont Floodplain Soils (F19) (LRR P, T) alous Bright Floodplain Soils (F20) RA 153B) Parent Material (F21) Shallow Dark Surface (F22) sside MLRA 138, 152A in FL, 154) r Islands Low Chroma Matrix (TS7)
	Bleved Matrix (S4)		Delta Ochric	16	28/2/202	1983 32 112.0	·	RA 153B, 153D)
	Redox (S5)		Reduced Ve	CALL ROOM AND AND AND				(Explain in Remarks)
Stripped	Matrix (S6)		Piedmont Fl	oodplain	Soils (F	19) <b>(MLR</b> /	A 149A)	
and the set of the set of the set of the	rface (S7) <b>(LRR P, S</b> ,	S 16855 1985458	Anomalous	19455 (1 <del>77</del> 7) (1945) (1955)		2001-0110-0120-0120	10	
	e Below Surface (S8)	)	(MLRA 14					ators of hydrophytic vegetation and
LKK	S, T, U)		Very Shallov (MLRA 13					land hydrology must be present, ess disturbed or problematic.
	Layer (if observed):							
Type: Depth (ii							Hydric Soil Pres	sent? Yes X No

WETLAND DETERMINATION DATA SHEE	Prps of Engineers ET – Atlantic and Gulf Coastal Pl proponent agency is CECW-CO-		OMB Control #: 0710-0024, Exp: 11/30/2024 Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)
Project/Site: Champeaux Evans Hotard - St. Lou	uis High City/County:	Lake Charles/0	Calcasieu Sampling Date: 10/9/23
Applicant/Owner: Lake Charles Diocese			State: LA Sampling Point: 2
Investigator(s): J.King/L. Demary	Section, Township	o, Range: 23-1	
Landform (hillside, terrace, etc.): Slight Depressi	sion Local relief (concave	, convex, none	): Concave Slope (%): 0-1
Subregion (LRR or MLRA): LRR T, MLRA 150A		Long: 33389	
Soil Map Unit Name: Mowata-Vidrine (Mt)			NWI classification: None
Are climatic / hydrologic conditions on the site typi	ical for this time of year? Ye	s N	lo X (If no, explain in Remarks.)
Are Vegetation No , Soil No , or Hydrology			nstances" present? Yes X No
Are Vegetation <u>No</u> , Soil <u>No</u> , or Hydrology			any answers in Remarks.)
SUMMARY OF FINDINGS – Attach site	e map showing sampling poir	nt locations	, transects, important features, etc.
Hydric Soil Present? Yes	X No Is the Sampl X No within a Wet		Yes <u>X</u> No
Remarks: Drier than normal site conditions			
HYDROLOGY			
Wetland Hydrology Indicators:		<u>Sec</u>	ondary Indicators (minimum of two required)
Primary Indicators (minimum of one is required; o	check all that apply)		Surface Soil Cracks (B6)
Surface Water (A1)	Aquatic Fauna (B13)		Sparsely Vegetated Concave Surface (B8)
High Water Table (A2)	Marl Deposits (B15) (LRR U)		Drainage Patterns (B10)
Saturation (A3)	_Hydrogen Sulfide Odor (C1) Oxidized Rhizospheres on Living Root		Moss Trim Lines (B16)
Water Marks (B1) X Sediment Deposits (B2)	Presence of Reduced Iron (C4)		Dry-Season Water Table (C2) Crayfish Burrows (C8)
Drift Deposits (B3)	Recent Iron Reduction in Tilled Soils (	ethologica	Saturation Visible on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Thin Muck Surface (C7)	35	Geomorphic Position (D2)
Iron Deposits (B5)	Other (Explain in Remarks)		Shallow Aquitard (D3)
Inundation Visible on Aerial Imagery (B7)			FAC-Neutral Test (D5)
Water-Stained Leaves (B9)			Sphagnum Moss (D8) <b>(LRR T, U)</b>
Field Observations:			
Surface Water Present? Yes No	X Depth (inches):		
Water Table Present? Yes No	X Depth (inches):		
Saturation Present? Yes No	X Depth (inches):	Wetland Hydr	ology Present? Yes X No
(includes capillary fringe)		2585 KI 0367 1057 10	
Describe Recorded Data (stream gauge, monitor	ring well, aerial photos, previous inspec	tions), if availat	ble:
Remarks:			

Sampling Point: ____2

	Absolute	Dominant	Indicator	The a test of the test of
Tree Stratum (Plot size: <u>30</u> )	% Cover	Species?	Status	Dominance Test worksheet:
1				Number of Dominant Species
2				That Are OBL, FACW, or FAC:(A)
3				Total Number of Dominant
4				Species Across All Strata: 2 (B)
5				Percent of Dominant Species
6.				That Are OBL, FACW, or FAC: 100.0% (A/B)
7.				Prevalence Index worksheet:
8.				Total % Cover of: Multiply by:
		=Total Cover		OBL species 30 x 1 = 30
50% of total cover:		of total cover:		FACW species 0 x 2 = 0
Sapling/Shrub Stratum (Plot size: 30 )				FAC species $42 \times 3 = 126$
1. Croton capitatus	1	No	UPL	FACU species $20 \times 4 = 80$
2.				UPL species $1 \times 5 = 5$
3.		<u> </u>		Column Totals: 93 (A) 241 (B)
4				Prevalence Index = B/A =
5				Hydrophytic Vegetation Indicators:
6				1 - Rapid Test for Hydrophytic Vegetation
7	<u> </u>			X 2 - Dominance Test is >50%
8.				X 3 - Prevalence Index is ≤3.0 ¹
	1	=Total Cover		Problematic Hydrophytic Vegetation ¹ (Explain)
50% of total cover: 1	20%	of total cover:	1	
Herb Stratum (Plot size: 30 )				
1. Stenotaphrum secundatum	40	Yes	FAC	
2. Juncus effusus	30	Yes	OBL	¹ Indicators of hydric soil and wetland hydrology must be present, unless disturbed or problematic.
3. Cynodon dactylon	10	No	FACU	Definitions of Four Vegetation Strata:
	5		FACU	
4. Paspalum notatum		No		<b>Tree</b> – Woody plants, excluding vines, 3 in. (7.6 cm) or more in diameter at breast height (DBH), regardless of
5. Erigeron annuus	5	No	FACU	height.
6. Cuphea viscosissima	2	No	FAC	noight.
7				Sapling/Shrub – Woody plants, excluding vines, less
8				than 3 in. DBH and greater than 3.28 ft (1 m) tall.
9				
10				
11.				<b>Herb</b> – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall.
12.				
	92	=Total Cover		Woody Vine – All woody vines greater than 3.28 ft in
50% of total cover: 4		of total cover:	19	height.
Woody Vine Stratum (Plot size: 30 )				
// ·/				
2.				
3.		<u> </u>		
4				
5				Hydrophytic
		=Total Cover		Vegetation
50% of total cover:	20%	of total cover:		Present? Yes X No
Remarks: (If observed, list morphological adaptation	ns below.)			
, <u>,</u> , , , , , , , , , , , , , , , , ,				

Image: Sign of Color (moist)       %       Color (moist)       %       Type1       Loc ² Texture       Remarks         4       10YR 3/2       100	Depth	ription: (Describe) Matrix			x Featur					
15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         16       1       1       Mill 2       1       Indicators for Problematic Hydric Solls ³ :       1         15       10 Castors for Problematic Hydric Solls ³ :       1       1       cm Muck (A10) (LRR Q)       2       2       m Muck (A10) (LRR Q)       2       2       m Muck (A10) (LRR Q)       2       2       m Muck (A10) (LR Q)       2       2       m Muck (A10) (LR R)       2       2       2       2       2       1       cm Muck (A10) (LR R)       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2	inches)	3	%		11 N 15 A	4	Loc ²	Те	xture	Remarks
15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         15       10YR 4/2       98       7.5YR 5/6       2       C       M       Learny/Clayey       Prominent redox concentration         16       1       1       Mill 2       1       Indicators for Problematic Hydric Solls ³ :       1         15       10 Castors for Problematic Hydric Solls ³ :       1       1       cm Muck (A10) (LRR Q)       2       2       m Muck (A10) (LRR Q)       2       2       m Muck (A10) (LRR Q)       2       2       m Muck (A10) (LR Q)       2       2       m Muck (A10) (LR R)       2       2       2       2       2       1       cm Muck (A10) (LR R)       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2       2	0-4	10YR 3/2	100					Loam	v/Clavev	
:: C=Concentration, D=Depletion, RM=Reduced Matrix, MS=Masked Sand Grains. ² Location: PL=Pore Lining, M=Matrix.         c Soil Indicators: (Applicable to all LRRs, unless otherwise noted.)       Indicators: for Problematic Hydric Solls ³ :         istosol (A1)       Thin Dark Surface (S9) (LRR S, T, U)       1 cm Muck (A9) (LRR O)         istic Epipedon (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR S)         iack Histic (A3)       (MLRA 153B, 153D)       X Cosast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       custide MLRA 150A)         tratified Layers (A5)       Loamy Mucky Mineral (F1)       Redox Dark Surface (F6)         rganic Bodies (A6) (LRR P, T, U)       Redox Dark Surface (F6)       Peledmont Floodplain Soils (F19) (LRR P,         cm Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B, 152A in FL, 154)         cast Prairie Redox (A16)       Mari (F10) (LRR U)       Depleted Oark Surface (F7)         cast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       Very Shallow Dark Surface (F22)         cast Prairie Redox (A16) (MLRA 150A)       Dehle Ochric (F11) (MLRA 151)       (MLRA 153B, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Pledmont Floodplain Soils (F19) (MLRA 149A)       Other (Explain in Remarks)         ripped Matrix (S6)       Pledmont Floodplain Soils (F10) (MLR	Control and Control of									
c Soll Indicators: (Applicable to all LRRs, unless otherwise noted.)       Indicators: (Applicable to all LRRs, unless otherwise noted.)         istosol (A1)       Thin Dark Surface (S9) (LRR S, T, U)       Indicators for Problematic Hydric Solls ³ :         istosol (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR O)         lack Histic (A3)       (MLRA 153B, 153D)       X Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         tratified Layers (A5)       Depleted Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         num Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Mari (F10) (LRR U)       Pieleted Ochric (F11) (MLRA 151)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (MLRA 150A, 150B)       Other (Explain in Remarks)         riped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B, 153D)         andy Redox (S5)       Piedmont Floodplain Soils (F19) (MLRA 150A)       Other (Explain in Remarks)         ripped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B,	4-15	10YR 4/2		7.5YR 5/6			<u> </u>	Loam	y/Clayey	Prominent redox concentrations
c Soll Indicators: (Applicable to all LRRs, unless otherwise noted.)       Indicators: (Applicable to all LRRs, unless otherwise noted.)         istosol (A1)       Thin Dark Surface (S9) (LRR S, T, U)       Indicators for Problematic Hydric Solls ³ :         istosol (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR O)         lack Histic (A3)       (MLRA 153B, 153D)       X Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         tratified Layers (A5)       Depleted Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         num Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Mari (F10) (LRR U)       Pieleted Ochric (F11) (MLRA 151)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (MLRA 150A, 150B)       Other (Explain in Remarks)         riped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B, 153D)         andy Redox (S5)       Piedmont Floodplain Soils (F19) (MLRA 150A)       Other (Explain in Remarks)         ripped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B,					·					
c Soll Indicators: (Applicable to all LRRs, unless otherwise noted.)       Indicators: (Applicable to all LRRs, unless otherwise noted.)         istosol (A1)       Thin Dark Surface (S9) (LRR S, T, U)       Indicators for Problematic Hydric Solls ³ :         istosol (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR O)         lack Histic (A3)       (MLRA 153B, 153D)       X Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         tratified Layers (A5)       Depleted Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         num Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Mari (F10) (LRR U)       Pieleted Ochric (F11) (MLRA 151)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (MLRA 150A, 150B)       Other (Explain in Remarks)         riped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B, 153D)         andy Redox (S5)       Piedmont Floodplain Soils (F19) (MLRA 150A)       Other (Explain in Remarks)         ripped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B,						<u></u>				
c Soll Indicators: (Applicable to all LRRs, unless otherwise noted.)       Indicators: (Applicable to all LRRs, unless otherwise noted.)         istosol (A1)       Thin Dark Surface (S9) (LRR S, T, U)       Indicators for Problematic Hydric Solls ³ :         istosol (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR O)         lack Histic (A3)       (MLRA 153B, 153D)       X Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         tratified Layers (A5)       Depleted Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         num Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Mari (F10) (LRR U)       Pieleted Ochric (F11) (MLRA 151)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (MLRA 150A, 150B)       Other (Explain in Remarks)         riped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B, 153D)         andy Redox (S5)       Piedmont Floodplain Soils (F19) (MLRA 150A)       Other (Explain in Remarks)         ripped Matrix (S6)       Piedmont Floodplain Soils (F20)       MLRA 153B,	,				ő <del></del>	(21)				
istosol (A1)       Thin Dark Surface (S9) (LRR S, T, U)       1 cm Muck (A9) (LRR O)         istic Epipedon (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR S)         lack Histic (A3)       (MLRA 153B, 153D)       X Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         rratified Layers (A5)       Loamy Gleyed Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       X Depleted Matrix (F3)       (outside MLRA 150A)         cm Muck (A9) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         uck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Mari (F10) (LRR U)       Red Parent Material (F21)         very Shallow Dark Surface (A12)       Depleted Ochric (F11) (MLRA 151)       Very Shallow Dark Surface (F22)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (MLRA 150A, 150B)       Piedmont Floodplain Soils (F19) (MLRA 149A)         ark Surface (S5)       Piedmont Floodplain Soils (F19) (MLRA 149A)       Other (Explain in Remarks)         ripped Matrix (S6)       Piedmont Floodplain Soils (F20)       Other (Explain in Remarks) <td>Type: C=Co</td> <td>oncentration, D=Depl</td> <td>letion, RM</td> <td>Reduced Matrix, N</td> <td>/IS=Mas</td> <td>ked Sand</td> <td>d Grains.</td> <td></td> <td>²Location: F</td> <td>PL=Pore Lining, M=Matrix.</td>	Type: C=Co	oncentration, D=Depl	letion, RM	Reduced Matrix, N	/IS=Mas	ked Sand	d Grains.		² Location: F	PL=Pore Lining, M=Matrix.
istic Epipedon (A2)       Barrier Islands 1 cm Muck (S12)       2 cm Muck (A10) (LRR S)         lack Histic (A3)       (MLRA 153B, 153D)       X Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         tratified Layers (A5)       Loamy Gleyed Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       X Depleted Matrix (F3)       Reduced Vertic (F18)         cm Mucky Mineral (A7) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         nuck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Marl (F10) (LRR U)       Red Parent Material (F21)         very Shallow Dark Surface (F13) (LRR O, P, T)       Ion-Manganese Masses (F12) (LRR O, P, T)       Red Parent Material (F21)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         piedmont Floodplain Soils (F20)       (MLRA 1338, 152A in FL, 154)       Slndicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic.         tritive Layer (if observed):       ype:       (MLRA 138, 152A in FL, 154)       Slndicators of hydrophytic vegetation and wetland hydrology must be pres	ydric Soil I	ndicators: (Applica	ble to all	LRRs, unless othe	erwise n	oted.)			Indicators f	for Problematic Hydric Soils ³ :
lack Histic (A3)       (MLRA 153B, 153D)       X       Coast Prairie Redox (A16)         ydrogen Sulfide (A4)       Loamy Mucky Mineral (F1) (LRR O)       (outside MLRA 150A)         tratified Layers (A5)       Loamy Gleyed Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       X       Depleted Matrix (F3)       (outside MLRA 150A, 150B)         cm Mucky Mineral (A7) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P, 1)         nuck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Marl (F10) (LRR U)       Red Parent Material (F21)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       Red Parent Material (F21)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F20)       Other (Explain in Remarks)         otype Layer (if observed):       Very Shallow Dark Surface (F22)       3         indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic.       1						tivera at cesta	000000			
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tratified Layers (A5)       Loamy Gleyed Matrix (F2)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       X       Depleted Matrix (F3)       Reduced Vertic (F18)         rganic Bodies (A6) (LRR P, T, U)       X       Depleted Matrix (F3)       Piedmont Floodplain Soils (F19) (LRR P, T)         rganic Bodies (A8) (LRR U)       Depleted Dark Surface (F7)       Anomalous Bright Floodplain Soils (F20)       Marl (F10) (LRR U)         rganic Bodies (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Marl (F10) (LRR U)       Red Parent Material (F21)         very Shallow Dark Surface (A12)       Depleted Ochric (F11) (MLRA 151)       Very Shallow Dark Surface (F22)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       Goutside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F19) (MLRA 149A)       3         ark Surface (S7) (LRR P, S, T, U)       Anomalous Bright Floodplain Soils (F20)       3         (MLRA 138, 152A in FL, 154)       unless disturbed or problematic.         (MLRA 138, 152A in FL, 154)       unl		• •		÷.	5					10. TV
rganic Bodies (A6) (LRR P, T, U) X Depleted Matrix (F3) (outside MLRA 150A, 150B) cm Mucky Mineral (A7) (LRR P, T, U) Redox Dark Surface (F6) luck Presence (A8) (LRR U) Depleted Dark Surface (F7) Anomalous Bright Floodplain Soils (F19) (LRR P, cm Muck (A9) (LRR P, T) Redox Depressions (F8) (MLRA 153B) epleted Below Dark Surface (A11) Marl (F10) (LRR U) Red Parent Material (F21) Very Shallow Dark Surface (F22) oast Prairie Redox (A16) (MLRA 150A) Iron-Manganese Masses (F12) (LRR O, P, T) andy Mucky Mineral (S1) (LRR O, S) Umbric Surface (F13) (LRR P, T, U) Barrier Islands Low Chroma Matrix (TS7) andy Gleyed Matrix (S4) Delta Ochric (F17) (MLRA 151) (MLRA 150A, 150B) tripped Matrix (S6) Reduced Vertic (F18) (MLRA 150A, 150B) Piedmont Floodplain Soils (F20) (MLRA 149A, 153C, 153D) (MLRA 149A) ark Surface (S7) (LRR P, S, T, U) (MLRA 149A) Anomalous Bright Floodplain Soils (F20) (MLRA 149A, 153C, 153D) (MLRA 153D) ³ Indicators of hydrophytic vegetation and wetland hydrology must be present, (MLRA 138, 152A in FL, 154) unless disturbed or problematic.		CALIFORNIA CONTRACTOR AND				COLUMN CONTRACTOR	RR O)		11 <b>5</b> 00990657306	
cm Mucky Mineral (A7) (LRR P, T, U)       Redox Dark Surface (F6)       Piedmont Floodplain Soils (F19) (LRR P,         luck Presence (A8) (LRR U)       Depleted Dark Surface (F7)       Anomalous Bright Floodplain Soils (F20)         cm Muck (A9) (LRR P, T)       Redox Depressions (F8)       Marl (F10) (LRR U)         epleted Below Dark Surface (A11)       Marl (F10) (LRR U)       Red Parent Material (F21)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       Red Parent Material (F21)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Gleyed Matrix (S4)       Delta Ochric (F17) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F20)       Other (Explain in Remarks)         ark Surface (S7) (LRR P, S, T, U)       Anomalous Bright Floodplain Soils (F20)       Other (Explain in Remarks)         olyvalue Below Surface (S8)       (MLRA 149A, 153C, 153D)       Other (Explain in Remarks)         (LRR S, T, U)       Very Shallow Dark Surface (F22) ³ Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic.         tritter Layer (if observed):       ype:		ten ten allerant era terteratu		the second se		0 0				en second se a des caraceres
Luck Presence (A8) (LRR U)       Depleted Dark Surface (F7)       Anomalous Bright Floodplain Soils (F20)         cm Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Marl (F10) (LRR U)       Red Parent Material (F21)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F20)       Other (Explain in Remarks)         olyvalue Below Surface (S8)       (MLRA 149A, 153C, 153D)       3Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic.         ype:		12 14 12 13	(80) 25	· ·	10 II.				25	
cm Muck (A9) (LRR P, T)       Redox Depressions (F8)       (MLRA 153B)         epleted Below Dark Surface (A11)       Marl (F10) (LRR U)       Red Parent Material (F21)         hick Dark Surface (A12)       Depleted Ochric (F11) (MLRA 151)       Very Shallow Dark Surface (F22)         oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F19) (MLRA 149A)       Other (Explain in Remarks)         ark Surface (S7) (LRR P, S, T, U)       Anomalous Bright Floodplain Soils (F20) ³ Indicators of hydrophytic vegetation and         very Shallow Dark Surface (if observed):       ype:		and a second second second second	anine e sectore. o	AND MUSE CONSIST		All Contraction				
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oast Prairie Redox (A16) (MLRA 150A)       Iron-Manganese Masses (F12) (LRR O, P, T)       (outside MLRA 138, 152A in FL, 154)         andy Mucky Mineral (S1) (LRR O, S)       Umbric Surface (F13) (LRR P, T, U)       Barrier Islands Low Chroma Matrix (TS7)         andy Gleyed Matrix (S4)       Delta Ochric (F17) (MLRA 151)       (MLRA 153B, 153D)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F19) (MLRA 149A)       Other (Explain in Remarks)         ark Surface (S7) (LRR P, S, T, U)       Anomalous Bright Floodplain Soils (F20)       Indicators of hydrophytic vegetation and         (LRR S, T, U)       Very Shallow Dark Surface (F22)       wetland hydrology must be present,       unless disturbed or problematic.         ictive Layer (if observed):       ype:	Depleted	Below Dark Surface	e (A11)	Marl (F10) (I	.RR U)				<u> </u>	× 9
andy Mucky Mineral (S1) (LRR O, S) andy Gleyed Matrix (S4) andy Redox (S5) tripped Matrix (S6) ark Surface (S7) (LRR P, S, T, U) olyvalue Below Surface (S8) (LRR S, T, U) (MLRA 138, 152A in FL, 154) Mucky Mineral (S1) (LRR O, S) Delta Ochric (F13) (LRR P, T, U) (MLRA 151) (MLRA 153B, 153D) (MLRA 153B, 153D) Other (Explain in Remarks) ³ Indicators of hydrophytic vegetation and wetland hydrology must be present, unless disturbed or problematic.	ALADOTTALIA: ADVIS	A REAL PROPERTY AND A REAL		the second second	14 - 129 <b>9</b> (1960) - 1960 - 1960 - 1960 - 1960		13 100000000000000000000000000000000000			
andy Gleyed Matrix (S4)       Delta Ochric (F17) (MLRA 151)       (MLRA 153B, 153D)         andy Redox (S5)       Reduced Vertic (F18) (MLRA 150A, 150B)       Other (Explain in Remarks)         tripped Matrix (S6)       Piedmont Floodplain Soils (F19) (MLRA 149A)       Other (Explain in Remarks)         ark Surface (S7) (LRR P, S, T, U)       Anomalous Bright Floodplain Soils (F20)       Indicators of hydrophytic vegetation and         olyvalue Below Surface (S8)       (MLRA 149A, 153C, 153D)       Indicators of hydrophytic vegetation and         (LRR S, T, U)       Very Shallow Dark Surface (F22)       wetland hydrology must be present,         (MLRA 138, 152A in FL, 154)       unless disturbed or problematic.         ictive Layer (if observed):       ype:		en a erre d'averañ he		· —		e a suite s	a andreasa	), P, T)	atus 12 12	
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ype:				(MLRA 13	8, 152A	in FL, 1	54)		unles	s disturbed or problematic.
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이 같은 것 같은	Type:			- 3						
epth (inches): Yes X No	Depth (ir	nches):						Hydri	c Soil Prese	nt? Yes <u>X</u> No

U.S. Army WETLAND DETERMINATION DATA S See ERDC/EL TR-10-20; th		OMB Control #: 0710-0024, Exp: 11/30/2024 Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)	
Project/Site: Champeaux Evans Hotard - St	. Louis High	City/County: Lake Charles/	Calcasieu Sampling Date: 10/9/23
Applicant/Owner: Lake Charles Diocese			State: LA Sampling Point: 3
Investigator(s): J.King/L. Demary	Se	ection, Township, Range: 23-	
Landform (hillside, terrace, etc.): Flat		I relief (concave, convex, non	
Subregion (LRR or MLRA): LRR T, MLRA 15		Long: 3338	
2	Lat. 400100	Eong3336.	
Soil Map Unit Name: Mowata-Vidrine (Mt)	2 1 2 2 2 2 2 2		NWI classification: None
Are climatic / hydrologic conditions on the site		2	No X (If no, explain in Remarks.)
Are Vegetation <u>No</u> , Soil <u>No</u> , or Hydrol	ogy <u>No</u> significantly distu	urbed? Are "Normal Circu	mstances" present? Yes X No
Are Vegetation <u>No</u> , Soil <u>No</u> , or Hydrol	ogy <u>No</u> naturally problem	natic? (If needed, explain	any answers in Remarks.)
SUMMARY OF FINDINGS - Attach	site map showing sa	mpling point locations	, transects, important features, etc
Hydric Soil Present?	Yes No X Yes X No Yes No X	Is the Sampled Area within a Wetland?	YesNo_X
Remarks: Drier than normal site conditions			
HYDROLOGY			
			condary Indicators (minimum of two required)
Wetland Hydrology Indicators: Primary Indicators (minimum of one is requir	ed: check all that apply)	<u></u>	Surface Soil Cracks (B6)
Surface Water (A1)	Aquatic Fauna (B13)		Sparsely Vegetated Concave Surface (B8)
High Water Table (A2)	Marl Deposits (B15) (L	RR U)	Drainage Patterns (B10)
Saturation (A3)	Hydrogen Sulfide Odor	5	Moss Trim Lines (B16)
Water Marks (B1)	Oxidized Rhizospheres	on Living Roots (C3)	Dry-Season Water Table (C2)
Sediment Deposits (B2)	Presence of Reduced I	ron (C4)	Crayfish Burrows (C8)
Drift Deposits (B3)	Recent Iron Reduction	in Tilled Soils (C6)	Saturation Visible on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Thin Muck Surface (C7	[′] )	Geomorphic Position (D2)
Iron Deposits (B5)	Other (Explain in Rema	arks)	Shallow Aquitard (D3)
Inundation Visible on Aerial Imagery (B7	)		FAC-Neutral Test (D5)
Water-Stained Leaves (B9)			Sphagnum Moss (D8) (LRR T, U)
Field Observations:			
Surface Water Present? Yes	No X Depth (inches)		
Water Table Present? Yes	No X Depth (inches)	N. H	
Saturation Present? Yes	No X Depth (inches)	): Wetland Hyd	rology Present? Yes No X
(includes capillary fringe) Describe Recorded Data (stream gauge, mo	nitoring well, aerial photos, r	nrevious inspections), if availa	ble:
	filtering wear, dental priotos, j	previous inspections), il uvult	
Remarks:			

Sampling Point: ____3

<u>Tree Stratum</u> (Plot size: 30)	Absolute % Cover	Dominant Species?	Indicator Status	Dominance Test worksheet:
1				Number of Dominant Species That Are OBL, FACW, or FAC: 1 (A)
3.				Total Number of Dominant
4.				Species Across All Strata: <u>4</u> (B)
5				Percent of Dominant Species That Are OBL, FACW, or FAC: 25.0% (A/B)
7.			8	Prevalence Index worksheet:
8.			5	Total % Cover of: Multiply by:
		=Total Cover		OBL species 0 x 1 = 0
50% of total cover:	20%	of total cover:		FACW species 0 x 2 = 0
Sapling/Shrub Stratum (Plot size: 30 )				FAC species 27 x 3 = 81
1. Croton capitatus	5	Yes	UPL	FACU species 50 x 4 = 200
2. Triadica sebifera	5	Yes	FAC	UPL species y0 x 5 =450
3.				Column Totals: 167 (A) 731 (B)
4.				Prevalence Index = B/A = 4.38
5.				Hydrophytic Vegetation Indicators:
6.				1 - Rapid Test for Hydrophytic Vegetation
7.				2 - Dominance Test is >50%
8.				3 - Prevalence Index is ≤3.0 ¹
	10	=Total Cover		Problematic Hydrophytic Vegetation ¹ (Explain)
50% of total cover: 5	20%	of total cover:	2	
Herb Stratum (Plot size: 30 )				
1. Bothriochloa ischaemum	80	Yes	UPL	¹ Indicators of hydric soil and wetland hydrology must be
2. Paspalum notatum	50	Yes	FACU	present, unless disturbed or problematic.
3. Stenotaphrum secundatum		No	FAC	Definitions of Four Vegetation Strata:
4. Iva angustifolia	5	No	UPL	<b>Tree</b> – Woody plants, excluding vines, 3 in. (7.6 cm) or
5. Cuphea viscosissima	2	No	FAC	more in diameter at breast height (DBH), regardless of
6.				height.
7.				
8.				Sapling/Shrub – Woody plants, excluding vines, less
9.				than 3 in. DBH and greater than 3.28 ft (1 m) tall.
10.				
14				Herb – All herbaceous (non-woody) plants, regardless
12.				of size, and woody plants less than 3.28 ft tall.
	157	=Total Cover		Woody Vine – All woody vines greater than 3.28 ft in
50% of total cover: 75		of total cover:	32	height.
Woody Vine Stratum (Plot size: 30 )				
1.				
2.				
3.				
4.				
5.				
· · · · · · · · · · · · · · · · · · ·		=Total Cover		Hydrophytic
50% of total cover:		of total cover:		Vegetation Present? Yes No X
		or total cover.		
Remarks: (If observed, list morphological adaptation	ns below.)			

I

Depth	Matrix	200 (1993), 1997, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 1998, 19	Redo	x Featur	es					
inches)	Color (moist)	%	Color (moist)	%	Type ¹	Loc ²	Tex	ture	Remarks	
0-16	10YR 4/2	95	7.5YR 5/6	5	С	PL/M	Loamy	/Clayey	Prominent redox conce	ntrations
				_	<u>.</u>	·		·		
	oncentration, D=Depl		Reduced Matrix, N	  //S=Mas	ked Sand			² Location: PI	L=Pore Lining, M=Matrix.	
ydric Soil	Indicators: (Applica	ble to all L	RRs, unless othe	erwise n	noted.)				or Problematic Hydric So	ils³:
Histosol	(A1)		Thin Dark Su	urface (S	69) <b>(LRR</b>	S, T, U)		1 cm Mu	ck (A9) <b>(LRR O)</b>	
Histic Ep	pipedon (A2)		Barrier Islan	ds 1 cm	Muck (S	12)	-	2 cm Mu	ck (A10) <b>(LRR S)</b>	
Black Hi	istic (A3)		(MLRA 15	3B, 153	D)			X Coast Pr	airie Redox (A16)	
Hydroge	en Sulfide (A4)		Loamy Muck	y Miner	al (F1) <b>(L</b>	RR O)		(outsic	ie MLRA 150A)	
Stratified	d Layers (A5)		Loamy Gleye	ed Matri	x (F2)		_	Reduced	l Vertic (F18)	
Organic	Bodies (A6) (LRR P,	T, U)	X Depleted Ma	trix (F3)	e e		-	(outsic	ie MLRA 150A, 150B)	
5 cm Mu	ucky Mineral (A7) <b>(LR</b>	R P, T, U)	Redox Dark	Surface	(F6)			Piedmon	t Floodplain Soils (F19) <b>(L</b>	RR P, T
Muck Pr	esence (A8) (LRR U)		Depleted Da	rk Surfa	ce (F7)		-	Anomalo	us Bright Floodplain Soils	(F20)
1 cm Mu	uck (A9) <b>(LRR P, T)</b>		Redox Depre	essions	(F8)		-	(MLRA	(153B)	
	d Below Dark Surface	e (A11)	Marl (F10) (I	RR U)				Red Pare	ent Material (F21)	
— Thick Da	ark Surface (A12)		Depleted Oc	hric (F1	1) (MLRA	A 151)	1	Very Sha	allow Dark Surface (F22)	
	rairie Redox (A16) (M	LRA 150A	) Iron-Mangan	ese Ma	sses (F12	2) (LRR O	, P, T)	(outsic	ie MLRA 138, 152A in FL	, 154)
Sandy N	/lucky Mineral (S1) <b>(L</b>	RR O, S)	Umbric Surfa	ace (F13	3) (LRR F	P, T, U)		Barrier Is	slands Low Chroma Matrix	(TS7)
 Sandy G	Gleyed Matrix (S4)		Delta Ochric	(F17) <b>(</b>	MLRA 15	1)	1	(MLRA	153B, 153D)	a 10
The second s	Redox (S5)		Reduced Ve				0B)		xplain in Remarks)	
Stripped	I Matrix (S6)		Piedmont Flo	oodplain	Soils (F	19) (MLR	A 149A)	_	an management of the state of the second strategy of the second stra	
- 10 - 10	rface (S7) (LRR P, S	. T. U)	Anomalous I	12	10	2622533	1000			
erri Constitución - Serro O Re	e Below Surface (S8		(MLRA 14	9A. 153	C. 153D)			³ Indicato	rs of hydrophytic vegetatio	n and
	S, T, U)	ć	Very Shallov	10-10-10-10-10-10-10-10-10-10-10-10-10-1					d hydrology must be prese	
\$			(MLRA 13		· · · · · · · · · · · · · · · · · · ·	35%e			disturbed or problematic.	
estrictive	Layer (if observed):									
Туре:										
Depth (ir	nah co):						Uv del o	Soil Presen	t? Yes X No	

U.S. Army Corps of En WETLAND DETERMINATION DATA SHEET – Atlant See ERDC/EL TR-10-20; the proponent	ic and Gulf Coastal Plain Region	OMB Control #: 0710-0024, Exp: 11/30/2024 Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)
Project/Site: Champeaux Evans Hotard - St. Louis High	City/County: Lake Charles/	Calcasieu Sampling Date: 10/9/23
Applicant/Owner: Lake Charles Diocese	80 - 11 ⁴	State: LA Sampling Point: 4
Investigator(s): J.King/L. Demary	Section, Township, Range: 23-	
Landform (hillside, terrace, etc.): Slight Depression	Local relief (concave, convex, none	e): Concave Slope (%): 0-1
Subregion (LRR or MLRA): LRR T, MLRA 150A Lat: 48513		
Soil Map Unit Name: Mowata-Vidrine (Mt)		NWI classification: None
Are climatic / hydrologic conditions on the site typical for this ti	me of year? Yes N	No X (If no, explain in Remarks.)
		mstances" present? Yes X No
Are Vegetation <u>No</u> , Soil <u>No</u> , or Hydrology <u>No</u> signifi		
Are Vegetation <u>No</u> , Soil <u>No</u> , or Hydrology <u>No</u> natura		any answers in Remarks.)
SUMMARY OF FINDINGS – Attach site map sho	wing sampling point locations	, transects, important features, etc.
Hydrophytic Vegetation Present?       Yes       X       No         Hydric Soil Present?       Yes       X       No         Wetland Hydrology Present?       Yes       X       No	Is the Sampled Area within a Wetland?	Yes <u>X</u> No
Remarks: Drier than normal site conditions		
HYDROLOGY		
	Sec.	anden (Indiactors (minimum of two volumed)
Wetland Hydrology Indicators: Primary Indicators (minimum of one is required; check all tha	9	condary Indicators (minimum of two required) Surface Soil Cracks (B6)
Surface Water (A1) Aquatic Fau		Sparsely Vegetated Concave Surface (B8)
	ts (B15) (LRR U)	Drainage Patterns (B10)
Saturation (A3)	ulfide Odor (C1)	Moss Trim Lines (B16)
Water Marks (B1) X Oxidized Rh	izospheres on Living Roots (C3)	Dry-Season Water Table (C2)
Sediment Deposits (B2) Presence of	Reduced Iron (C4) X	Crayfish Burrows (C8)
	Reduction in Tilled Soils (C6)	Saturation Visible on Aerial Imagery (C9)
Algal Mat or Crust (B4)Thin Muck S		Geomorphic Position (D2)
	ain in Remarks)	Shallow Aquitard (D3)
Inundation Visible on Aerial Imagery (B7)		FAC-Neutral Test (D5)
Water-Stained Leaves (B9)		Sphagnum Moss (D8) <b>(LRR T, U)</b>
Field Observations:		
	oth (inches):	
	oth (inches):	
Saturation Present? Yes No X De (includes capillary fringe)	oth (inches): Wetland Hydi	rology Present? Yes X No
Describe Recorded Data (stream gauge, monitoring well, aeri	al photos, previous inspections), if availa	ble:
Remarks:		

Sampling Point:

4

<u>Tree Stratum</u> (Plot size: <u>30</u> )	Absolute % Cover	Dominant Species?	Indicator Status	Dominance Test worksheet:	
1				Number of Dominant Species	
2					(A)
3				Total Number of Dominant	
4				Species Across All Strata: 5 (	(B)
5				Percent of Dominant Species	
6.			5	· · · · · · · · · · · · · · · · · · ·	A/B)
7.				Prevalence Index worksheet:	
8				Total % Cover of: Multiply by:	-
		=Total Cover		OBL species         3         x 1 =         3           54000 mmsize         25         22         170	-
50% of total cover:	20%	of total cover:		FACW species $85$ $x 2 =$ $170$ FAC species $2$ $24$	-
Sapling/Shrub Stratum (Plot size: 30)	-	N/ mark	540	FAC species $8 \times 3 = 24$	-
1. <u>Morella cerifera</u>		Yes	FAC	FACU species $4   x 4 = 16$	-
2. Croton capitatus	2	Yes		UPL species $3 \times 5 = 15$	
3. Triadica sebifera	2	Yes	FAC	Column Totals: 103 (A) 228	– ^(B)
4				Prevalence Index = B/A =221	_
5				Hydrophytic Vegetation Indicators:	
6				1 - Rapid Test for Hydrophytic Vegetation	
7	i		. <u> </u>	X 2 - Dominance Test is >50%	
8				X_3 - Prevalence Index is ≤3.0 ¹	
	9	=Total Cover		Problematic Hydrophytic Vegetation ¹ (Explain)	)
50% of total cover: 5	20%	of total cover:	2		
Herb Stratum (Plot size: 30 )					
1. Saccharum giganteum	60	Yes	FACW	¹ Indicators of hydric soil and wetland hydrology mu	ust be
2. Bidens aristosa	25	Yes	FACW	present, unless disturbed or problematic.	
3. Persicaria punctata	3	No	OBL	Definitions of Four Vegetation Strata:	
4. Erigeron annuus	2	No	FACU	Tree – Woody plants, excluding vines, 3 in. (7.6 cr	m) or
5. Paspalum notatum	2	No	FACU	more in diameter at breast height (DBH), regardles	
6. Iva angustifolia	1	No	UPL	height.	
7. Panicum virgatum	1	No	FAC		
8.				Sapling/Shrub – Woody plants, excluding vines, I than 3 in. DBH and greater than 3.28 ft (1 m) tall.	less
9.					
10.					
11.	U.			<b>Herb</b> – All herbaceous (non-woody) plants, regard of size, and woody plants less than 3.28 ft tall.	lless
12.	U.			of size, and woody plants less than 3.20 it tail.	
	94	=Total Cover		Woody Vine – All woody vines greater than 3.28 f	ft in
50% of total cover: 47		of total cover:	19	height.	
Woody Vine Stratum (Plot size: 30 )					
1.					
2.	u U.				
3.	U.				
4.	U.				
5.					
		=Total Cover		Hydrophytic	
50% of total cover:		of total cover:		Vegetation Present? Yes X No	
Remarks: (If observed, list morphological adaptation	s below.)				

Depth	 Matrix	29 NG2261 N72998.	Redo	x Featur	es				i da kana da kena kena den da kata da <b>k</b> ata	
inches)	Color (moist)	%	Color (moist)	%	Type ¹	Loc ²	Te	xture	Remarks	
0-16	10YR 4/2	95	5YR 5/8	5	С	PL/M	Loam	y/Clayey	Prominent redox concentrati	ons
Hydric Soil Histosol Histic Er Black Hi Hydroge Stratifier Organic 5 cm Mu Muck Pr 1 cm Mu Depleter Thick Da Coast P Sandy M Sandy R	oncentration, D=Deple Indicators: (Applicat (A1) bipedon (A2) stic (A3) in Sulfide (A4) d Layers (A5) Bodies (A6) (LRR P, icky Mineral (A7) (LR esence (A8) (LRR U) ick (A9) (LRR P, T) d Below Dark Surface ark Surface (A12) rairie Redox (A16) (M fucky Mineral (S1) (Ll Sleyed Matrix (S4) Redox (S5)	ble to all T, U) R P, T, U) (A11) LRA 150/	LRRs, unless othe Thin Dark Si Barrier Islan (MLRA 15 Loamy Muck Loamy Gley X Depleted Ma Redox Dark Depleted Da Redox Depri Marl (F10) (I Depleted Oc	erwise n urface (S ds 1 cm 3 <b>B, 153</b> cy Miner ed Matrii atrix (F3) Surface rk Surfa essions LRR U) chric (F1 esse Ma ace (F13 (F17) (I rtic (F18	noted.) S9) (LRR Muck (S D) al (F1) (L x (F2) (F6) (F6) (F6) (F8) 1) (MLRA Sses (F12 3) (LRR F MLRA 15 3) (MLRA	S, T, U) 12) RR O) 2) (LRR C 2) (LRR C 2, T, U) 1) 150A, 15	0B)	Indicators fo 1 cm Mu 2 cm Mu Coast Pr (outsid Piedmon Anomalo (MLRA Very Sha (outsid Barrier Is (MLRA	L=Pore Lining, M=Matrix. or Problematic Hydric Soils ³ : ck (A9) (LRR O) ck (A10) (LRR S) rairie Redox (A16) de MLRA 150A) I Vertic (F18) de MLRA 150A, 150B) It Floodplain Soils (F19) (LRR F bus Bright Floodplain Soils (F20 A 153B) ent Material (F21) allow Dark Surface (F22) de MLRA 138, 152A in FL, 154 slands Low Chroma Matrix (TS7 A 153B, 153D) xplain in Remarks)	)
Polyvalu	rface (S7) <b>(LRR P, S,</b> e Below Surface (S8)		Anomalous (MLRA 14	9A, 153	C, 153D)		0)		rs of hydrophytic vegetation and	d
(LRR	S, T, U)		Very Shallov (MLRA 13			1000			nd hydrology must be present, s disturbed or problematic.	
Restrictive	Layer (if observed):									
£352	nches):							c Soil Presen	100 100 100 100	

U.S. Army Corps of Engineers WETLAND DETERMINATION DATA SHEET – Atlantic and Gulf Coasta See ERDC/EL TR-10-20; the proponent agency is CECW-	
Project/Site: Champeaux Evans Hotard - St. Louis High City/Cou	ty: Lake Charles/Calcasieu Sampling Date: 10/9/23
Applicant/Owner: Lake Charles Diocese	State: LA Sampling Point: 5
Investigator(s): J.King/L. Demary Section, Town	ship, Range: 23-10S-08W
	ave, convex, none): None Slope (%): 0-1
Subregion (LRR or MLRA): LRR T, MLRA 150A Lat: 485088	Long: 3338829 Datum: UTM NAD 83
Soil Map Unit Name: Mowata-Vidrine (Mt)	NWI classification: None
Are climatic / hydrologic conditions on the site typical for this time of year?	Yes No X (If no, explain in Remarks.)
	If needed, explain any answers in Remarks.)
SUMMARY OF FINDINGS – Attach site map showing sampling p	oint locations, transects, important features, etc.
	mpled Area Netland? Yes <u>No X</u>
Remarks: Drier than normal site conditions	
HYDROLOGY	
Wetland Hydrology Indicators:         Primary Indicators (minimum of one is required; check all that apply)         Surface Water (A1)       Aquatic Fauna (B13)         High Water Table (A2)       Marl Deposits (B15) (LRR U)         Saturation (A3)       Hydrogen Sulfide Odor (C1)         Water Marks (B1)       Oxidized Rhizospheres on Living F         Sediment Deposits (B2)       Presence of Reduced Iron (C4)         Drift Deposits (B3)       Recent Iron Reduction in Tilled Sc         Algal Mat or Crust (B4)       Thin Muck Surface (C7)         Iron Deposits (B5)       Other (Explain in Remarks)         Inundation Visible on Aerial Imagery (B7)         Water-Stained Leaves (B9)         Field Observations:         Surface Water Present?       Yes         No       X       Depth (inches):         Water Table Present?       Yes       No         X       Depth (inches):       (includes capillary fringe)         Describe Recorded Data (stream gauge, monitoring well, aerial photos, previous instance       Instance	Crayfish Burrows (C8)         Saturation Visible on Aerial Imagery (C9)         Geomorphic Position (D2)         Shallow Aquitard (D3)         FAC-Neutral Test (D5)         Sphagnum Moss (D8) (LRR T, U)
Remarks:	

Sampling Point: ____5

<u>Tree Stratum</u> (Plot size: 30)	Absolute % Cover	Dominant Species?	Indicator Status	Dominance Test worksheet:		
1				Number of Dominant Species		
2				That Are OBL, FACW, or FAC:(A)		
3.				Total Number of Dominant		
4				Species Across All Strata: <u>3</u> (B)		
5.				Percent of Dominant Species That Are OBL, FACW, or FAC: 33.3% (A/B)		
6 7.				That Are OBL, FACW, or FAC: <u>33.3%</u> (A/B) Prevalence Index worksheet:		
8.				Total % Cover of: Multiply by:		
· · · · · · · · · · · · · · · · · · ·		=Total Cover		$\frac{1}{\text{OBL species}}  0 \qquad \text{x1} = 0$		
50% of total cover:		of total cover:		FACW species $0 \times 2 = 0$		
Sapling/Shrub Stratum (Plot size: 30 )	2070			FAC species $16 \times 3 = 48$		
1. Croton capitatus	15	Yes	UPL	FACU species $15 \times 4 = 60$		
2. Triadica sebifera	5	Yes	FAC	$\frac{1}{100} + \frac{1}{100} + \frac{1}$		
3.		103	170	Column Totals: 117 (A) 538 (B)		
4.				$\frac{1}{2} \frac{1}{2} \frac{1}$		
5.				Hydrophytic Vegetation Indicators:		
6.		<u> </u>		1 - Rapid Test for Hydrophytic Vegetation		
7.				2 - Dominance Test is >50%		
8.				$3 - Prevalence Index is \leq 3.0^{1}$		
0.		=Total Cover		Problematic Hydrophytic Vegetation ¹ (Explain)		
EQ9/ of total accur:		of total cover:	4			
50% of total cover: <u>10</u> <u>Herb Stratum</u> (Plot size: 30 )	J20%	of total cover.	4			
	70	Vaa				
1. Bothriochloa ischaemum	10	Yes No		¹ Indicators of hydric soil and wetland hydrology must be		
2. Paspalum notatum 3. Andropogon virginicus	10	<u>No</u>	FACU	present, unless disturbed or problematic.		
, , , , , , , , , , , , , , , , , , , ,	5	No	FAC	Definitions of Four Vegetation Strata:		
4. Sporobolus indicus		<u>No</u>	FACU	<b>Tree</b> – Woody plants, excluding vines, 3 in. (7.6 cm) or more in diameter at breast height (DBH), regardless of		
5. Iva annua		No	FAC	height.		
6. <u>Solidago odora</u>		No	UPL			
7				Sapling/Shrub – Woody plants, excluding vines, less		
8.				than 3 in. DBH and greater than 3.28 ft (1 m) tall.		
9.						
10				Herb – All herbaceous (non-woody) plants, regardless		
11				of size, and woody plants less than 3.28 ft tall.		
12		-Tatal Cause		Mander Minnes All warden in a surget at these 2 20 ft in		
EQ9/ of total accord		=Total Cover	20	<b>Woody Vine</b> – All woody vines greater than 3.28 ft in height.		
50% of total cover: 4	9 20%	of total cover:	20			
<u>Woody Vine Stratum</u> (Plot size: <u>30</u> )						
1						
2.						
3.						
4.						
5				Hydrophytic		
=Total Co				Vegetation		
50% of total cover:	20%	of total cover:		Present?         Yes         No         X		
Remarks: (If observed, list morphological adaptation	ns below.)					

0-16 10 Type: C=Concentrati Higtric Soil Indicator: Histosol (A1) Histic Epipedon (A Black Histic (A3) Hydrogen Sulfide Stratified Layers (A	Applicable			e <b>rwise n</b> urface (S ds 1 cm	ioted.) 69) (LRR Muck (S	S, T, U)		Clayey	100016 IS 46 02	
Type: C=Concentrati <b>lydric Soil Indicator</b> Histosol (A1) Histic Epipedon (A Black Histic (A3) Hydrogen Sulfide Stratified Layers (A	on, D=Depleti s: (Applicable	on, RM=R	Reduced Matrix, M Reduced Matrix, M Rs, unless othe Thin Dark Su Barrier Island	AS=Mas prwise m urface (S ds 1 cm	ked Sand oted.) 59) (LRR Muck (S		21	Location: PL= ndicators for 1 cm Muck	Pore Lining, M= Problematic Hy	Matrix.
Histosol (A1) Histic Epipedon (A Black Histic (A3) Hydrogen Sulfide Stratified Layers (A	Applicable		Rs, unless othe Thin Dark Su Barrier Island	e <b>rwise n</b> urface (S ds 1 cm	ioted.) 69) (LRR Muck (S	S, T, U)		ndicators for 1 cm Muck	Problematic Hy	
Organic Bodies (A 5 cm Mucky Miner Muck Presence (A 1 cm Muck (A9) (L Depleted Below D Thick Dark Surfac Coast Prairie Red Sandy Mucky Mine	6) (LRR P, T, ral (A7) (LRR 8) (LRR U) .RR P, T) ark Surface (/ e (A12) ox (A16) (MLI	P, T, U) 	Loamy Muck Loamy Gleye X Depleted Ma Redox Dark Depleted Da Redox Depre Marl (F10) (L Depleted Oc Iron-Mangan Umbric Surfa	y Miner ed Matrii trix (F3) Surface rk Surfa essions <b>.RR U)</b> hric (F1 esse Ma	al (F1) <b>(L</b> x (F2) (F6) ce (F7) (F8) 1) <b>(MLR</b> sses (F1:	4 151) 2) (LRR O		Coast Prain (outside Reduced V (outside Piedmont F Anomalous (MLRA 1 Red Paren Very Shallo (outside	MLRA 150A, 15 Floodplain Soils Bright Floodpla	50 <b>B)</b> (F19) <b>(LRR P, T</b> iin Soils (F20) : (F22) 2 <b>A in FL, 154)</b>
Sandy Gleyed Matrix (S4) Delta Ochric (F17) (MLRA				WLRA 15	51)					
Sandy Redox (S5) Reduced Vertic (F18) (MLRA 150A,					150A, 15	i0B)	Other (Exp	lain in Remarks)	)	
Stripped Matrix (S	6)	_	Piedmont Flo	oodplain	Soils (F	19) <b>(MLR</b> /	A 149A)			
Dark Surface (S7)	(LRR P, S, T	; U) _	Anomalous I	Bright Fl	oodplain	Soils (F20	0)			
Polyvalue Below S	Surface (S8)		(MLRA 14		16 17 July 1				of hydrophytic v	52
(LRR S, T, U)		-	Very Shallov (MLRA 13)			17/10			hydrology must listurbed or prob	5 5

## ATTACHMENT D

Site Photographs



Photograph 1 Sample Plot 1



Photograph 2 General View of Plot 1 Facing North



Photograph 3 General View of Plot 1 Facing East



Photograph 4 General View of Plot 1 Facing South



Photograph 5 General View of Plot 1 Facing West



Photograph 6 Sample Plot 2



Photograph 7 General View of Plot 2 Facing North



Photograph 8 General View of Plot 2 Facing East



Photograph 9 General View of Plot 2 Facing South



Photograph 10 General View of Plot 2 Facing West



Photograph 11 Sample Plot 3



Photograph 12 General View of Plot 3 Facing North



Photograph 13 General View of Plot 3 Facing East



Photograph 14 General View of Plot 3 Facing South



Photograph 15 General View of Plot 3 Facing West



Photograph 16 Sample Plot 4



Photograph 17 General View of Plot 4 Facing North



Photograph 18 General View of Plot 4 Facing East



Photograph 19 General View of Plot 4 Facing South



Photograph 20 General View of Plot 4 Facing West



Photograph 21 Sample Plot 5



Photograph 22 General View of Plot 5 Facing North



Photograph 23 General View of Plot 5 Facing East



Photograph 24 General View of Plot 5 Facing South



Photograph 25 General View of Plot 5 Facing West

APPENDIX 5. EPA Sole Source Aquifer Program Response Letter



December 12, 2023

Ms. Tiffany Spann-Winfield Deputy EHP Program Lead, Environmental Liaison Officer FEMA-DR 4559 LA / Louisiana Integration and Recovery Office 1500 Main Street Baton Rouge, LA 70802

Dear Ms. Spann-Winfield:

We have received your December 4, 2023, letter requesting our evaluation of the potential environmental impacts which might result from the following project:

Propose Roman Catholic Church/Diocese of Lake Charles, Replace/Rebuild: St. Louis High School Facilities in Alternative Location, Funded By The Federal Emergency Management Agency (FEMA), (PW#s 1265, 2284, 2495 FEMA-DR-4559-LA) /// General Area: (30.181700, -93.158600), 47 Acres, Near Intersection: James Court & Corbina Road, Lake Charles, Calcasieu Parish, LA 70615

The project funded by the Federal Emergency Management Agency (FEMA), is located on the Chicot aquifer system which has been designated a sole source aquifer (SSA) by the EPA. Based on the information provided for the project, we have determined that the project, as proposed, should not have an adverse effect on the quality of the ground water underlying the project site.

This approval of the proposed project does not relieve the applicant from adhering to other State and Federal requirements, which may apply. This approval is based solely upon the potential impact to the quality of ground water as it relates to the EPA's authority pursuant to Section 1424(e) of the Safe Drinking Water Act.

EPA intends to evaluate and respond to all projects submitted for formal review or evaluation purposes within forty-five (45) calendar days, from the Stamped Date the project is received by the EPA. However, if EPA is unable to complete its review within that timeframe, no assumption of a determination of a lack of impacts can be made. EPA acknowledges our approval is not required by law for the project to proceed with funding.

If you did not include the parish, project description, project location, area map, plat or the federal funding agency, please do so in future SSA correspondence.

If you have any questions on this letter or the SSA program please contact me at (214) 665-8485.

Sincerely yours Omar T. Martinez, Coordinator Sole Source Aquifer Program Ground Water/UIC Section

cc: Jesse Means, LDEQ Lead Environmental Protection Specialist | FEMA | EHP | LIRO, Region 6

#### **Date: December 12, 2023**

#### FYI: We have moved and have a New Address & Mail Code, please see below.

Omar T. Martinez, Environmental Scientist Sole Source Aquifer Program Coordinator Ground Water/UIC Section (Mail Code: WDDG) U.S. Environmental Protection Agency, Region 6 1201 Elm Street, Suite 500 Dallas, Texas 75270 APPENDIX 6. U.S. Fish & Wildlife Service Consultation Letter, Species List Louisiana Ecological Services Field Office, and NE Consistency Letter_ Louisiana Endangered Species Act project



## United States Department of the Interior

FISH AND WILDLIFE SERVICE Louisiana Ecological Services Field Office 200 Dulles Drive Lafayette, LA 70506 Phone: (337) 291-3100 Fax: (337) 291-3139



In Reply Refer To: Project Code: 2024-0004556 Project Name: St. Louis High School Relocation October 13, 2023

Subject: List of threatened and endangered species that may occur in your proposed project location or may be affected by your proposed project

To Whom It May Concern:

The enclosed species list identifies threatened, endangered, and candidate species, as well as designated and proposed critical habitat that may occur within the boundary of your proposed project and may be affected by your proposed project. The Fish and Wildlife Service (Service) is providing this list under section 7 (c) of the Endangered Species Act (Act) of 1973, as amended (16 U.S.C. 1531 et seq.). Changes in this species list may occur due to new information from updated surveys, changes in species habitat, new listed species and other factors. Because of these possible changes, feel free to contact our office (337-291-3109) for more information or assistance regarding impacts to federally listed species. The Service recommends visiting the IPaC site or the Louisiana Ecological Services Field Office website (https://www.fws.gov/ southeast/lafayette) at regular intervals during project planning and implementation for updated species lists and information. An updated list may be requested through the IPaC system by completing the same process used to receive the enclosed list.

The purpose of the Act is to provide a means whereby threatened and endangered species and the habitats upon which they depend may be conserved. Under sections 7(a)(1) and 7(a)(2) of the Act and its implementing regulations (50 CFR 402 et seq.), Federal agencies are required to utilize their authorities to carry out programs for the conservation of Federal trust resources and to determine whether projects may affect Federally listed species and/or designated critical habitat.

A Biological Assessment is required for construction projects (or other undertakings having similar physical impacts) that are major Federal actions significantly affecting the quality of the human environment as defined in the National Environmental Policy Act (42 U.S.C. 4332(2) (c)).

Bald eagles have recovered and were removed from the List of Endangered and Threatened Species as of August 8, 2007. Although no longer listed, please be aware that bald eagles are protected under the Bald and Golden Eagle Protection Act (BGEPA) (16 U.S.C. 668 et seq.).

The Service developed the National Bald Eagle Management (NBEM) Guidelines to provide landowners, land managers, and others with information and recommendations to minimize potential project impacts to bald eagles, particularly where such impacts may constitute "disturbance", which is prohibited by the BGEPA. A copy of the NBEM Guidelines is available at: https://www.fws.gov/migratorybirds/pdf/management/ nationalbaldeaglenanagementguidelines.pdf

Those guidelines recommend: (1) maintaining a specified distance between the activity and the nest (buffer area); (2) maintaining natural areas (preferably forested) between the activity and nest trees (landscape buffers); and (3) avoiding certain activities during the breeding season. Onsite personnel should be informed of the possible presence of nesting bald eagles within the project boundary, and should identify, avoid, and immediately report any such nests to this office. If a bald eagle nest occurs or is discovered within or adjacent to the proposed project area, then an evaluation must be performed to determine whether the project is likely to disturb nesting bald eagles. That evaluation may be conducted on-line at: https://www.fws.gov/ southeast/our-services/eagle-technical-assistance/. Following completion of the evaluation, that website will provide a determination of whether additional consultation is necessary. The Division of Migratory Birds for the Southeast Region of the Service (phone: 404/679-7051, e-mail: SEmigratorybirds@fws.gov) has the lead role in conducting any necessary consultation.

Activities that involve State-designated scenic streams and/or wetlands are regulated by the Louisiana Department of Wildlife and Fisheries and the U.S. Army Corps of Engineers, respectively. We, therefore, recommend that you contact those agencies to determine their interest in proposed projects in these areas.

Activities that would be located within a National Wildlife Refuge are regulated by the refuge staff. We, therefore, recommend that you contact them to determine their interest in proposed projects in these areas.

Additional information on Federal trust species in Louisiana can be obtained from the Louisiana Ecological Services website at: https://www.fws.gov/southeast/lafayette

We appreciate your concern for threatened and endangered species. The Service encourages Federal agencies to include conservation of threatened and endangered species into their project planning to further the purposes of the Act. Please include the Consultation Tracking Number in the header of this letter with any request for consultation or correspondence about your project that you submit to our office.

Attachment(s):

- Official Species List
- USFWS National Wildlife Refuges and Fish Hatcheries
- Bald & Golden Eagles
- Migratory Birds

# **OFFICIAL SPECIES LIST**

This list is provided pursuant to Section 7 of the Endangered Species Act, and fulfills the requirement for Federal agencies to "request of the Secretary of the Interior information whether any species which is listed or proposed to be listed may be present in the area of a proposed action".

This species list is provided by:

Louisiana Ecological Services Field Office 200 Dulles Drive Lafayette, LA 70506 (337) 291-3100

### **PROJECT SUMMARY**

Project Code:	2024-0004556
Project Name:	St. Louis High School Relocation
Project Type:	New Constr - Above Ground
Project Description:	The applicant proposes to replace the St. Louis High School Old Gym and
	Main Building by relocating and rebuilding the facilities. The proposed
	location has been identified as approximately 47 acres located east of the
	intersection of Corbina Road and James Court in Lake Charles, (30.1817,
	-93.1586).
<b>Б</b> ( ), <b>Т</b> ( ),	

#### Project Location:

The approximate location of the project can be viewed in Google Maps: <u>https://www.google.com/maps/@30.181656500000003,-93.15587125789477,14z</u>



Counties: Calcasieu County, Louisiana
## **ENDANGERED SPECIES ACT SPECIES**

There is a total of 4 threatened, endangered, or candidate species on this species list.

Species on this list should be considered in an effects analysis for your project and could include species that exist in another geographic area. For example, certain fish may appear on the species list because a project could affect downstream species.

IPaC does not display listed species or critical habitats under the sole jurisdiction of NOAA Fisheries¹, as USFWS does not have the authority to speak on behalf of NOAA and the Department of Commerce.

See the "Critical habitats" section below for those critical habitats that lie wholly or partially within your project area under this office's jurisdiction. Please contact the designated FWS office if you have questions.

1. <u>NOAA Fisheries</u>, also known as the National Marine Fisheries Service (NMFS), is an office of the National Oceanic and Atmospheric Administration within the Department of Commerce.

#### BIRDS

NAME	STATUS		
Red-cockaded Woodpecker <i>Picoides borealis</i> No critical habitat has been designated for this species. Species profile: <u>https://ecos.fws.gov/ecp/species/7614</u>	Endangered		
Whooping Crane <i>Grus americana</i> Population: U.S.A (Southwestern Louisiana) No critical habitat has been designated for this species. Species profile: <u>https://ecos.fws.gov/ecp/species/758</u>	Experimental Population, Non- Essential		
REPTILES NAME	STATUS		
Alligator Snapping Turtle <i>Macrochelys temminckii</i> No critical habitat has been designated for this species. Species profile: <u>https://ecos.fws.gov/ecp/species/4658</u>	Proposed Threatened		
INSECTS NAME	STATUS		
Monarch Butterfly Danaus plexippus No critical habitat has been designated for this species. Species profile: <u>https://ecos.fws.gov/ecp/species/9743</u>	Candidate		

### **CRITICAL HABITATS**

THERE ARE NO CRITICAL HABITATS WITHIN YOUR PROJECT AREA UNDER THIS OFFICE'S JURISDICTION.

YOU ARE STILL REQUIRED TO DETERMINE IF YOUR PROJECT(S) MAY HAVE EFFECTS ON ALL ABOVE LISTED SPECIES.

# USFWS NATIONAL WILDLIFE REFUGE LANDS AND FISH HATCHERIES

Any activity proposed on lands managed by the <u>National Wildlife Refuge</u> system must undergo a 'Compatibility Determination' conducted by the Refuge. Please contact the individual Refuges to discuss any questions or concerns.

THERE ARE NO REFUGE LANDS OR FISH HATCHERIES WITHIN YOUR PROJECT AREA.

## **BALD & GOLDEN EAGLES**

Bald and golden eagles are protected under the Bald and Golden Eagle Protection Act¹ and the Migratory Bird Treaty Act².

Any person or organization who plans or conducts activities that may result in impacts to bald or golden eagles, or their habitats³, should follow appropriate regulations and consider implementing appropriate conservation measures, as described below.

- 1. The Bald and Golden Eagle Protection Act of 1940.
- 2. The Migratory Birds Treaty Act of 1918.
- 3. 50 C.F.R. Sec. 10.12 and 16 U.S.C. Sec. 668(a)

#### There are bald and/or golden eagles in your project area.

For guidance on when to schedule activities or implement avoidance and minimization measures to reduce impacts to migratory birds on your list, click on the PROBABILITY OF PRESENCE SUMMARY at the top of your list to see when these birds are most likely to be present and breeding in your project area.

NAME	BREEDING SEASON
Bald Eagle Haliaeetus leucocephalus	Breeds Sep 1 to
This is not a Bird of Conservation Concern (BCC) in this area, but warrants attention	Jul 31
because of the Eagle Act or for potential susceptibilities in offshore areas from certain	
types of development or activities.	
https://ecos.fws.gov/ecp/species/1626	

## **PROBABILITY OF PRESENCE SUMMARY**

The graphs below provide our best understanding of when birds of concern are most likely to be present in your project area. This information can be used to tailor and schedule your project activities to avoid or minimize impacts to birds. Please make sure you read the supplemental information and specifically the FAQ "Proper Interpretation and Use of Your Migratory Bird Report" before using or attempting to interpret this report.

#### Probability of Presence (

Green bars; the bird's relative probability of presence in the 10km grid cell(s) your project overlaps during that week of the year.

#### Breeding Season (=)

Yellow bars; liberal estimate of the timeframe inside which the bird breeds across its entire range.

#### Survey Effort ()

Vertical black lines; the number of surveys performed for that species in the 10km grid cell(s) your project area overlaps.

#### No Data (-)

A week is marked as having no data if there were no survey events for that week.



Additional information can be found using the following links:

- Eagle Managment https://www.fws.gov/program/eagle-management
- Measures for avoiding and minimizing impacts to birds <u>https://www.fws.gov/library/</u> <u>collections/avoiding-and-minimizing-incidental-take-migratory-birds</u>
- Nationwide conservation measures for birds <u>https://www.fws.gov/sites/default/files/</u> <u>documents/nationwide-standard-conservation-measures.pdf</u>
- Supplemental Information for Migratory Birds and Eagles in IPaC <u>https://www.fws.gov/media/supplemental-information-migratory-birds-and-bald-and-golden-eagles-may-occur-project-action</u>

## **MIGRATORY BIRDS**

Certain birds are protected under the Migratory Bird Treaty Act¹ and the Bald and Golden Eagle Protection Act².

Any person or organization who plans or conducts activities that may result in impacts to migratory birds, eagles, and their habitats³ should follow appropriate regulations and consider implementing appropriate conservation measures, as described below.

- 1. The Migratory Birds Treaty Act of 1918.
- 2. The Bald and Golden Eagle Protection Act of 1940.
- 3. 50 C.F.R. Sec. 10.12 and 16 U.S.C. Sec. 668(a)

For guidance on when to schedule activities or implement avoidance and minimization measures to reduce impacts to migratory birds on your list, click on the PROBABILITY OF PRESENCE SUMMARY at the top of your list to see when these birds are most likely to be present and breeding in your project area.

NAME	BREEDING SEASON
American Golden-plover <i>Pluvialis dominica</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/10561</u>	Breeds elsewhere
Bald Eagle Haliaeetus leucocephalus This is not a Bird of Conservation Concern (BCC) in this area, but warrants attention because of the Eagle Act or for potential susceptibilities in offshore areas from certain types of development or activities. https://ecos.fws.gov/ecp/species/1626	Breeds Sep 1 to Jul 31
Chimney Swift Chaetura pelagica This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. https://ecos.fws.gov/ecp/species/9406	Breeds Mar 15 to Aug 25
Dickcissel <i>Spiza americana</i> This is a Bird of Conservation Concern (BCC) only in particular Bird Conservation Regions (BCRs) in the continental USA <u>https://ecos.fws.gov/ecp/species/9453</u>	Breeds May 5 to Aug 31
Gull-billed Tern <i>Gelochelidon nilotica</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/9501</u>	Breeds May 1 to Jul 31

NAME	BREEDING SEASON
King Rail <i>Rallus elegans</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/8936</u>	Breeds May 1 to Sep 5
Lesser Yellowlegs <i>Tringa flavipes</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/9679</u>	Breeds elsewhere
Painted Bunting Passerina ciris This is a Bird of Conservation Concern (BCC) only in particular Bird Conservation Regions (BCRs) in the continental USA https://ecos.fws.gov/ecp/species/9511	Breeds Apr 25 to Aug 15
Pectoral Sandpiper <i>Calidris melanotos</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/9561</u>	Breeds elsewhere
Red-headed Woodpecker <i>Melanerpes erythrocephalus</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/9398</u>	Breeds May 10 to Sep 10
Swallow-tailed Kite <i>Elanoides forficatus</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/8938</u>	Breeds Mar 10 to Jun 30
Willet <i>Tringa semipalmata</i> This is a Bird of Conservation Concern (BCC) throughout its range in the continental USA and Alaska. <u>https://ecos.fws.gov/ecp/species/10669</u>	Breeds Apr 20 to Aug 5

## **PROBABILITY OF PRESENCE SUMMARY**

The graphs below provide our best understanding of when birds of concern are most likely to be present in your project area. This information can be used to tailor and schedule your project activities to avoid or minimize impacts to birds. Please make sure you read the supplemental information and specifically the FAQ "Proper Interpretation and Use of Your Migratory Bird Report" before using or attempting to interpret this report.

#### **Probability of Presence** (**■**)

Green bars; the bird's relative probability of presence in the 10km grid cell(s) your project overlaps during that week of the year.

#### Breeding Season (=)

Yellow bars; liberal estimate of the timeframe inside which the bird breeds across its entire range.

#### Survey Effort ()

Vertical black lines; the number of surveys performed for that species in the 10km grid cell(s) your project area overlaps.

#### No Data (–)

A week is marked as having no data if there were no survey events for that week.

		<b>p</b> robabi	lity of presend	ce breeding s	season survey	y effort — no data
SPECIES American Golden- plover BCC Rangewide (CON)	JAN FEB MA		AY JUN +++ -++-	JUL AUG	SEP OCT	NOV DEC + ++ +++++
Bald Eagle Non-BCC Vulnerable	<u> </u> +++ <u> </u> +++ +-	++++++	• • • • • • • •			+ + • • • <u>I</u> + • + <u>I</u>
Chimney Swift BCC Rangewide (CON)	+++++++++++++++++++++++++++++++++++++++	+++++	+ 1 + - 1 +			+ ++ +++++
Dickcissel BCC - BCR	++++ ++++ +-	++ +	• 1 1 - 1 1 -	1 I		+ ++ ++++
Gull-billed Tern BCC Rangewide (CON)	++++ ++++ +-	·++ <b>I</b> -++ <mark>+</mark>			+-+++++++++++++++++++++++++++++++++	+ ++ ++++
King Rail BCC Rangewide (CON)	++++ + <mark>1</mark> ++ +-	+	• + + • • •	• • • • • • • •	· · + + + + + + + + + + + + + + + + + +	+ + <mark> </mark> ++++
Lesser Yellowlegs BCC Rangewide (CON)	<b>*</b> +++ ++++ + <b>-</b>	++++	· ++ -++-		+++ ++++	+ ++ ++ <b>    </b>
Painted Bunting BCC - BCR	++++ ++++ +-	++ +-+ <mark>+</mark> [		••	· · · · · · · · · · · · · · · · · · ·	+ ++ ++++
Pectoral Sandpiper BCC Rangewide (CON)	++++ ++++ +-	+	+++++-	- + + + +		+ ++ ++++
Red-headed Woodpecker BCC Rangewide (CON)	∎+++ ++++ +-	++ +- 1 1 +	• + 1 - + + -		· · · · · · · · · · · · · · · · · · ·	+ ++ ++++
Swallow-tailed Kite	· ++++ ++++ I	+++++++		++++	+ + + + +	+ ++ ++++

BCC Rangewide (CON)

Additional information can be found using the following links:

- Eagle Management https://www.fws.gov/program/eagle-management
- Measures for avoiding and minimizing impacts to birds <u>https://www.fws.gov/library/</u> <u>collections/avoiding-and-minimizing-incidental-take-migratory-birds</u>
- Nationwide conservation measures for birds <u>https://www.fws.gov/sites/default/files/</u> <u>documents/nationwide-standard-conservation-measures.pdf</u>
- Supplemental Information for Migratory Birds and Eagles in IPaC <u>https://www.fws.gov/media/supplemental-information-migratory-birds-and-bald-and-golden-eagles-may-occur-project-action</u>

## **IPAC USER CONTACT INFORMATION**

- Agency: Federal Emergency Management Agency
- Name: Gunnar Muckelberg
- Address: 500 C St SW, Washington, DC 20472
- City: Washington
- State: DC
- Zip: 20472
- Email gunnar.muckelberg@associates.fema.dhs.gov
- Phone: 2256035967

**U.S. Department of Homeland Security** Federal Emergency Management Agency Louisiana Integration and Recovery Office 1500 Main Street Baton Rouge, LA 70802



September 16, 2020

Joseph Ranson Field Supervisor U.S. Fish & Wildlife Service 200 Dulles Drive Lafayette, LA 70506

Dear Mr. Ranson,

The President of the United States issued a Major Disaster Declaration FEMA 4559-DR-LA (Declaration) (3538-EM-LA) on August 28, 2020 (Amendment No. 1 signed on August 30, 2020; Amendment No. 2 signed on August 31, 2020; Amendment No. 3 signed on September 1, 2020, Amendment No. 4 signed on September 5, 2020; Amendment No. 5 signed September 7, 2020; Amendment No. 6 signed September 9, 2020, Amendment No. 7 signed September 11, 2020; Amendment No. 8 September 12, 2020) for the damages caused by Hurricane Laura in Louisiana that occurred from August 22, 2020 to August 27, 2020. The Federal Emergency Management Agency (FEMA) will provide federal funds authorized under the Robert T. Stafford Disaster Relief and Emergency Assistance Act, 42 U.S.C. §§5121-5207 *et. seq.*, (P.L. 93-288, as amended). These FEMA funds are available to eligible state, tribal, and local governments as well as certain eligible Private Non-Profit (PNP) organizations (sub-recipients).

The Declaration authorizes Individual Assistance funding for assistance to individuals and households for eligible Sub-recipients within the following parishes: Acadia, Allen, Beauregard, Calcasieu, Cameron, Grant, Jackson, Jefferson Davis, Lincoln, Natchitoches, Ouachita, Rapides, Sabine, Vermilion, Vernon, and Winn Parish.

The Declaration authorizes Public Assistance funding for emergency work, the repair or replacement of disaster-damaged facilities, and improved or alternate projects beyond the predisaster condition for eligible Applicants within the following parishes: Allen, Beauregard, Calcasieu, Cameron, Jefferson Davis, and Vernon for Public Assistance Category A (debris removal) and all parishes for Public Assistance Category **B** (emergency protective measures), including direct Federal assistance.

Bienville, Catahoula, and Sabine Parishes for debris removal [Category A (already designated for emergency protective measures [Category B, including direct federal assistance, under the Public Assistance program) for Jackson, Lincoln, and Rapides Parishes for debris removal [Category A (already designated for Individual Assistance and emergency protective measures [Category B, including direct federal assistance, under the Public Assistance program) Additional parishes may be designated for assistance at a later date and FEMA will notify your office at that time.

The Declaration authorizes Public Assistance [Categories C-G] for Allen, Beauregard, Calcasieu, Cameron, Jefferson Davis, and Vernon Parishes for Public Assistance [Categories C-G] (already designated for Individual Assistance and assistance for debris removal and emergency protective measures [Categories A and B], including direct federal assistance, under the Public Assistance program.

The Declaration also authorizes Acadia, Grant, Natchitoches, Vermilion, and Winn Parishes for Public Assistance [Category A] (already designated for Individual Assistance and assistance for emergency protective measures [Category B], including direct federal assistance, under the Public Assistance program) and Morehouse and Union Parishes for Individual Assistance (already designated for emergency protective measures [Category B), including direct federal assistance, under the Public Assistance for emergency protective measures [Category B), including direct federal assistance, under the Public Assistance program.

Caddo, La Salle, and St. Landry Parishes for Individual Assistance (already designated for emergency protective measures [Category B], including direct federal assistance, under the Public Assistance program).

Under FEMA 4559-DR-LA, sub-recipients in all jurisdictions in the State of Louisiana are eligible for funding under Section 404 of FEMA's Hazard Mitigation Grant Program (HMGP). Eligible Section 404 HMGP projects include acquisition of hazard-prone property, retrofitting existing buildings and facilities, elevation of flood-prone structures, infrastructure protection measures, drainage projects, wildfire mitigation projects, individual and community safe rooms, and nonstructural measures such as planning. Should a sub-recipient propose a project outside of a declared jurisdiction, FEMA will contact you for initial information on that Parish as appropriate.

The Endangered Species Act of 1973, 16 U.S.C. §1531 *et seq.*, P.L. 93-205, as amended, requires federal agencies to determine the effects of their actions on threatened and endangered (T&E) species of fish, wildlife, plants, and their critical habitat, and take steps to conserve and protect these species.

FEMA requests informal consultation with the U.S. Fish & Wildlife Service (USFWS) in accordance with Section 7 of the Endangered Species Act of 1973 (87 Stat.884, as amended); E.O. 13186, Migratory Bird Treaty Act (16 U.S.C. 703-711); Fish and Wildlife Coordination Act (48 Stat. 401, as amended; 16 U.S.C. 661 et seq.); Clean Water Act of 1972 (33 U.S.C. 1344); National Environmental Policy Act of 1969 (83 Stat. 852; 42 U.S.C. 4321 et seq.); and the Coastal Barrier Resources Act of 1982 (96 Stat. 1653; 16 U.S.C. 3501 et seq.) to assist FEMA in determining potential project impacts.

In emergency situations in designated parishes, some projects will have already taken place to protect the health and safety of the public. Most of the permanent repair projects in these parishes will typically restore the damaged facility to its pre-disaster footprint and condition. The majority of the projects for this disaster will be repairs to buildings, equipment, utilities, and debris disposal activities.

Initial Disaster Notification 4559-DR-LA September 18, 2020

FEMA Public Assistance has divided disaster-related work into two broad Categories of Work: Emergency and Permanent Work. These categories are further divided into seven categories. FEMA's past experience with recovery projects in the State of Louisiana allows us to anticipate no adverse effects to T&E species for the majority of projects in the following categories.

In cases where the recovery work requires additional efforts with potential to impact T&E species or habitat, our office will make an initial determination of effect and seek concurrence with your office on that determination prior to proceeding with federal funding.

- A. Debris Removal and Disposal (Emergency Work) this involves the clearance of trees and woody debris; building components or contents; sand, mud, silt, and gravel; and disaster related wreckage.
  - a. Vegetative Debris
    - 1. Debris placed by the curbside from private property will be collected, and generally taken to a staging site and then disposed by chipping, hauling to a landfill or occasionally burned under a Louisiana Department of Environmental Quality (LDEQ) burn permit. Root balls will be left in place unless they present a safety hazard. Some sub-applicants compost the chips into mulch, which is either sold or available for residents.
    - 11. In parks, most vegetative debris that will be removed with FEMA funds is located along trails and in improved and pre-disturbed areas such as campgrounds, day-use areas, parking lots, and picnic areas. Debris along trails will generally be moved to the side of the trail and left in place to decompose. Debris in the improved areas will generally be hauled away to a staging site or disposed of by chipping and spreading.
    - 111. FEMA does not fund any actions on federal property under the PA Program with the exception of emergency debris removal from Federal Highway Administration roads.
    - FEMA does not normally fund removal of debris in undeveloped areas or streams, except within 50 feet upstream of structures. If FEMA does become involved with vegetative debris removal from streams or riparian areas, we will consult with your office as appropriate.
  - b. Construction and Other Non-Vegetative Debris
    - 1. To be eligible for reimbursement from FEMA under the PA Program, the sub-applicant must dispose of all waste materials resulting from projects, such as construction and demolition debris, silt, excess dirt, or overburden in an approved landfill. Other disposal options, such as burning, burying, and stockpiling, shall comply with the LDEQ standards and requirements.

11. FEMA will recommend that channel work in permanent streams be avoided as much as possible. FEMA will also recommend that debris removal from streams should be conducted from the stream bank whenever possible.

Therefore, FEMA will likely make a "No Effect" determination for the majority of these projects. However, FEMA is aware of critical habitats and potential species presence in certain sensitive areas (parks, waterways, springs, etc.) and if a project arises that has the potential to affect T&E species or habitat, FEMA will contact your office for advice and/or further consultation.

B. Emergency Protective Measures (Emergency Work)- Emergency protective measures are those activities undertaken by a community before, during, and following a disaster. Generally, this includes actions such as sheltering displaced disaster victims, activating Office of Emergency Management operations, and compensating police and fire departments for overtime. Occasionally an emergency berm or sandbags may be placed to prevent flooding, and these temporary structures are removed as part of FEMA funding.

FEMA will likely make a "No Effect" determination for Emergency Protective Measure projects. However, if a project arises that has the potential to affect T&E species and/or critical habitat, FEMA will contact your office for advice and/or further consultation.

- C. Roads and Bridges (Permanent Work)- this involves roads, bridges, and associated facilities (e.g., auxiliary structures, lighting, and signage).
  - a. Most work in this category will be for the repair of existing roads within the footprint of the right of way.
  - b. FEMA will recommend only using staging areas in previously disturbed sites and existing road rights-of-way.
  - c. Work conducted in water, such as repair or replacement of culverts or bridges and wing-wall and wing-wall protection would proceed through the normal permitting process, and any culvert that is upgraded beyond one size will be evaluated with a hydrology and hydraulics study to determine potential downstream effects.
  - d. FEMA does not typically fund erosion control measures in streams involving replacement of riprap and repair of material on a stream bank unless those measures would protect improved property such as a dam, bridge, or road.

Therefore, FEMA will likely make a "No Effect" determination for these projects. However, if a project arises that has the potential to affect T&E species or habitat, FEMA will contact your office for advice and/or further consultation.

D. Water and Water Control Facilities - this involves dams and reservoirs; levees, lined and unlined engineered drainage channels; canals, aqueducts, sediment basins, shore protective devices, some irrigation facilities, and pumping facilities.

a. While FEMA does not anticipate many projects in this category under funding requests from FEMA 4559-DR-LA, if such requests are received, the application would be evaluated and FEMA will consult with USFWS if any potential sensitive species issues are identified.

E. Buildings and Equipment (Permanent Work) - this involves buildings, structural components, interior systems such as electrical or mechanical work, equipment, and contents including furnishings.

- a. Normally repairs to buildings and equipment will occur within the footprint of the structure.
- b. FEMA will recommend only using staging areas in a previously disturbed sites and existing rights-of-way.

Therefore, FEMA will likely make a "No Effect" determination for these projects. However, if a project arises that has the potential to affect T&E species or habitat, FEMA will contact your office for advice and/or further consultation.

- F. Utilities (Permanent Work) this involves water treatment plants and delivery systems; power generation and distribution facilities; including natural gas systems, wind turbines, generators, substations, and power lines; sewage collection systems and treatment plants; and communications.
  - a. Normally projects in Category Fare repair to pre-disaster condition within existing rights-of-way.

Therefore, FEMA will likely make a "No Effect" determination for these projects. However, if a project arises that has the potential to affect T&E species or habitat, FEMA will contact your office for advice and/or further consultation.

- G. Parks, Recreation, and other (Permanent Work) this involves mass transit facilities such as railways, swimming pools, bath houses, tennis courts, boat docks, piers, picnic tables, golf courses, fish hatcheries, and facilities that do not fit Categories C-F.
  - a. Most funding requests in this category are structure repairs, such as a roof on a gazebo, and would not impact sensitive species. FEMA does not anticipate many projects in this category under funding requests from FEMA 4559-DR-LA.

Therefore, FEMA will likely make a "No Effect" determination for these projects.

The attached list references the USFWS list of federally listed threatened, endangered, and proposed species provided by the USFWS via the Information, Planning, and Conservation (IPaC) System (*http://ecos.fws.gov/ipac/*). In addition, each project will be checked for proximity to critical habitat based on the IPaC System and the USFWS Critical Habitat Portal (*http://ecos.fws.gov/crithab/*) to determine if additional consultation with USFWS is necessary.

Initial Disaster Notification 4559-DR-LA September 18, 2020

FEMA will utilize this list in making its determinations. According to the attached list, there are no critical habitats established within the declared area. Louisiana is also located with the Mississippi flyway region for Migratory Birds.

FEMA hereby requests any additional information from your office including any updates to the IPaC species list and critical habitat designations, Migratory Birds; and Bald Eagles for the above listed Parishes or on any special concerns that USFWS has regarding FEMA's proposed work in these areas.

In some cases, FEMA may be funding an activity that has already undergone Section 7 consultation through another federal agency. For instance, the U.S. Army Corps of Engineers may have issued an individual Clean Water Act permit to cover certain activities along beaches and in other waters of the U.S.

The issuance of a permit may have required informal or formal consultation with the USFWS and the resulting terms and conditions are incorporated into the permit requirements.

In cases like this where there is an existing consultation agreement between USFWS and another federal agency; where that other federal agency is playing a regulatory or other role in the approval or implementation of the FEMA-funded project; where the FEMA-funded activity aligns with the activity described in the other agency's Section 7 consultation; and where the consultation or permit is not expired; it is FEMA's intent to adopt the other federal agency's Section 7 consultation, including all avoidance and minimization measures and terms and conditions that resulted from that consultation, without further notification to USFWS.

FEMA believes this approach furthers Congress's intent in creating the Unified Federal Review process for which FEMA and DOI are signatory agencies (Section 429 of the Stafford Act).

Thank you in advance for your assistance. Should you have any questions, please contact Tiffany Spann-Winfield at 504-218-6800 or <u>tiffany.spann@fema.dhs.gov</u> or Jerame Cramer at (504) 247-7771 or jerame.cramer@fema.dhs.gov.

Sincerely, JERAME J CRAMER Jerame J. Cramer EHP Advisor DR-4559-LA FEMA Region 6 Louisiana Integration & Recovery Office 1500 Main St. Baton Rouge, LA 70802

Enclosures: Declaration Map for FEMA 4559-DR-LA USFWS List of Federally Listed Threatened, and Endangered Species in Declared Jurisdictions in the State of Louisiana **APPENDIX 7. Section 106 Review Consultation and Continuing Consultation** 



BILLY NUNGESSER LIEUTENANT GOVERNOR State of Louisiana Office of the Lieutenant Governor Department of Culture, Recreation & Tourism Office of Cultural Development Division of Historic Preservation

CARRIE BROUSSARD INTERIM ASSISTANT SECRETARY

October 22, 2024

Tiffany Spann-Winfield Environmental Liaison Officer Louisiana Integration & Recovery Office FEMA Region 6

- Re: SECTION 106 REVIEW CONTINUING CONSULTATION, HURRICANE LAURA, FEMA-4559-DR-LA THE SOCIETY OF ROMAN CATHOLIC CHURCH OF THE DIOCESE OF LAKE CHARLES PROPOSED DEMOLITION AND RELOCATION, PW01265, PT02284, PW02495, AND AIDB 3158:
  - ST. LOUIS HIGH SCHOOL MAIN BUILDING (30.21808, -93.20770), GRANTS MANAGER PROJECT #167257
  - THE LANDRY MEMORIAL GYMNASIUM (30.218386, -93.208367), GRANTS MANAGER PROJECT #171267

• THE KRAJICEK GYMNASIUM (30.218296, -93.208831), GRANTS MANAGER PROJECT #689991 1620 BANK STREET, LAKE CHARLES, CALCASIEU PARISH, LA

ADVERSE EFFECT AND REQUEST TO IMPLEMENT THE ABBREVIATED CONSULTATION PROCESS (ACP)

Dear Ms. Spann-Winfield:

Thank you for your letter received on October 10, 2024, regarding the Federal Emergency Management Agency (FEMA) to provide funds authorized under the Robert T. Stafford Disaster Relief and Emergency Assistance Act, P.L. 93-288, as amended, in response to the following major Disaster Declaration, FEMA-4559-DR-LA, for Hurricane Laura, dated August 28, 2020. FEMA is continuing the Section 106 review for the above-referenced properties in accordance with the *Programmatic Agreement among FEMA, the Louisiana State Historic Preservation Officer (SHPO), the Governor's Office of Homeland Security and Emergency Preparedness (GOHSEP), and Participating Tribes, dated December 21, 2016, as amended, pursuant to Stipulation I.A.3 of the 2024 Statewide PA, in response to a request by The Society of Roman Catholic Church of the Diocese of Lake Charles (DLOC or subrecipient) to provide funds for the demolition of campus structures and the relocation of the St. Louis High School (undertaking). Our office concurs with FEMA's determination that the proposed demolition of the above-referenced buildings constitutes an adverse effect to the NRHP-eligible St. Louis Catholic High School Neighborhood Historic District and the individually NRHP-eligible Landry Memorial Gymnasium.* 

Our office has reviewed the ACP treatment measures to mitigate adverse effects and have the following comment to offer. Regarding the recordation of the Landry Memorial Gym, to avoid any misunderstandings, SHPO recommends that FEMA share the draft ACP with the NPS Southeast Regional Office and receive their official feedback regarding the appropriate HABS level and documentation format. If you have questions or concerns, please contact Jennie Garcia in our Division of Historic Preservation at jgarcia@crt.la.gov.

Sincerely,

CarrieBroussard

Carrie Broussard State Historic Preservation Officer



BILLY NUNGESSER LIEUTENANT GOVERNOR State of Louisiana Office of the Lieutenant Governor Department of Culture, Recreation & Tourism Office of Cultural Development

KRISTIN P. SANDERS ASSISTANT SECRETARY

February 9, 2024

Tiffany Spann-Winfield Environmental Liaison Officer Louisiana Integration & Recovery Office FEMA Region 6

Re: THE SOCIETY OF ROMAN CATHOLIC CHURCH OF THE DIOCESE OF LAKE CHARLES PROPOSED CAMPUS RELOCATION, PW01265, PW02284, AND PW02495:

- ST. LOUIS HIGH SCHOOL MAIN BUILDING (30.21808, -93.20770), GRANS MANAGER PROJECT #167257
- THE LANDRY MEMORIAL GYMNASIUM (30.218386, -93.208367), GRANTS MANAGER PROJECT #171267
- THE KRAJICEK GYMNASIUM (30.218296, -93.208831), GRANTS MANAGER PROJECT #689991 1620 BANK STREET, LAKE CHARLES, CALCASIEU PARISH, LOUISIANA

Dear Ms. Spann-Winfield:

Thank you for your letter received on February 7, 2024, regarding the continued consultation for the above referenced National Register eligible properties. Based on the updated scope of work where the Subrecipient is no longer demolishing the three properties and will instead render the buildings safe and secure, our office concurs that there will be no adverse effect to historic properties.

If you have questions or concerns, please contact Jennie Garcia in our Division of Historic Preservation at jgarcia@crt.la.gov.

Sincerely,

Kater P. Danders

Kristin Sanders State Historic Preservation Officer

**APPENDIX 8. Louisiana Nonattainment Maintenance Status USEPA** 

You are here: EPA Home > Green Book > >National Area and County-Level Multi-Pollutant Information > Louisiana Nonattainment/Maintenance Status for Each County by Year for All Criteria Pollutants

## Louisiana Nonattainment/Maintenance Status for Each County by Year for All Criteria Pollutants

Data is current as of September 30, 2023

Listed by County, NAAQS, Area. The 8-hour Ozone (1997) standard was revoked on April 6, 2015 and the 1-hour Ozone (1979) standard was revoked on June 15, 2005.

* The 1997 Primary Annual PM-2.5 NAAQS (level of 15 µg/m³) is revoked in attainment and maintenance areas for that NAAQS. For additional information see the PM-2.5 NAAQS SIP Requirements Final Rule, effective October 24, 2016. (81 FR 58009)

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LOUISIANA	V	GO
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Important I	Votes		Download	National Datas	et: dbf   xls	Data	dictionary	(PDF)
1.00	NAAQS	Area Name	Nonattainment in Year	Redesignation to Maintenance	Classification	Whole or/ Part County	Population (2010)	State/ County FIPS Codes
LOUISIA		1 ·····			-			· · · · · · · · · · · · · · · · · · ·
Ascension Parish	NAAQS revoked	Baton Rouge, LA	92939495969798990001020304	11	Severe-15	Whole	107,215	22/005
Ascension Parish	8-Hour Ozone (1997)- NAAQS revoked	Baton Rouge, LA	04050607080910	12/30/2011	Moderate	Whole	107,215	22/005
Ascension Parish	(2008)	Baton Rouge, LA	1213141516	03/21/2017	Marginal	Whole	107,215	22/005
Beauregar Parish	1-Hour Ozone (1979)- NAAQS revoked	Beauregard Parish, LA	929394	10/17/1995	Incomplete Data	Whole	35,654	22/011
Calcasieu Parish	1-Hour	Lake Charles,	9293949596	06/02/1997	Marginal	Whole	192,768	22/019

**APPENDIX 9. Phase I Environmental Assessment** 



#### SENT VIA EMAIL

April 4, 2023

Ms. Bridget Evans, Architect Champeaux, Evans, Hotard, APAC 702 Dr. Michael DeBakey Drive Lake Charles, LA 70601

RE: Phase I Environmental Site Assessment 47-Acre Tract Corbina Road Lake Charles, LA

Dear Ms. Evans,

Southland Environmental, LLC is pleased to provide this electronic copy of the Phase I Environmental Site Assessment for the referenced property. This assessment was performed in accordance with the guidelines set forth in ASTM E 1527-21.

If you have any questions, please do not hesitate to contact us. We appreciate the opportunity to provide this service for you.

Sincerely,

C. Blaine Johnson, P.E. Owner/Sr. Engineer

Attachment

## PHASE I ENVIRONMENTAL SITE ASSESSMENT

## CORBINA ROAD 47-ACRE TRACT LAKE CHARLES, CALCASIEU PARISH, LOUISIANA

Prepared for:

Champeaux, Evans, Hotard, APAC 702 Dr. Michael DeBakey Drive Lake Charles, Louisiana 70601

April 4, 2023

Jared R. King, P.G. tal Scientist

0

C. Baine Johnson, P.E. Owner/ Sr. Engineer

Prepared by:



Southland Environmental, LLC 510 Clarence Street Lake Charles, Louisiana 70601 (337) 436-3248

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#### SUMMARY

Southland Environmental, LLC (Southland Environmental) conducted a Phase I Environmental Site Assessment (ESA) of property located adjacent to and east of Corbina Road in Lake Charles, Louisiana. The property is currently undeveloped and 47 acres in size. Based on the results of the activities performed during this Phase I ESA, no recognized environmental conditions were identified on the subject property.

#### **1.0 INTRODUCTION**

Southland Environmental was retained Champeaux, Evans, Hotard, APAC to conduct a Phase I ESA of an approximate 47-acre tract located along Corbina Road in Lake Charles, Louisiana. The subject property is currently undeveloped.

#### 1.1 PURPOSE

The purpose of this investigation was to identify recognized environmental conditions present at the property. A recognized environmental condition is defined as (1) the presence of hazardous substances or petroleum products in, on or at the subject property due to a release to the environment; (2) the likely presence of hazardous substances or petroleum products in, on or at the subject property due to a release or likely release to the environment; or (3) the presence of hazardous substances or petroleum products in, on or at the subject property under conditions that pose a material threat of future release to the environment. This definition is taken from the ASTM Standards on Environmental Site Assessments for Commercial Real Estate, as specified in E 1527-21 (November 2021).

#### 1.2 DETAILED SCOPE OF SERVICES

Prior to performing the site reconnaissance, an environmental database search was conducted and a review of the Louisiana Department of Natural Resources Strategic Online Natural Resources Information System (SONRIS) website for oil and gas wells in the vicinity of the subject property was conducted. A United States Geological Survey topographical map and historical aerial photographs were reviewed to determine elevations, composition of surrounding properties, and possible sources of environmental concern. Upon review of the environmental database report, SONRIS website, maps, and historical aerial photographs, the site reconnaissance was performed on the subject property. The site reconnaissance was performed by inspecting the subject property for possible sources of environmental concern. Upon completion of the visual inspection of the subject property a driving tour was conducted within a 1.0-mile radius of the subject property to determine additional possible sources of environmental concerns, which have the possibility to impact the subject property.

Upon completion of the site reconnaissance, interviews with landowners and state regulatory agencies were conducted to determine any additional environmental concerns associated with the subject property.

#### 1.3 SIGNIFICANT ASSUMPTIONS

At the time of this Phase I ESA, there were no facilities or structures identified on or adjacent to the subject property, which would cause any significant assumptions to be made regarding the condition of the property.

#### 1.4 LIMITATIONS AND EXCEPTIONS OF THE STUDY

The findings and opinions of Southland Environmental are based, in part, on data and information provided by others. Southland Environmental has identified the sources of such information, but makes no warranty or guarantee regarding the accuracy or completeness of such data, the information obtained, or the conclusions solely based on such data.

Environmental assessments and other preliminary investigations are, by their nature, limited investigations. Southland Environmental neither guarantees nor warrants that the sites are free of toxic or hazardous wastes, or other environmental risks that further investigation might reveal. Additionally, the scope of this Phase I ESA does not constitute an evaluation of the environmental compliance record, requirements, or status of these sites.

In addition, the activities of this Phase I ESA have been conducted for the sole purpose of gathering information pertinent to identifying recognized environmental conditions. This assessment does not address physical and working conditions of site improvements and/or buildings, including to structures, roofs, foundations, electrical and plumbing systems, air conditioning/heating systems, on-site sanitary sewer systems, and storm drainage.

#### 1.5 SPECIAL TERMS AND CONDITIONS

There are no special terms or conditions, which are applicable to this Phase I ESA.

#### 1.6 DATA GAPS

There were no data gaps encountered during the performance of this Phase I ESA.

#### 1.7 USER RELIANCE

No information obtained in performing this Phase I ESA is suspected to be incorrect, skewed, or inaccurate. The reliance of this report is limited to only the report user.

#### 2.0 SITE DESCRIPTIONS

#### 2.1 LOCATION AND LEGAL DESCRIPTION

The subject property is located in Section 23, Township 10 South, Range 8 West of Calcasieu Parish. The approximate coordinates of the center of the property are Latitude 30° 10' 54.4" N and Longitude 93° 09' 19.7" W. A Site Location Map is included as Figure 1 and a Site Survey, provided by the Report User, is included as Figure 2 in Appendix A of this report.

#### Southland Environmental, LLC

#### 2.2 SITE AND VICINITY CHARACTERISTICS

The subject property is located along Corbina Road in southeast Lake Charles, Louisiana. Corbina Road is located on the west boundary of the property and pasture land is located on the east boundary of the subject property. Land uses in the vicinity of the subject property are primarily a mixture of new and upcoming residential development and agricultural pastures.

#### 2.3 CURRENT USES OF THE PROPERTY

The subject property is currently undeveloped and used for agricultural purposes.

# 2.4 DESCRIPTIONS OF STRUCTURES, ROADS, OTHER IMPROVEMENTS ON THE SITE

No structures, roads, or other improvements are located on the subject property. A drainage ditch is located immediately west and adjacent of the subject property, paralleling Corbina Road. The adjoining utilities include fiber optic communications and natural gas distribution. No additional improvements, structures, or roads were noted on the subject property.

#### 2.5 CURRENT USES OF THE ADJOINING PROPERTIES

The properties north of the subject property are undeveloped and used for cattle grazing and consists of property that contains old storage buildings that were once used by the former Chennault Airforce base. East of the subject property is property used for cattle grazing. South of the subject property is land that is undeveloped and agricultural in use and land that is part of a residential development at the southeast corner of the subject property. Corbina Road is located on the west boundary of the subject property. The property across Corbina Road is a mix of residential properties and undeveloped land.

#### 3.0 USER PROVIDED INFORMATION

The information contained in Section 3.0 was based on information provided by the report user. The user questionnaire was completed by Ms. Bridget Evans of Champeaux, Evans, Hotard, APAC. A copy of the user information questionnaire is included in Appendix B.

#### 3.1 TITLE RECORDS

The task of performing a title records search or environmental liens search is the responsibility of the report user. It is the option of the report user to perform this service during the Phase I ESA. Title records and environmental lien searches were not performed by the report user or Southland Environmental as part of this assessment.

#### 3.2 ENVIRONMENTAL LIENS OR ACTIVITY AND USE LIMITATIONS

The provided information indicates that the user is not aware of any environmental liens or use

limitations on the subject property.

#### 3.3 SPECIALIZED KNOWLEDGE

Southland Environmental was not made aware of any specialized knowledge or experiences that are material to recognized environmental conditions in connection with the subject property.

#### 3.4 COMMONLY KNOWN OR REASONABLY ASCERTAINABLE INFORMATION

Southland Environmental was not made aware of any commonly known or reasonably ascertainable information within the local community that is material to recognized environmental conditions in connection to the subject property.

#### 3.5 VALUATION REDUCTION FOR ENVIRONMENTAL ISSUES

No valuation reduction of the property, due to hazardous substances, is known to have occurred on the subject property.

#### 3.6 OWNER, PROPERTY MANAGER, AND OCCUPANT INFORMATION

According to the Calcasieu Parish Police Jury Mapping Application on March 14, 2023, the subject property is currently owned by Lake Charles Catholic High Schools, Inc.

#### 3.7 REASON FOR PERFORMING PHASE I ESA

This Phase I ESA was performed to identify and understand potential environmental conditions which could potentially impact the subject property. In addition, the Phase I ESA was also performed to qualify the user for Limited Liability Protection to CERCLA liability.

#### 3.8 OTHER

No other information regarding the subject property was provided to Southland Environmental by the report user.

#### 4.0 **RECORDS REVIEW**

#### 4.1 STANDARD ENVIRONMENTAL RECORD SOURCES

A computer database search of environmental agency file records was conducted for Southland Environmental by Banks Environmental Data (Banks). A copy of the Banks report (ES# 141754) is included as Appendix C.

4.1.1 National Priorities List Sites

The National Priorities List (NPL) is the list of high priority hazardous waste sites in the United States eligible for long-term remedial action financed under the federal Superfund program and

the Comprehensive Environmental Response, Compensation, and Liability ACT (CERCLA). The Banks Report did not identify any Federal NPL or State NPL sites within the 1.0-mile search radius of the subject property.

#### 4.1.2 Delisted NPL Sites

The Delisted NPL is a list of all sites that have been deleted from the Environmental Protection Agency's (EPA) NPL list. These sites are taken off the NPL list usually due to no further response or remedial action being required on them. The Banks Report did not identify any Delisted NPL sites listed within the 0.5-mile search radius of the subject property.

#### 4.1.3 CERCLIS Sites

Comprehensive Environmental Response, Compensation, and Liability Information System (CERCLIS) sites come from the CERCLA, a federal law designed to clean up abandoned hazardous waste sites. These sites are either proposed, listed, or under review currently to be a part of the NPL. The Banks Report did not identify any CERCLIS sites within the 0.5-mile search radius of the subject property.

4.1.4 No Further Remedial Action Planned Sites

CERCLIS sites designated No Further Remedial Action Planned (NFRAP) have been removed from CERCLIS. NFRAP sites may be sites where, following an initial investigation, either no contamination was found, contamination was removed quickly without the need for the site to be placed on the NPL, or the contamination was not serious enough to require federal Superfund action or NPL consideration. The Banks Report did not identify any CERCLIS NFRAP sites within the 0.5-mile search radius of the subject property.

#### 4.1.5 RCRA-CORRACTS Sites

These sites are registered hazardous waste generators or handlers that fall under the Resource Conservation and Recovery Act (RCRA) and subject to corrective action activity. The Banks Report did not identify any RCRA-CORRACTS sites within the 1.0-mile search radius of the subject property.

#### 4.1.6 RCRA-TSD Facilities

This database lists all treatment, storage, and disposal of hazardous material sites that fall under RCRA. The Banks Report did not identify any RCRA-TSD facilities within the 0.5-mile search radius of the subject property.

#### 4.1.7 RCRA Large/Small Quantity Generators

The EPA and the LDEQ maintain lists of registered large and small quantity generators of hazardous wastes. A Large Quantity Generator of hazardous waste generate 1,000 kilograms (kg) per month or more of acutely hazardous waste. A Small Quantity Generator generates between

100 kg and 1000 kg of waste per month. A Conditionally Exempt Small Quantity Generator generates no more than 100 kg of hazardous waste per month. The Banks Report did not identify any RCRA-GEN hazardous waste generators within the 0.25-mile search radius of the subject property.

#### 4.1.8 Emergency Response Notification System

The Emergency Response Notification System (ERNS) is a national database used to store information on unauthorized release of oil and hazardous substances that have been reported to the National Response Center since 2001. The Banks Report did not identify any ERNS site within the 0.25-mile search radius of the subject property.

#### 4.1.9 Engineering Control/Institutional Control Sites

This is a listing of Brownfield Management System (BMS) sites that have had Engineering Controls (ECs) or Institutional Controls (ICs) placed on them. ECs are physical methods or modifications put into place on a site to reduce or eliminate the possibility of human exposure to known contamination. ICs are administrative constraints, such as legal controls, that help minimize the potential for human exposure to known contamination by ensuring appropriate land and resource use. The Banks Report did not identify any EC or IC sites within the 0.5-mile search radius of the subject property.

#### 4.1.10 Federal and State Brownfields Sites

This is a listing of sites that assist the EPA in collecting, tracking, and uploading information of sites in relation to the Small Business Liability Relief and Brownfields Revitalization Act. These sites are real property that is either abandoned or underutilized where redevelopment or expansion is complicated by real or perceived environmental contamination. The Banks Report did not identify any Brownfields sites within the 0.5-mile search radius of the subject property.

#### 4.1.11 Solid Waste Landfill Sites

This database contains listings of all solid waste disposal facilities or landfills registered with the Solid Waste Program for the LDEQ. The Banks Report did not identify any solid waste landfill sites within the 0.5-mile search radius of the subject property.

#### 4.1.12 Leaking Underground Storage Tank Sites

This database is a list of all known leaking underground storage tanks (identified as LPST in the Banks Report) as registered with the Remediation Services Division of the LDEQ. The Banks Report did not identify any LPST sites within the 0.5-mile search radius of the subject property.

4.1.13 Registered Underground Storage Tanks

This database is a list of all known underground storage tanks (identified as PST in the Banks Report) as registered with the Remediation Services Division of the LDEQ. The Banks Report

identified one PST site within the 0.25-mile search radius of the subject property. This site is described as follows:

• Morgan Field C Store, 3170 E. McNeese Street, Lake Charles, located approximately 0.23mile southwest of the subject property. The site is due south of the subject property. Refer to Section 4.5 of this report for more details about this facility.

#### 4.1.14 Voluntary Cleanup Program Sites

This database contains information about sites that have been placed in the Louisiana Voluntary Cleanup Program (VCP). This is a program that provides current property owners with the opportunity to clean up contaminated properties and attain a release of liability for further cleanup of historical contamination at the site. The Banks Report did not identify any VCP sites within the 0.5-mile search radius of the subject property.

#### 4.1.15 State Hazardous Waste Sites

This database contains information on facilities which store, process, or dispose of hazardous waste as maintained by the Industrial and Hazardous Waste Permits section of the Texas Commission of Environmental Quality (TCEQ), or other state regulatory agencies. This database is not currently available from LDEQ. The Banks Report did not identify any State Hazardous Waste (HW) sites within the 0.25-mile search radius of the subject property.

#### 4.1.16 Unmapped Sites

The Banks Report did not identify any unmapped sites within the search radius of the subject property.

#### 4.2 ADDITIONAL ENVIRONMENTAL RECORD SOURCES

The Banks Report presents additional databases other than the standard ASTM required information. A description of these databases and details of the search area for the databases are listed in the Banks Report. The Banks report did not identify any additional environmental record sources within the search radius of the subject property.

#### 4.3 PHYSICAL SETTING SOURCE

A United States Geological Survey (USGS) 7.5-minute Topographical Map was reviewed as part of this Phase I ESA. The natural site elevation is approximately 15 feet above National Geodetic Vertical Datum (NGVD) based on the USGS Topographical Map. Drainage on the subject property appears to be toward the property boundaries, with a roadside drainage ditch located along Corbina Road and the various drainage swales located throughout the subject property.

# 4.4 HISTORICAL USE INFORMATION ON THE PROPERTY AND ADJOINING PROPERTIES

#### 4.4.1 Aerial Photographs Review

Historical aerial photographs from flights flown in 1940, 1953, 1963, 1975, 1983, 1990, 1998, 2004, 2010, 2017, and 2021 were reviewed as part of this Phase I ESA. The aerial photographs are included as Appendix D.

In the 1940 and 1953 aerial photographs, the subject property and surrounding properties appear to be undeveloped. Various stormwater drainage laterals can be seen in the vicinity of the subject property.

In the 1963, 1975, and 1983 aerial photographs, the subject property appears to have some agricultural use as access roads can be seen near the property. The storage buildings utilized by the Chennault Airforce Base can be seen constructed north of the subject property. In the 1975 photograph, oil & gas exploration activities are visible on property located northwest of the subject property. This includes an access road north of the subject property leading to a well location pad. A pit is visible east of the well pad. In the 1983 aerial photograph, the oil and gas exploration activities are no longer visible, however the access road leading to the pad remains. The remainder of the surrounding properties appear to be used for agricultural purposes.

In the 1990, 1998, 2004, and 2010 aerial photographs, the subject property and surrounding properties remain undeveloped and agricultural in use. Additional drainage laterals are visible in the vicinity. No development other than the previously mentioned storage buildings north of the subject property are present. East McNeese Street is visible south of the subject property.

In the 2017 and 2021 aerial photographs, the subject property remains predominantly undeveloped and agricultural as it presently exists. Corbina Road can be seen on the west boundary of the subject property and East McNeese Street is seen further to the south. Residential development is visible southeast and southwest of the subject property.

No pits, ponds, or excavations are visible on the subject property in any of the reviewed aerial photographs.

#### 4.4.2 City Directory Review

A historical directory search was conducted for Southland Environmental by Banks Environmental Data (Banks). A copy of the Banks City Directory Report (ES# 141754) is included as Appendix E. The report includes City Directory listings from 1970, 1975, 1980, 1986-87, 1992, 1997, 2002, 2007, 2012, 2017, and 2022. The directories were reviewed for listings at and in the vicinity of Corbina Road, Advent Court, Basin Way, Cabot Drive, East McNeese Street, East Prien Lake Road, Fairwood Lane, Forestwood Drive, Gardenwood Parkway, James Court, Lake Crest Drive, Meadow Brook Way, Rosehill Drive, and Village Lane. There were earlier City Directories available for Lake Charles, LA but they did not list the subject property area.

The subject property was not identified in any of the City Directories searched. Personal residences, apartments, and commercial properties are listed in the vicinity of the subject property in each of these directories. There were no properties listed that would be expected to cause an environmental concern to the subject property.

#### 4.5 LDEQ RECORDS REVIEW

A review of the LDEQ Environmental Data Management System (EDMS) for issues pertaining to the subject property and surrounding properties was also performed as part of this Phase I ESA. This review was performed to determine any additional possible environmental concerns for the subject property. Due to the absence of a property address, EDMS files for East McNeese Street and Corbina Road were reviewed. The only EDMS files identified within the area of the subject property were associated with construction companies developing at Morganfield Subdivision south of the subject property. Files for each of the companies were associated with storm water discharge permits.

The Morgan Field C Store is located at 3170 E. McNeese Street approximately 0.23-mile south of the subject property. EDMS files indicated the site has a 3-compartment UST with a capacity of 25,000 gallons. The tank was installed in August 2022. Site reconnaissance revealed this is a new convenience store under construction and it is not yet in operation.

#### 4.6 OIL AND GAS REVIEW

A review of the SONRIS website was performed for oil and gas wells or historical oil and gas wells in the vicinity of the subject property. Ten permitted well sites were identified within 1.0-mile of the subject property.

Well Serial	Permit Date	Well Status
Number		
121342	8/31/1967	PLUGGED AND ABANDONED GAS
122698	12/11/1967	PLUGGED AND ABANDONED GAS
164521	7/30/1979	PLUGGED AND ABANDONED GAS
168388	4/22/1980	PLUGGED AND ABANDONED GAS
168446	4/24/1980	PLUGGED AND ABANDONED GAS
175229	5/11/1981	PLUGGED AND ABANDONED GAS
152273	6/16/1976	PLUGGED AND ABANDONED NO PRODUCT SPECIFIED
143570	9/18/1973	DRY AND PLUGGED NO PRODUCT SPECIFIED
148470	4/21/1975	DRY AND PLUGGED NO PRODUCT SPECIFIED
147021	10/10/1974	PERMIT EXPIRED

A table of LDNR SONRIS wells within a 1.0-mile radius is presented below:

A review of the LDNR database revealed that a gas well was installed on a tract located northwest of the subject property in December of 1967. The well (serial number 122698), which was installed by Pan American Petroleum Corporation, was plugged and abandoned in November of 1979. According to the Plug and Abandonment report, the upper casing of the well was cutoff at six feet below ground surface and a steel plate was welded onto the top end of the casing. No pit registration records were identified during the LDNR database review. In addition, the property

at which this well was located was subject to soil sampling and analysis activities as part of another due diligence research project. The results from these activities indicate it is not expected that this well location would have an adverse effect on the subject property.

Although generally accurate, mapped SONRIS well locations are not exact. No well sites are indicated to be present on the subject property. Oil and gas exploration and production activities can be a source of soil and groundwater contaminants. Based on the status and distance from these wells to the subject property, they are not expected to pose an environmental concern to the subject property.

#### 5.0 SITE RECONNAISSANCE

#### 5.1 METHODOLOGY AND LIMITING SITE CONDITIONS

A site inspection was performed on March 30, 2023 by Blaine Johnson of Southland Environmental. There were no limiting conditions that impeded the complete inspection of the subject property. Photographs taken during the inspection are included in Appendix F.

#### 5.2 SITE OBSERVATIONS

#### 5.2.1 Exterior Observations

The subject property, which is currently undeveloped, is accessed from Corbina Road. A barbed wire fence is located along the southern and western boundaries of the property. A gate is located on the adjacent property to the north (from Corbina Road) which provides access near the northwest corner of the subject property.

A dense line of trees and shrubs is located along the southern boundary of the subject property. The subject property is maintained through mowing on a regular basis, as there is primarily only grassy vegetation and very small trees growing throughout the remainder of the subject property. A few small drainage swales are located throughout the subject property, the largest swale running north/south is located at the approximate center of the property.

There was no stained or stressed vegetation identified on the subject property.

#### 5.2.2 Interior Observations

As there were no buildings on the property, no interior observations were made.

#### 5.3 HAZARDOUS SUBSTANCES

No hazardous substances were identified on the subject property at the time of the site inspection.

#### 5.4 INDICATORS OF POLYCHLORINATED BIPHENYLS (PCBs)

No pole-mounted transformers were observed on the subject property. Electrical providers have been contacted in the past with respect to transformers. These providers have stated in previous correspondence that their transformers are operated in compliance with all Federal and State regulatory guidelines, including those promulgated by the US EPA in Part 761 of Title 40, Toxic Substance Control Act. In case of a spill from a transformer on any site, these providers will take the appropriate action.

#### 5.5 SOLID WASTE DISPOSAL

No evidence of solid waste disposal was observed on the subject property at the time of the site inspection.

#### 5.6 STORAGE TANKS

There was no evidence of any storage tanks located on the subject property at the time of the site inspection.

#### 6.0 INTERVIEWS

Interview questionnaires for each interview performed as part of this Phase I ESA is included in Appendix G.

#### 6.1 INTERVIEWS WITH OWNERS

According to information obtained from the Calcasieu Parish Tax Assessor on-line database, the subject property is currently owned by the Lake Charles Catholic High Schools, Inc. Since the subject property was just recently purchased, Southland Environmental contacted the previous landowner as part of this ESA. Mr. James Palma of East Prien Lake Properties, LLC was contacted in regards to the historic use of the subject property. Mr. Palma indicated that East Prien Lake Properties had owned the property since about 2006. Mr. Palma stated that to his knowledge, he was unaware of any USTs, pipelines, or environmental issues associated with the subject property. He also stated he was unaware of any instances where an environmental agency had to respond to the subject property.

#### 6.2 INTERVIEW WITH SITE MANAGER

No site manager interview was conducted during this Phase I ESA.

#### 6.3 INTERVIEWS WITH OCCUPANTS

The site was unoccupied at the time of the site inspection.
### 6.4 INTERVIEWS WITH LOCAL GOVERNMENT OFFICIALS

Mr. Jason Roy with the LDEQ was interviewed regarding environmental issues pertaining to the subject property. He stated that he was unaware of any environmental concerns associated with the subject property. Mr. Roy indicated that any documentation that the LDEQ would have on file for facilities in that area is available on the LDEQ EDMS.

### 6.5 INTERVIEWS WITH OTHERS

No additional interviews were conducted as part of this assessment.

### 7.0 ADDITIONAL SERVICES

No additional services were provided as part of this Phase I ESA.

### 8.0 FINDINGS

Based on the results of the activities performed during this Phase I ESA, no recognized environmental conditions were identified with the subject property.

A recognized environmental condition is defined as (1) the presence of hazardous substances or petroleum products in, on or at the subject property due to a release to the environment; (2) the likely presence of hazardous substances or petroleum products in, on or at the subject property due to a release or likely release to the environment; or (3) the presence of hazardous substances or petroleum products in, on or at the subject property under conditions that pose a material threat of future release to the environment.

### 8.1 VAPOR INTRUSION

Based on information obtained during this Phase I ESA, there have been no documented soil or groundwater contamination at the subject property or adjacent to the subject property. Therefore, vapor intrusion impacts to structures on the property would not be anticipated to be a concern.

### 9.0 **OPINIONS**

Based on the results of the activities performed during this Phase I ESA, no recognized environmental conditions were identified on the subject property.

### **10.0 CONCLUSIONS**

Southland Environmental, LLC has performed a Phase I ESA in conformance with the scope and limitations of ASTM Practice E 1527-21 of property located along Corbina Road in Lake Charles, Louisiana and described in Section 2.1 of this report. The subject property is undeveloped. Any exceptions to, or deletions from, this practice are described in Section 1.4 of this report. Based on the results of the activities performed during this Phase I ESA, no recognized environmental conditions were identified on the subject property.

### **11.0 DEVIATIONS**

No deviations from ASTM Practice E 1527-21 were made during the investigation.

### 12.0 QUALIFICATIONS OF ENVIRONMENTAL PROFESSIONALS

Southland Environmental personnel have extensive experience in environmental investigations and in Phase I and II Environmental Site Assessments. Many of these assessments have been performed for repeat clients and have involved diverse properties including private, commercial, light industrial, and heavy industrial properties. These properties have ranged in size from hundreds of acres and many buildings, to small lots containing no buildings.

### 12.1 QUALIFICATIONS AND CREDENTIALS OF SOUTHLAND ENVIRONMENTAL PERSONNEL

Resumes of Southland Environmental personnel who participated in this investigation are included as Appendix H. The Environmental Professional's Statement is included in Appendix I.

### **13.0 REFERENCES**

- ASTM International, E 1527-21, "Standard Practice for Environmental Site Assessments: Phase I Environmental Site Assessment Process", ASTM International, West Conshohocken, PA.
- Banks Environmental Data, The Banks Regulatory Database Report, ES #141754, prepared for Southland Environmental, LLC, Lake Charles, Louisiana.
- Calcasieu Parish Police Jury Mapping Application, <u>https://gis-cppj.hub.arcgis.com</u>.
- City Directory Report obtained from Banks Environmental Data, ES #141754.
- Historical Aerial Photography obtained from Banks Environmental Data, ES #141754.
- Louisiana Department of Environmental Quality Environmental Data Management System (EDMS) records obtained from <u>http://edms.deq.louisiana.gov/app/doc/_querydef.aspx</u>, Louisiana Department of Environmental Quality, Baton Rouge, Louisiana.
- Louisiana Department of Environmental Quality Geographic Information Systems Interactive Mapping Application, <u>http://gis.deq.state.la.us/menu.aspx</u>, Louisiana Department of Environmental Quality, Baton Rouge, Louisiana.
- Louisiana Department of Natural Resources Strategic Online Natural Resources Information System (SONRIS) records obtained from http://sonris.com, Louisiana Department of Natural Resources, Baton Rouge, Louisiana.

### **APPENDIX** A

Figures

### FIGURE 1

Site Location Map



### FIGURE 2

Site Survey



### **APPENDIX B**

User Provided Information

### **ASTM E 1527-13 USER QUESTIONNAIRE INTRODUCTION**

In order to qualify for one of the landowner liability Protections  $(llPs)'x^7$  offered by the Small Business liabili(Y Relief and Brownfields Revitalization Act of 2001 (the "Brownfields Amendments").³⁸ the user must conduct the foffowing inquiries required by 40 CFR 312.25, 312.28, 312.29, 312.30 and 312.31. These inquiries must also be conducted by EPA Brownfield Assessment and Characterization grantees. The user should provide the following information to the environmental professional. Failure to conduct these inquiries could result in a determination that "all appropriate inquiries" is not complete.

### (1.) Environmental liens that are filed or recorded against the property (40 CFR 312.25).

Did a search of recorded land title records (or judicial records where appropriate, see Note 1 below) identify any  $NJ^{0}$ environmental liens filed or recorded against the property wider federal tribal, state or local law?

Note 1 - In certain jurisdictions, federal, tribal, state, or local statues, or regulations specify that environmental liens and Activity and Use Limitations (AULs) be filed in judicial records rather than in land title records. In such cases judicial records must be searched for environmental liens and AULs.

### (2.) Activity and use limitations that are in place on the property or that have been filed or recorded against the property (40 CFR 312.26(a)(l)(v) and (vi)).

Did a search of recorded land title records (or judicial records where appropriate, see Note 1 above) identify any AULs such as engineering controls, land use restrictions or institutional controls that are in place at the property No and/or have been filed or recorded against the property under federal, tribal, state, or local law?

### (3.) Specialized knowledge or experience of the person seeking to qualify for the LLP (40 CFR 312.28).

Do you have any specialized knowledge or experience related to the property or nearby properties? For example, are you involved in the same line of business as the current or former occupants of the property or an adjoining property so that you would have specialized knowledge of the chemicals and processes used by this type of business?

### t10

### (4.) Relationship of the purchase price to the fair market value of the property ifit were not contaminated (40 CFR 312.29).

Does the purchase price being paid for this property reasonably reflect the fair market value of the property? If you conclude that there is a difference, have you considered whether the lower purchase price is because contamination is known or believed to be present at the property?  $\bigvee S$ 

### (5.) Commonly known or reasonably ascertainable information about the property (40 CFR 312.30).

Are you aware of commonly known or reasonably ascertainable information about the property that would help the environmental professional to identify conditions indicative of releases or threatened releases? For example,

- (a.) Do you know the past uses of the property?  $\underline{A V}, ct., v1, fvw-e...,$

- (d.) Do you know of any environmental cleanups that have taken place at the property? N

(6.) The degree of obviousness of the presence or likely presence of contamination at the property, and the ability to detect the contamination by appropriate investigation (40 CFR 312.31).

Based on your knowledge and experience related to the property are there any obvious indicators that point to the presence or likely presence of contamination at the property? <u>N,-o</u>

 11_s  landowner Liabi/iry Protections. or llPs. is the term used to describe the three rypes of potential defenses to Superfind /iabiliry in EPA's Interim Guidance Regarding Criteria landowners Must Meer in Order to Qualify for Bona Fide Prospective Purchaser. Contiguous Properly Owner. or Innocent landowner limitations on CERCIA liability ("Common Elements" Guide) issued on March 6.2003.

цлл *Р.1.* 107-1/8.

3/14/2023

Signed VJ'0{50=e1htvis1 Architect Printed Name/ Title

### APPENDIX C

Regulatory Records Documentation

Prepared for:

SOUTHLAND ENVIRONMENTAL LLC 510 Clarence St Lake Charles, LA 70601



# RegulatoryASTM E1527-21/AAI Con<br/>Corbina Rd TractDatabaseLake Charles, LA 70607 Report

## ASTM E1527-21/AAI Compliant **Calcasieu** County

PO #: 12055

ES-141754

Tuesday, March 14, 2023



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### **Geographic Summary**



Location						
Calcasieu County, LA						
Target location is 0.073 square miles and has a 7	1.11 mile perimeter					
Coordinates						
Longitude & Latitude in Degrees Minutes Sec						
Longitude & Latitude in Decimal Degrees	NA					
X and Y in UTM	NA					
Elevation						
NA						
Zip Codes Searched						
Search Distance	Zip Codes (historical zip codes included)					
Target Property	70607					
0.25 miles	70615, 70607					
0.5 miles	70615, 70607					
1 mile	70615, 70607					
Topos Searched						
Search Distance	Topo Name					
Target Property	Lake Charles (1977)					
0.25 miles	Lake Charles (1977)					
0.5 miles	Lake Charles (1977)					
1 mile	Lake Charles (1977)					

### **Database Summary**



Databases Searched	Distance Searched	# Mapped	# Not Mapped	Total
Federal - ASTM 1527-21/AAI Required				
National Priority List (NPL)	1	0	0	0
Delisted National Priority List (DNPL)	0.5	0	0	0
SEMS (CER SEMS)	0.5	0	0	0
SEMS NFRAP (CER SEMS NFRAP)	0.5	0	0	0
RCRA CORRACTS (RCRA COR)	1	0	0	0
RCRA non-CORRACTS TSD (RCRA TSD)	0.5	0	0	0
RCRA Generators (RCRA GEN)	0.25	0	0	0
Federal Brownfields (FED BWN)	0.5	0	0	0
Federal Institutional Control (FED IC)	0.5	0	0	0
Federal Engineering Control (FED EC)	0.5	0	0	0
ERNS List (ERNS)	0.25	0	0	0
State - ASTM 1527-21/AAI Required				
State/Tribal Equivalent NPL (ST NPL)	1	0	0	0
State/Tribal Equivalent CERCLIS (ST CER)	0.5	0	0	0
State/Tribal Disposal or Landfill (SWLF)	0.5	0	0	0
State/Tribal Leaking Storage Tank (LPST)	0.5	0	0	0
State/Tribal Storage Tank (PST)	0.25	1	0	1
State/Tribal Institutional Control (ST IC)	0.25	0	0	0
State/Tribal Engineering Control (ST EC)	0.5	0	0	0
State/Tribal Voluntary Cleanup (VCP)	0.5	0	0	0
State/Tribal Brownfield (ST BWN)	0.5	0	0	0
State/Tribal Hazardous Waste (HW)	0.25	0	0	0
Non-ASTM/AAI Required Databases				
RCRA (RCRA)	0.25	0	0	0
Dry Cleaners (DRYC)	0.25	0	0	0
Total Sites Found		1	0	1





### Summary Map - 1 Mile Buffer



Б



### Current Imagery Overlay Map - 0.5 Mile Buffer









et Prop n 0.25	miles of Target	Property		Mt, Cr Mr, Mt, Cr, Lt		
Гуре D	escriptions					
Crowle	y-Vidrine comp	lex, 0 to 1 percent slopes				
ent Hyd		4				
num De	epth to Bedrock	(				
Crow	ley (55 percent)					
	ologic Group		High runoff po	otential		
-	Drainage Class		Somewhat po			
Corro	sion Potential -	Uncoated Steel	High			
Depth	n to Restrictive I	Feature				
	Horizon	Soil Texture	Upper Boundary	Lower Boundary	AASHTO	Unified
	Ар	Silt loam	0 cm	18 cm	A-4, A-6	CL, CL-ML, ML
	Btg1	Silty clay	43 cm	102 cm	A-7-6	CH, CL
	Btg2	Clay loam	102 cm	203 cm	A-6, A-7-6	CH, CL
	Eg	Silt loam	18 cm	43 cm	A-4, A-6	CL, CL-ML, ML
Vidrin	ne (35 percent)					
	ologic Group		High runoff po	otential		
Soil D	Drainage Class		Somewhat po	oorly drained		
		Uncoated Steel	High			
Depth	n to Restrictive I	Feature				
	Horizon	Soil Texture	Upper Boundary	Lower Boundary	AASHTO	Unified
	Α	Silt loam	0 cm	15 cm	A-4	CL, CL-ML, ML
	BCtg	Silty clay loam	165 cm	203 cm	A-6, A-7-6	CH, CL
	Bt/E	Silty clay	36 cm	46 cm	A-6, A-7-6	CH, CL
	Btg E	Silty clay Silt loam	46 cm 15 cm	165 cm 36 cm	A-6, A-7-6	CH, CL
	E	Siit Ioani	15 CIII	30 CIII	A-4	CL, CL-ML, ML
Acad	iana (3 percent)					
	ologic Group					
	Drainage Class		Moderately w	ell drained		
		Uncoated Steel				
Depti	n to Restrictive I	reature				
Edge	rly (3 percent)					
-	ologic Group					
	Drainage Class		Poorly drained	d		
		Uncoated Steel				
Depth	n to Restrictive I	Feature				
Mowa	ata (2 percent)					
-	ologic Group					
	Drainage Class		Poorly drained	d		
		Uncoated Steel				
Depth	n to Restrictive I	reature				
Prairi	ieland (2 percen	t)				
Linda	ologic Group					
Hyard	Drainage Class		Poorly drained	d		
Soil D	-	Uncoated Steel				

Percent Hydric

82



Prairieland (80 percen	it)				
Hydrologic Group		Moderately hi	gh runoff potential when dra	ained and high runoff potentia	undrained
Soil Drainage Class		Poorly drained	ł		
Corrosion Potential -		High			
Depth to Restrictive F	eature				
Horizon	Soil Texture	Upper Boundary	Lower Boundary	AASHTO	Unified
Ар	Silt loam	0 cm	22 cm	A-4, A-6	CL-ML, ML
Btg/E	Loam	34 cm	60 cm	A-4, A-6, A-7-6	CH, CL
Btg1	Loam	60 cm	150 cm	A-6, A-7-6	CH, CL
Btg2	Clay loam	150 cm	203 cm	A-6, A-7-6	CH, CL
Eg	Silt loam	22 cm	34 cm	A-4, A-6	CL-ML, ML
Edgerly (11 percent)					
Hydrologic Group					
Soil Drainage Class		Poorly drained	t		
Corrosion Potential -	Uncoated Steel				
Depth to Restrictive F	eature				
Crowley (3 percent)					
Hydrologic Group					
Soil Drainage Class		Somewhat po	orly drained		
Corrosion Potential -	Uncoated Steel				
Depth to Restrictive F	eature				
Kaplan (2 percent)					
Hydrologic Group					
Soil Drainage Class		Somewhat po	orly drained		
Corrosion Potential -	Uncoated Steel				
Depth to Restrictive F	eature				
Kinder (2 percent)					
Hydrologic Group					
Soil Drainage Class		Poorly drained	Ł		
Corrosion Potential -	Uncoated Steel				
Depth to Restrictive F	eature				
Midland (2 percent)					
Hydrologic Group					
Soil Drainage Class		Poorly drained	k		
Corrosion Potential -	Uncoated Steel				
Depth to Restrictive F	eature				
dgerly loam, 0 to 1 pe	rcent slopes, rarely flood	ed			
nt Hydric	9				
um Depth to Bedrock					
Edgerly (82 percent)					
Hydrologic Group		High runoff po	otential		
Soil Drainage Class		Poorly drained			
Corrosion Potential -	Uncoated Steel	High			
Depth to Restrictive F	eature				
Horizon	Soil Texture	Upper Boundary	Lower Boundary	AASHTO	Unified
Ар	Loam	0 cm	19 cm	A-4, A-6	CL, CL-ML, ML
-	Loam	19 cm	78 cm	A-6, A-7-6	CL
Bt	Louin	10 0111	10 0111	71 0,71 1 0	<b>V</b> -



					A DIVISION OF THE BAN
Prairieland (6 percent)					
Hydrologic Group					
Soil Drainage Class		Poorly drained	d		
Corrosion Potential - Ur					
Depth to Restrictive Fea	ature				
Kaplan (4 percent)					
Hydrologic Group					
Soil Drainage Class		Somewhat po	oorly drained		
Corrosion Potential - Ur					
Depth to Restrictive Fea	ature				
Vidrine (3 percent)					
Hydrologic Group					
Soil Drainage Class		Somewhat po	oorly drained		
Corrosion Potential - Ur					
Depth to Restrictive Fea	ature				
Crowley (2 percent)					
Hydrologic Group					
Soil Drainage Class		Somewhat po	oorly drained		
Corrosion Potential - Ur					
Depth to Restrictive Fea	ature				
Midland (2 percent)					
Hydrologic Group					
Soil Drainage Class		Poorly drained	d		
Corrosion Potential - Ur					
Depth to Restrictive Fea	ature				
Mowata (1 percent)					
Hydrologic Group					
Soil Drainage Class		Poorly drained	d		
Corrosion Potential - Ur					
Depth to Restrictive Fea	ature				
-	a, 0 to 1 percent slopes, r				
nt Hydric	65	<b>;</b>			
um Depth to Bedrock					
Mowata (60 percent)					
Hydrologic Group		High runoff po			
Soil Drainage Class		Poorly drained	b		
Corrosion Potential - Un		High			
Depth to Restrictive Fea					
Horizon	Soil Texture	Upper Boundary	Lower Boundary	AASHTO	Unified
Ар	Silt loam	0 cm	20 cm	A-4	CL, CL-ML, ML
Btg	Silty clay	86 cm	203 cm	A-6, A-7-6	CL
Btg/E	Clay loam	46 cm	86 cm	A-7-6	CH, CL
Eg	Silt loam	20 cm	46 cm	A-4	CL, CL-ML, ML
Vidrine (30 percent)					
		High runoff po	otential		
Hydrologic Group Soil Drainage Class Corrosion Potential - Ui		Somewhat po High			



HorizonSoil TextureUpper BoundaryLower BoundaryAASHTOUnifiedASilt Ioam0 cm15 cmA-4CL, CL-ML, MLBCgSilty clay loam152 cm203 cmA-6, A-7-6CH, CLBVESilt Ioam48 cm56 cmA-6, A-7-6CH, CLBtgSilty clay56 cm152 cmA-6, A-7-6CH, CLESilt Ioam15 cm48 cmA-4CL, CL-ML, MLCrowley (3 percent)Its cm48 cmA-4CL, CL-ML, MLHydrologic GroupSomewhat poorly drainedCorrosion Potential - Uncoated SteelIts cmDepth to Restrictive FeatureIts cmIts cmIts cmIts cmEdgerly (2 percent)Its cmPoorly drainedIts cmIts cmHydrologic GroupSoil Drainage ClassPoorly drainedIts cmIts cmSoil Drainage ClassPoorly drainedIts cmIts cmIts cmEdgerly (2 percent)Its cmIts cmIts cmIts cmHydrologic GroupSoil Drainage ClassPoorly drainedIts cmIts cmSoil Drainage ClassPoorly drainedIts cmIts cmIts cmEdgerly (2 percent)Its cmIts cmIts cmIts cmHydrologic GroupSoil Drainage ClassPoorly drainedIts cmIts cmBeth to Restrictive FeatureIts cmIts cmIts cmIts cmBeth to Restrictive FeatureIts cmIts cmIts cmIts cmB	1								
BCtg     Silty clay loam     152 cm     203 cm     A-6, A-7-6     CH, CL       BVE     Silt loam     48 cm     56 cm     A-6, A-7-6     CH, CL       Btg     Silty clay     56 cm     152 cm     A-6, A-7-6     CH, CL       E     Silt loam     15 cm     48 cm     A-6, A-7-6     CH, CL       E     Silt loam     15 cm     48 cm     A-4     CL, CL-ML, ML Crowley (3 percent) Hydrologic Group Soil Drainage Class Corrosion Potential - Uncoated Steel Depth to Restrictive Feature Leton (3 percent) Hydrologic Group Soil Drainage Class Poorly drained Corrosion Potential - Uncoated Steel Depth to Restrictive Feature Edgerly (2 percent) Hydrologic Group Soil Drainage Class Poorly drained Corrosion Potential - Uncoated Steel Depth to Restrictive Feature		Horizon	Soil Texture	Upper Boundary	Lower Boundary	AASHTO	Unified		
Bt/E     Silt loam     48 cm     56 cm     A-6, A-7-6     CH, CL       Big     Silty clay     56 cm     152 cm     A-6, A-7-6     CH, CL       E     Silt loam     15 cm     48 cm     A-4, A-7-6     CH, CL       E     Silt loam     15 cm     48 cm     A-4, A-7-6     CH, CL       E     Silt loam     15 cm     48 cm     A-4     CL, CL-ML, ML   Corrowing Cass Soid Drainage Class Corrosion Potential - Uncoated Steel Depth to Restrictive Feature       Leton (3 percent)     Hydrologic Group     Soil Drainage Class     Poorly drained   Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature     Poorly drained     Corrosion Potential - Uncoated Steel   Depth to Restrictive Feature       Edgerly (2 percent)     Hydrologic Group     Soil Drainage Class     Poorly drained   Corrosion Potential - Uncoated Steel Depth to Restrictive Feature       Edgerly (2 percent)     Hydrologic Group     Soil Drainage Class     Poorly drained   Corrosion Potential - Uncoated Steel Depth to Restrictive Feature       Midland (2 percent)     Hydrologic Group     Soil Drainage Class     Poorly drained		Α	Silt loam	0 cm	15 cm	A-4	CL, CL-ML, ML		
BtgSilty clay56 cm152 cmA-6, A-7-6CH, CLESilt loam15 cm48 cmA-4CL, CL-ML, MLCrowley (3 percent)Hydrologic GroupSoil Drainage ClassSomewhat poorly drainedCorrosion Potential - Uncoated SteelDepth to Restrictive FeatureLeton (3 percent)Hydrologic GroupSoil Drainage ClassPoorly drainedCorrosion Potential - Uncoated SteelDepth to Restrictive FeatureLeton (3 percent)Hydrologic GroupSoil Drainage ClassPoorly drainedCorrosion Potential - Uncoated SteelDepth to Restrictive FeatureEdgerly (2 percent)Hydrologic GroupSoil Drainage ClassCorrosion Potential - Uncoated SteelDepth to Restrictive FeatureKidland (2 percent)Hydrologic GroupSoil Drainage ClassPoorly drainedCorrosion Potential - Uncoated SteelDepth to Restrictive FeatureMidland (2 percent)Hydrologic GroupSoil Drainage ClassPoorly drainedSoil Drainage ClassPoorly drained		BCtg	Silty clay loam	152 cm	203 cm	A-6, A-7-6	CH, CL		
E       Silt loam       15 cm       48 cm       A-4       CL, CL-ML, ML         Crowley (3 percent)       Hydrologic Group       Somewhat poorly drained       Somewhat poorly drained       Somewhat poorly drained         Soil Drainage Class       Somewhat poorly drained       Somewhat poorly drained       Somewhat poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature       Somewhat poorly drained       Somewhat poorly drained         Soil Drainage Class       Poorly drained       Somewhat poorly drained       Somewhat poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature       Soil Drainage Class       Poorly drained         Edgerly (2 percent)       Hydrologic Group       Soil Drainage Class       Poorly drained       Soil Drainage Class       Somewhat poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature       Soil Drainage Class       Poorly drained       Soil Drainage Class       Somewhat poorly drained         Midland (2 percent)       Hydrologic Group       Soil Drainage Class       Poorly drained       Soil Drainage Class       Soil Drainage Class		Bt/E	Silt loam	48 cm	56 cm	A-6, A-7-6	,		
Crowley (3 percent)         Hydrologic Group         Soil Drainage Class       Somewhat poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature             Leton (3 percent)         Hydrologic Group         Soil Drainage Class         Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature             Edgerly (2 percent)    Hydrologic Group          Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature             Edgerly (2 percent)         Hydrologic Group       Soil Drainage Class         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature		Btg	Silty clay	56 cm	152 cm	A-6, A-7-6	CH, CL		
Hydrologic Group         Soil Drainage Class       Somewhat poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Leton (3 percent)         Hydrologic Group         Soil Drainage Class         Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Soil Drainage Class         Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Midland (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained		E	Silt loam	15 cm	48 cm	A-4	CL, CL-ML, ML		
Soil Drainage Class       Somewhat poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature         Leton (3 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature         Depth to Restrictive Feature       Edgerly (2 percent)         Hydrologic Group       Soil Drainage Class         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature         Edgerly (2 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature         Midland (2 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained	Crow	ley (3 percent)							
Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Leton (3 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature	Hydro	ologic Group							
Depth to Restrictive Feature         Leton (3 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class         Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Midland (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained	Soil D	Drainage Class		Somewhat po	orly drained				
Leton (3 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class         Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Soil Drainage Class         Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Midland (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Soil Drainage Class       Poorly drained	Corro	sion Potential	- Uncoated Steel						
Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature         Edgerly (2 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Poorly drained         Depth to Restrictive Feature       Midland (2 percent)         Midland (2 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained         Soil Drainage Class       Poorly drained	Depth	n to Restrictive	Feature						
Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Depth to Restrictive Feature         Edgerly (2 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel       Poorly drained         Depth to Restrictive Feature       Midland (2 percent)         Midland (2 percent)       Hydrologic Group         Soil Drainage Class       Poorly drained         Soil Drainage Class       Poorly drained		(a							
Soil Drainage Class     Poorly drained       Corrosion Potential - Uncoated Steel     Poorly drained       Depth to Restrictive Feature     Image: Class of the strictive Feature       Edgerly (2 percent)     Poorly drained       Hydrologic Group     Poorly drained       Soil Drainage Class     Poorly drained       Corrosion Potential - Uncoated Steel     Poorly drained       Depth to Restrictive Feature     Image: Class of the strictive Feature       Midland (2 percent)     Poorly drained       Hydrologic Group     Soil Drainage Class       Soil Drainage Class     Poorly drained		•••							
Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Midland (2 percent)         Hydrologic Group         Soil Drainage Class         Poorly drained									
Depth to Restrictive Feature         Edgerly (2 percent)         Hydrologic Group         Soil Drainage Class       Poorly drained         Corrosion Potential - Uncoated Steel         Depth to Restrictive Feature         Midland (2 percent)         Hydrologic Group         Soil Drainage Class         Poorly drained		•							
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Hydrologic Group Soil Drainage Class Poorly drained Corrosion Potential - Uncoated Steel Depth to Restrictive Feature Midland (2 percent) Hydrologic Group Soil Drainage Class Poorly drained	Depth	Depth to Restrictive Feature							
Soil Drainage Class     Poorly drained       Corrosion Potential - Uncoated Steel     Poorly drained       Depth to Restrictive Feature     Midland (2 percent)       Midland (2 percent)     Feature       Soil Drainage Class     Poorly drained	Edge	Edgerly (2 percent)							
Corrosion Potential - Uncoated Steel Depth to Restrictive Feature  Midland (2 percent) Hydrologic Group Soil Drainage Class Poorly drained	Hydro	ologic Group							
Depth to Restrictive Feature       Midland (2 percent)       Hydrologic Group       Soil Drainage Class     Poorly drained	Soil D	Prainage Class		Poorly drained	Ł				
Midland (2 percent) Hydrologic Group Soil Drainage Class Poorly drained	Corro	sion Potential	- Uncoated Steel						
Hydrologic Group Soil Drainage Class Poorly drained	Depth	Depth to Restrictive Feature							
Hydrologic Group Soil Drainage Class Poorly drained	Midla	Midland (2 percent)							
Soil Drainage Class Poorly drained		•••							
-	-			Poorly drained	ł				
		-			-				
Depth to Restrictive Feature									

### **Soils Descriptions**



AASHTO Classification Definitions	
A-1, A-1-a, A-1-b	Granular materials (35% or less passing No. 200 sieve), sonte fragments, gravel and sand
A-2, A-2-4, A-2-5, A-2-6, A-2-7	Granular materials (35% or less passing No. 200 sieve), silty or clayey gravel and sand
A-3	Granular materials (35% or less passing No. 200 sieve), fine sand
A-4	Silt-Clay materials (more than 35% passing No. 200 sieve), silty soils
A-5	Silt-Clay materials (more than 35% passing No. 200 sieve), silty soils
A-6	Silt-Clay materials (more than 35% passing No. 200 sieve), clayey soils
A-7, A-7-5, A-7-6	Silt-Clay materials (more than 35% passing No. 200 sieve), clayey soils
A-8	Silt-Clay materials (more than 35% passing No. 200 sieve), clayey soils

СН	Fine-grained soils, silts and clays (liquid limit is 50% or more), Fat Clay
CL, CL-A (proposed), CL-K (proposed), CL-ML, CL-O (proposed),	Fine-grained soils, silts and clays (liquid limit is less than 50%), Lean Clay
CL-T (proposed)	
GC, GC-GM	Coarse-grained soils, Gravels, gravel with fines, Clayey Gravel
GM	Coarse-grained soils, Gravels, gravel with fines, Silty Gravel
GP, GP-GC, GP-GM	Coarse-grained soils, Gravels, clean gravels, Poorly Graded Gravel
GW, GW-GC, GW-GM	Coarse-grained soils, Gravels, clean gravels, Well-Graded Gravel
МН, МН-А, МН-К, МН-О, МН-Т	Fine-grained soils, silts and clays (liquid limit is 50% or more), Elastic Silt
ML, ML-A (proposed), ML-K (proposed), ML-O (proposed), ML-T	Fine-grained soils, silts and clays (liquid limit is less than 50%), Silt
(proposed)	
OH, OH-T (proposed)	Fine-grained soils, silts and clays (liquid limit is 50% or more), Organic Clay or Organic Silt
OL	Fine-grained soils, silts and clays (liquid limit is less than 50%), Organic Clay or Organic Silt
PT	Highly organic soils, Peat
SC, SC-SM	Coarse-grained soils, Sands, sands with fines, Clayey Sand
SM	Coarse-grained soils, Sands, sands with fines, Silty Sand
SP, SP-SC, SP-SM	Coarse-grained soils, Sands, clean sands, Poorly Graded Sand
SW, SW-SC, SW-SM	Coarse-grained soils, Sands, clean sands, Well-Graded Sand

Source

Natural Resources Conservation Service, Soil Survey Geographic (SSURGO) Database.

#### Disclaimer

This Soils Survey from Banks Environmental Data, Inc. has searched Natural Resources Conservation Service (NRCS) and the Soil Survey Geographic Database (SSURGO). All soil data presented on the map and in the details section are based on information obtained from NRCS. Although Banks performs quality assurance and quality control on all data, inaccuracies of the data and mapped locations could possibly be traced to the source. Banks Environmental Data, Inc. cannot fully guarantee the accuracy of the SSURGO database maintained by NRCS.



### Water & Oil/Gas Wells



1         669         CHENNAULT AFB         Water: Industrial         15 ft           2         USGS301108093091801         USGS         Water: Not Reported         15 ft           3         17019200960000         AMOCO PRODUCTION COMPANY         20         17 ft	Map ID	Well ID	Owner	Well Type	Elevation
	1	669	CHENNAULT AFB	Water: Industrial	15 ft
3 17019200960000 AMOCO PRODUCTION COMPANY 20 17 ft	2	USGS301108093091801	USGS	Water: Not Reported	15 ft
	3	17019200960000	AMOCO PRODUCTION COMPANY	20	17 ft

Source

U.S. Geological Survey, Louisiana Department of Natural Resources

Disclaimer

This well scan from Banks Environmental Data, Inc. has included a digital search of state and federal wells currently digitized in our geospatial database. Since this scan includes only well data that is currently mapped in our geospatial database, more wells could exist within the search area. For a complete well search or to locate more details, please contact Banks to obtain a full Water Well Report or Oil & Gas Well/Pipeline Search Report. More detailed individual well records can also be obtained from Banks for an additional cost, please reference a Well ID # from this well scan.

All well locations are based on information obtained from state and federal sources. Although Banks performs quality assurance and quality control on all data, inaccuracies of the records and mapped locations could possibly be traced to the specific regulatory authority or individual well driller. Banks Environmental Data, Inc. cannot fully guarantee the accuracy of the data or well location(s) of the maps and records maintained by the state and federal agencies.

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Mapped Sites Summary								
Database	Distance from Target Property	Map ID	Facility Site Name	Facility Site Address	Site Details Page #			
Sites are sorte	d by database tier,	database, an	d distance from the target site.	•				
PST	0.23 miles SW	1	Morgan Field C Store	3170 E McNeese St, Lake Charles, LA	21			

### **Unmapped Sites Summary**



### Banks Environmental Data performed a thorough search and no unmapped sites were found.



### MapID 1: PST - 3170 E McNeese St



### **PST - State/Tribal Storage Tank**

Map ID #1	PST	- State/Tribal Storage Tank	Source: LADEQ
Agency Interest ID: 235532		Secondary ID: NA	Banks ID: 235532
Morgan Field C Store			Rel. Loc.: 0.23 miles SW
3170 E McNeese St, Lake Charles, LA			Elevation: 16.4 feet (+16.4)
State Contact Name:			
Tank #:	#72103		
Status:	Active		
Capacity:			
Install Date:	8/31/2022		
Closure Certification Date:			
Removed:			
Above or Below Ground Tank:	below		
Piping Type:			
Tank Contents:	72103-gasoline & diesel		

### End of PST Sites Section

### **Dataset Descriptions and Sources**



Dataset	Source	Dataset Description	Update Schedule	Data Requested	Data Obtained	Data Updated	Source Updated
NPL National Priority List	EPA	NPL is the list of high priority hazardous waste sites in the United States eligible for long-term remedial action financed under the federal Superfund program or SEMS database (formerly known as the CERCLIS database). The EPA will only add sites to the NPL list based upon completion of the Hazard Ranking System (HRS) screening, public solicitation of comments about the proposed site, and after all comments have been addressed.	Quarterly	01/16/2023	01/16/2023	01/17/2023	12/22/2023
DNPL Delisted National Priority List	EPA	DNPL is a list of all sites that have been deleted from the EPA NPL list (SEMS database). These sites are taken off the NPL list usually due to no further response or remedial action being required on them. Notices to delete NPL sites are published in the Federal Register and become effective unless the EPA receives significant adverse or critical comments during the 30-day public comment period.	Quarterly	01/16/2023	01/16/2023	01/17/2023	12/22/2022
CER SEMS SEMS	EPA	The EPA maintains the SEMS database to track sites under the Comprehensive Environmental Response, Compensation, and Liability Act, a federal law designed to clean up abandoned hazardous waste sites. These sites are either proposed, listed or under review currently to be a part of the National Priority List.	Quarterly	01/16/2023	01/16/2023	01/17/2023	12/22/2022
CER SEMS NFRAP SEMS NFRAP	EPA	From the Superfund Enterprise Management System (SEMS) database No Further Remedial Action Planned or NFRAP have been removed from the listing. NFRAP sites may be sites where, following an initial investigation, no contamination was found, contamination was removed quickly without the site being placed on the NPL, or the contamination was not serious enough to require Federal Superfund action or NPL consideration.	Quarterly	01/16/2023	01/16/2023	01/17/2023	12/22/2023
RCRA COR RCRA CORRACTS	EPA	These sites are registered hazardous waste generators or handlers that fall under the Resource Conservation and Recovery Act (RCRA) and subject to corrective action activity.	Quarterly	01/18/2023	01/18/2023	01/24/2023	01/16/2023
RCRA TSD RCRA non-CORRACTS TSD	EPA	This database lists all treatment, storage and disposal of hazardous material sites that fall under the Resource Conservation and Recovery Act (RCRA). All hazardous waste TSD facilities are required to notify EPA of their existence.	Quarterly	01/18/2023	01/18/2023	01/24/2023	01/16/2023
RCRA GEN RCRA Generators	EPA	The EPA regulates all Hazardous Waste Generators subject to the Resource Conservation and Recovery Act (RCRA). They are classified by the quantity of hazardous waste generated. A Small Quantity Generator (SQG) generates between 100kg and 1,000 kg of waste per month. A Large Quantity Generator (LQG) generates over 1,000 kg of waste per month. A Conditionally Exempt SQG (CEG) generates less than 100 kg of waste per month.	Quarterly	01/18/2023	01/18/2023	01/24/2023	01/16/2023
FED BWN Federal Brownfields	EPA	A listing of sites that assist the EPA in collecting, tracking, and updating information of sites in relation to the Small Business Liability Relief and Brownfields Revitalization Act. These sites are real property that is either abandoned or underutilized where redevelopment or expansion is complicated by real or perceived environmental contamination.	Quarterly	12/19/2022	12/19/2022	12/26/2022	12/19/2022
FED IC Federal Institutional Control	EPA	This is a listing of Brownfield Management System (BMS) sites that have had Institutional Controls (ICs) placed on them. ICs are administrative restrictions, such as legal controls, that help minimize the potential for human exposure to known contamination by ensuring appropriate land or resource use. ICs are meant to supplement Engineering Controls and will rarely be the sole remedy at a site. ICs are a type of Activity and Use Limitation (AUL).	Quarterly	12/19/2022	12/19/2022	12/26/2022	12/19/2022
FED EC Federal Engineering Control	EPA	This is a listing of Brownfield Management System (BMS) sites that have had Engineering Controls (ECs) placed on them. ECs are physical methods or modifications put into place on a site to reduce or eliminate the possibility of human exposure to known contamination. ECs are a type of Activity and Use Limitation (AUL).	Quarterly	12/19/2022	12/19/2022	12/26/2022	12/19/2022

### **Dataset Descriptions and Sources**



Dataset	Source	Dataset Description	Update Schedule	Data Requested	Data Obtained	Data Updated	Source Updated
ERNS ERNS List	EPA/National Response Center	ERNS is a national database used to store information on unauthorized releases of oil and hazardous substances that have been reported to the National Response Center since 2001. The NRC is the sole federal point of contact for reporting oil and chemical spills. Prior to 2001 this information was maintained by the EPA.	Annually	01/09/2023	01/09/2023	01/09/2023	01/09/2023
ST NPL State/Tribal Equivalent NPL (LA)	LADEQ	This database contains 2 different types of records of hazardous properties in Louisiana that are considered or have already been through remediation. A confirmed status denotes that assessments have been performed and a determination made that (1) hazardous waste or substances are present at the site and (2) these sites are under the jurisdiction of the Inactive and Abandoned Sites regulations. A potential status is an indicator that sites are either waiting to be assessed or the assessment (investigation) is in progress.	Quarterly	01/20/2023	01/20/2023	01/27/2023	01/20/2023
ST CER State/Tribal Equivalent CERCLIS (LA)	N/A	This database is not currently available from this state. If this state does make this database available in the future, Banks Environmental Data will obtain it for reporting purposes.	N/A	N/A	N/A	N/A	N/A
SWLF State/Tribal Disposal or Landfill (LA)	LADEQ	This database contains listings of all Type I, Type II, Type III C&D solid waste landfills registered with the Solid Waste Program for the state of Louisiana.	Quarterly	01/20/2023	01/30/2023	02/01/2023	11/16/2022
LPST State/Tribal Leaking Storage Tank (LA)	LADEQ	This database is a list of all known leaking underground storage tanks as registered with the Remediation Services Division of the LDEQ. The Louisiana Department of Environmental Quality (LDEQ) migrated all environmental duality (LDEQ) migrated all environmental duality (LDEQ) migrated all environmental duality (ifferent databases with different formats to collect various types of data. The new system is now the primary tool used to track, collect and pull reports from DEQ data. After the migration took place the old database was locked and is no longer accessible. Prior to 1999 LDEQ reported LUSTs as individual instances of actual leaks. The new database reports LUSTs as tanks currently in remediation. Once a facility leak is evaluated and the remediation is closed, the site is no longer considered a 'LUST'. However, Banks will continue to report these sites as a LUST in the Regulatory Report.	Quarterly	01/20/2023	01/20/2023	01/27/2023	01/20/2023
LPST State/Tribal Leaking Storage Tank (LA)	EPA	The Tribal LUST database (maintained by EPA Region 6) provides information on leaking underground storage tank on tribal lands in Louisiana, Arkansas, Oklahoma, New Mexico and Tribal Nations.	Quarterly	12/29/2022	12/29/2022	12/29/2022	04/28/2022
PST State/Tribal Storage Tank (LA)	LADEQ	This database is a list of all known underground and aboveground storage tanks registered with the Remediation Services Division of the LDEQ.	Quarterly	01/20/2023	01/20/2023	01/27/2023	01/20/2023
PST State/Tribal Storage Tank (LA)	EPA	The Tribal UST database (maintained by EPA Region 6) provides underground storage tank information on tribal lands in Louisiana, Arkansas, Oklahoma, New Mexico and Tribal Nations.	Quarterly	12/29/2022	12/29/2022	12/29/2022	04/28/2022
ST IC State/Tribal Institutional Control (LA)	LADEQ	This database contains state Voluntary Cleanup Program sites that have an Institutional Control (ICs) placed on them. ICs are administrative restrictions, such as legal controls, that help minimize the potential for human exposure to known contamination by ensuring appropriate land or resource use.	Quarterly	02/09/2023	02/09/2023	02/09/2023	02/09/2023
ST EC State/Tribal Engineering Control (LA)	LADEQ	This database contains state Voluntary Cleanup Program sites that have Engineering Controls (ECs) placed on them. ECs are physical methods or modifications put into place on a site to reduce or eliminate the possibility of human exposure to known contamination.	Quarterly	02/09/2023	02/09/2023	02/09/2023	02/09/2023

### **Dataset Descriptions and Sources**



Dataset	Source	Dataset Description	Update Schedule	Data Requested	Data Obtained	Data Updated	Source Updated
VCP State/Tribal Voluntary Cleanup (LA)	LADEQ	This database contains information about sites that have been placed in the Louisiana Voluntary Remediation Program (VRP). The mission of the program is to provide a mechanism by which property owners (or potential owners) or others can clean up contaminated properties and receive a release of liability for further cleanup of historical contamination at a site. This release of liability flows to future owners of the property as well.	Quarterly	02/09/2023	02/09/2023	02/09/2023	02/09/2023
ST BWN State/Tribal Brownfield (LA)	N/A	This database is not currently available from this state. If this state does make this database available in the future, Banks Environmental Data will obtain it for reporting purposes.	N/A	N/A	N/A	N/A	N/A
HW State/Tribal Hazardous Waste (LA)	LADEQ	This database is not currently available from this state. If this state does make this database available in the future, Banks Environmental Data will obtain it for reporting purposes.	N/A	N/A	N/A	N/A	N/A
RCRA RCRA	EPA	This database lists all sites that fall under the Resource Conservation and Recovery Act (RCRA) and are not classifiable as treatment, storage, disposers of hazardous material, hazardous waste generator or subject to corrective action activity.	Quarterly	01/18/2023	01/18/2023	01/24/2023	01/16/2023
DRYC Dry Cleaners (LA)	N/A	This database is not currently available from this state. If this state does make this database available in the future, Banks Environmental Data will obtain it for reporting purposes.	N/A	N/A	N/A	N/A	N/A

### Disclaimer



The Banks Environmental Data Regulatory Database Report was prepared based upon data obtained from State, Tribal, and Federal sources known to Banks Environmental Data at the time the data was obtained. Great care has been taken by Banks in obtaining the best available data from the best available sources. However, there is a possibility that there are sources of data applicable or pertaining to this report's target property, and/or surrounding properties, to which Banks does not have access or has not accessed. Furthermore, although Banks Environmental Data performs quality assurance and quality control on all data, including data it obtains, Banks recognizes that inaccuracies in data from these sources may, and do, exist; accordingly, inaccurate data may have been used or relied upon in the preparation of this report. Even though Banks Environmental Data performs a thorough and diligent search to locate and fix any inaccuracies in the data relied upon in the preparation of this report, Banks cannot guarantee or warrant the accuracy of the locations, information, data, or report. The purchaser of this report accepts this report "as is" and assumes all risk related to any potential in accuracy contained in the report or not reported in it, whether due to a reliance by Banks Environmental Data on inaccurate data, or for any other reason [including but not limited to the negligence or express negligence of Banks Environmental Data]. If this report is being used for the Records Review section of a Phase I Site Assessment according to the ASTM 1527-21, for EPA's All Appropriate Inquiry, or for any other purpose (public or private), all liability and responsibility is assumed by the Environmental Professional or other individual or entity acquiring the report.

> Banks Environmental Data, Inc. - PO Box 12851 - Austin, TX 78711 - 800.531.5255 P - 512.478.1433 F www.banksenvdata.com
# **APPENDIX D**

Historical Aerial Photographs























# **APPENDIX E**

City Directory Report

**Prepared for:** 

SOUTHLAND ENVIRONMENTAL LLC 510 Clarence St Lake Charles, LA 70601



# CityCorbina Rd TractLake Charles, LA 70607DirectoryCalcasieu CountyReportPO #: 12055ES-141754 Friday, March 17, 2023

CTORY REPORT	BAN
March 17, 2023	ENVIRONMEN A DIVISION OF THE

DATA GROU



Street	Address Ranges Searched
Advent Ct	Any addresses
Basin Way	Any addresses
Cabot Dr	Any addresses
Corbina Rd	100-4000
E McNeese St	2700-4000
E Prien Lake	4228-4644 (evens)
Fairwood Ln	Any addresses
Forestwood Dr	Any addresses
Gardenwood Pkwy	Any addresses
James Ct	Any addresses
Lake Crest Dr	Any addresses
Meadow Brook Way	Any addresses
Rosehill Dr	Any addresses
Village Ln	Any addresses



## **RESEARCH PROTOCOL**

Banks Environmental Data, Inc. (Banks) has completed your request for a historical tenant search for the above site. The information in this report was developed to aid the Environmental Engineer/Consultant in determining a history of previous uses of a subject property in order to help identify the likelihood of past uses having led to recognized environmental conditions in connection with a subject property as specified by ASTM 1527-05 Section 8.3. Banks has researched Haines, Coles and Polk crisscross directories back to 1940 or to the earliest year available at the Allen County Public Library in Fort Wayne, IN for any occurrences of the above address. The findings are listed in the table below.

CITY DIRECT	ORY REPORT
ES-141754	March 17, 2023



### **CURRENT TENANT INFORMATION**

#### Source: Polk's 2022 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	Personal residences (3013, 3032, 3048, 3052,
		3056, 3060, 3068)
3024 Basin Way	Nearby St	(listed as "no current listing")
Cabot Dr	Nearby St	Personal residences (listed at 4308, 4328)
Corbina Rd	Nearby St	(no tenants listed in address range)
E McNeese St	Nearby St	(no tenants listed in address range)
E Prien Lake Rd	Nearby St	(no tenants listed in address range)
3247 Fairwood Ln	Nearby St	Calibrated Performance LLC (nonclassified)
Fairwood Ln	Nearby St	Personal residences (listed at 3203, 3207, 3211,
		3219, 3223, 3227, 3231, 3234, 3235, 3238, 3239,
		3242, 3243, 3250, 3251, 3254, 3255, 3258, 3259,
		3267, 3271, 3275, 3279, 3283, 3287)
3215 Fairwood Ln	Nearby St	(listed as "no current listing")
Forestwood Dr	Nearby St	Personal residences (listed at 3009, 3013, 3017,
		3020, 3024, 3032)
4316 Gardenwood Pkwy	Nearby St	Personal residence
James Ct	Nearby St	(street not listed)
4430 Lake Crest Dr	Nearby St	A1 Notary Mobile Service
Lake Crest Dr	Nearby St	Personal residences (listed at 3214, 3218, 3222,
		3226, 3234, 3235, 3238, 3246, 3258, 3259, 3262,
		3263, 3266, 3270, 3274, 4402, 4403, 4406, 4407,
		4410, 4411, 4414, 4415, 4418, 4419, 4422, 4423,
		4426, 4427, 4431, 4434, 4435, 4438, 4439, 4442)
Meadow Brook Way	Nearby St	Personal residences (listed at 4402, 4406, 4407,
		4410, 4414, 4415, 4418, 4419, 4422, 4423, 4426,
		4427, 4430, 4431, 4434, 4435, 4438, 4442)
Rosehill Dr	Nearby St	Personal residences (listed at 3200, 3203)
922 Village Ln	Nearby St	Abate's Plumbing (contractors)
4315 Village Ln	Nearby St	Apartments (4 tenants listed)
Village Ln	Nearby St	Personal residences (listed at 803, 804, 815,
		816, 827, 828, 903, 904, 915, 916, 934)

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CITY DIRECTORY REPORT		
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# HISTORICAL TENANT INFORMATION

#### Source: Polk's 2017 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	Personal residences (3040, 3060)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(no tenants listed in address range)
E McNeese St	Nearby St	(no tenants listed in address range)
E Prien Lake Rd	Nearby St	(no tenants listed in address range)
Fairwood Ln	Nearby St	Personal residences (listed at 3219, 3223, 3231,
		3234, 3238, 3239, 3243, 3247, 3251, 3258, 3259)
3283 Fairwood Ln	Nearby St	(listed as "no current listing")
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	Personal residences (listed at 4407, 4423, 4427)
Meadow Brook Way	Nearby St	Personal residences (listed at 4406, 4414, 4415,
Decekill De	Na subar Ct	4418, 4427)
Rosehill Dr	Nearby St	(street not listed)
922 Village Ln	Nearby St	Abate's Plumbing (contractors)
Village Ln	Nearby St	Personal residences (listed at 803, 804, 815,
		816, 828, 903, 904, 915, 916, 934)
827 Village Ln	Nearby St	(listed as "no current listing")

CITY DIRECTORY REPORT		
ES-141754	March 17, 2023	



#### Source: Polk's 2012 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(no tenants listed in address range)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Dyno Nobel Inc (explosives)
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
922 Village Ln	Nearby St	Abate's Plumbing (contractors)
Village Ln	Nearby St	Personal residences (listed at 803, 804, 815,
		816, 828, 903, 904, 915, 916, 934)
827 Village Ln	Nearby St	(listed as "no current listing")

CITY DIRECTORY REPORT		
ES-141754	March 17, 2023	



#### Source: Polk's 2007 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(no tenants listed in address range)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Acme Sandblasting & Painting
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
922 Village Ln	Nearby St	Abate's Plumbing (contractors)
Village Ln	Nearby St	Personal residences (listed at 803, 804, 815,
		816, 827, 828, 903, 904, 915, 916, 934)

CITY DIRECTORY REPORT		
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#### Source: Polk's 2002 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(no tenants listed in address range)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Acme Sandblasting & Painting
		Dyno Nobel Mid America (detergents/soaps)
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
922 Village Ln	Nearby St	Abate's Plumbing (contractors)
Village Ln	Nearby St	Personal residences (listed at 803, 804, 816,
		827, 904, 915, 916)
815, 828, 903 Village Ln	Nearby St	(listed as "not verified")

CITY DIRECTORY REPORT		
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#### Source: Polk's 1997 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(no tenants listed in address range)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Acme Sandblasting & Painting
		Strawn Explosives
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
Village Ln	Nearby St	(street not listed)

CITY DIRECTORY REPORT		
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# Source: Polk's 1992 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(street not listed)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Clark College Inc (professional driving school)
		Pioneer Storage Service Inc
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
Village Ln	Nearby St	(street not listed)

CITY DIRECTORY REPORT		
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#### Source: Polk's 1986-87 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(street not listed)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Pioneer Storage Service Inc
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
Village Ln	Nearby St	(street not listed)

CITY DIRECTORY REPORT		
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#### Source: Polk's 1980 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(street not listed)
E McNeese St	Nearby St	(no tenants listed in address range)
4420 E Prien Lake Rd	Nearby St	Allison Moving & Storage Co Inc
		Pioneer Storage Service Inc
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
Village Ln	Nearby St	(street not listed)

Note: Polk's 1981 Lake Charles, LA City Directory not available.

CITY DIRECTORY REPORT		
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# Source: Polk's 1975 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(street not listed)
E McNeese St	Nearby St	(street not listed)
(unnumbered) E Prien Lake Rd	Nearby St	Allison Moving & Storage Co Inc
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
Village Ln	Nearby St	(street not listed)

CITY DIRECTORY REPORT		
ES-141754	March 17, 2023	



# Source: Polk's 1970 Lake Charles, LA City Directory

Address	Location	Tenants
Advent Ct	Nearby St	(street not listed)
Basin Way	Nearby St	(street not listed)
Cabot Dr	Nearby St	(street not listed)
Corbina Rd	Nearby St	(street not listed)
E McNeese St	Nearby St	(street not listed)
E Prien Lake Rd	Nearby St	(no tenants listed in address range)
Fairwood Ln	Nearby St	(street not listed)
Forestwood Dr	Nearby St	(street not listed)
Gardenwood Pkwy	Nearby St	(street not listed)
James Ct	Nearby St	(street not listed)
Lake Crest Dr	Nearby St	(street not listed)
Meadow Brook Way	Nearby St	(street not listed)
Rosehill Dr	Nearby St	(street not listed)
Village Ln	Nearby St	(street not listed)

Note: Earlier directories are available for Lake Charles, LA but do not cover the research area.



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# **APPENDIX F**

Site Photographs



**Photograph 1.** View of north boundary of subject property facing east.



Photograph 2. View of across center of subject property facing south. Southland Environmental, LLC



**Photograph 3.** View across north portion of subject property facing southwest.



Photograph 4. View of north boundary of subject property facing west. Southland Environmental, LLC



**Photograph 5.** View of east boundary of subject property facing south



**Photograph 6** View of south boundary of subject property facing east.



**Photograph 7.** View across east portion of subject property facing northeast.



 Photograph 8.

 View of south boundary of subject property facing west.

 Southland Environmental, LLC



**Photograph 9.** View from south boundary of subject property facing south. Future PST site in background.



**Photograph 10.** View of west boundary of subject property facing north.



**Photograph 11.** View of north boundary of subject property facing west.



View of soil fill activities on north boundary of subject property. Southland Environmental, LLC



**Photograph 13.** View drainage swale which runs north/south through center of subject property.



Photograph 14.View of cattle grazing area near north boundary of subject property.Southland Environmental, LLCPage 7 of 8


**Photograph 15.** View of typical ground surface of subject property.

# **APPENDIX G**

Interview Documentation

## Phase I: Environmental Questionnaire for Persons Knowledgeable of Site

Name of Landowner: James Palma- Owner East Prien Lake Properties, LLC

- How long have you owned the investigated property? Since 2006
- What, if any, were the known past uses of the investigated property? Only use for hunting and cattle grazing
- If known, who was the previous owner of the investigated property? Not known
- Have there ever been any Underground Storage Tanks (USTs) in service at the investigated property? If so, what were they utilized for? No
- Are there any pipelines on the investigated property? If so, what substances do they transport (if known)?

No

• Have there ever been any pits or ponds constructed on the investigated property? If so, what was their purpose?

No

- Have any fires ever occurred on the investigated property, or has the local fire department ever had to respond to a call at this location? No
- Have there ever been any instances where federal environmental agencies or local health department have had to respond at this location? No
- Is there any other information, not requested above, that would be applicable to this Phase I investigation?

No

Signature of Person Interviewed/Interviewer:

Date: 3-28-2023

## Phase I: Environmental Questionnaire for Persons Knowledgeable of Site

Name ofInterview	ved/Affiliation:	<u>.JA-lbA)</u>	$R_{\underline{i}\underline{i}\underline{Y}}$ ,	
Name of Interview	ver: <u> </u>	Aine	Johnson	
Site Location:	Corbing	Rd -	EAST side	

• Are you aware of any known past or present environmental impacts associated with the investigated property?

No

• Do you know of any possible sources for environmental impacts from the properties surrounding the investigated tract?

No

• Is there any additional information that LDEQ is aware of regarding the investigated tract or surrounding properties that would be applicable to this Phase I investigation?

Any documentation that the LDEQ would have on file for this area is available on the LDEQ EDMS.

Signature of Interviewer:	
Date of Interview:	

# **APPENDIX H**

Resumes

### C. BLAINE JOHNSON, P. E. PROJECT MANAGEMENT/OVERSIGHT SITE INVESTIGATION AND REMEDIATION SOIL AND GROUNDWATER REMEDIATION HAZARDOUS/SOLID WASTE MANAGEMENT GROUNDWATER MONITORING AND REPORTING ENVIRONMENTAL PERMITTING AND ENGINEERING WETLANDS AND NEPA PERMITTING/DOCUMENTATION

## **EDUCATION**

B.S., Civil Engineering, McNeese State University, 1984

### **PROFESSIONAL HISTORY**

May 2018-Present	Owner and Senior Engineer, Southland Environmental, LLC	
1999-May 2018	Senior Engineer, Arabie Environmental Solutions, LLC	
	(Formerly Triegel & Associates, Inc.)	
1996-1999	Senior Engineer, Triegel & Associates, Inc. (LA Office)	
1995-1996	Senior Project Manager, RETEC Inc., Lake Charles, LA	
1991-1995	Senior Engineer, Radian Corporation, Baton Rouge, LA	
1987-1991	Project Manager, IT Corporation, Baton Rouge, LA	
1985-1987	Project Engineer, Trinity Engineering Testing Corporation, Dallas, TX	

### PROFESSIONAL REGISTRATIONS AND AFFILIATIONS

- Registered Professional Engineer in Louisiana
- Louisiana Engineering Society
- Louisiana Air and Waste Management Association
- Louisiana Chemical Industry Alliance

#### **REPRESENTATIVE EXPERIENCE**

Mr. Johnson has over thirty-five years of experience as a Project Manager/Engineer having performed project work on various environmental projects including civil and geotechnical design, subsurface remediation, regulatory permitting, and surface and subsurface investigations. He has been involved for over 20 years in the oversight and preparation of numerous Section 404/10 Permit Applications and provided project management and regulatory interaction with the US Army Corps of Engineers and other programmatic agencies and entities participating in the permitting process for projects with wetlands impacts and projects occurring within the Waters of the United States, such as dredging and construction of marine vessel required structures.

He is experienced in projects dealing with engineering investigation, design, construction, closure, and remediation of hazardous and solid waste management facilities, which are regulated by the pertaining HSWA, RCRA, and CERCLA requirements. Mr. Johnson is experienced with the engineering and permitting procedures in preparation of hazardous and solid waste applications for existing facilities as well as Post-Closure permits for treatment, disposal, and storage facilities which are in operation and are being closed. He has technical experience in the operation and maintenance of groundwater/non-aqueous phase liquids/leachate recovery and treatment systems. He is able to provide the project management, technical applications, and regulatory interaction pertinent for the performance of these types of projects. Mr. Johnson has provided Project Manager and Engineer services required in accordance with the National Environmental Policy Act (NEPA) for various projects in the Gulf Coast Region.

### **REGULATORY COMPLIANCE**

Preparation, review, and certification of permit applications for solid waste disposal facilities, stormwater discharge permit applications for various commercial and industrial clients, and air permit and renewal applications for solid waste facilities and chemical manufacturing facilities.

Preparation of numerous Section 404/10 Permit Applications and provided project management and regulatory interaction with the US Army Corps of Engineers, Louisiana Department of Coastal Management, and other programmatic agencies and entities participating in the permitting process.

Project Manager and Engineer for engineering and construction projects in Louisiana that entailed the performance of services required to provide the documentation necessary for Environmental Assessment and/or Categorical Exclusion in accordance with the NEPA, LADOTD, and FHWA regulations and guidelines. He has also served as the Project Manager and Engineer for projects entailing data gathering, compilation, and documentation preparation of NEPA required EA's for multiple sites in Louisiana, Texas, Alabama, Arkansas, Mississippi, and Florida.

Preparation and development of RCRA Facility Investigation (RFI) strategy and workplan and current condition documents for clients in Louisiana and Arkansas.

Preparation of certification reports for various treatment, storage, and disposal facilities (surface impoundments, tanks, landfills), to verify compliance with RCRA, and other state and local regulations.

Preparation of hazardous waste permit applications (Part A and Part B) and post-closure care permits applications, including providing technical review and regulatory interaction on behalf of the clients in Louisiana and Arkansas.

#### **CORRECTIVE ACTION DESIGN AND CONSTRUCTION**

Project Manager for the design, implementation, and operation and maintenance of corrective action plans for various underground storage tank projects. This included regulatory agency negotiation and recommendations prior to commencement of the corrective actions. Corrective actions that were implemented include the recovery and treatment of dissolved and free-phase petroleum hydrocarbons in soils and groundwater due to petroleum fuel releases. Other remediation techniques included source removal by excavation, in-situ treatment via introduction of contaminant reduction compounds, and engineering controls to prevent migration and infiltration of materials throughout the affected areas.

Evaluation, design, implementation, and third party oversight of remedial actions and retrofits of RCRA hazardous wastes units in Louisiana, Arkansas, and Mississippi.

Project Manager for the installation and operation/maintenance of a groundwater recovery system. This recovery system was designed to separately recover impacted groundwater and free-phase chlorinated solvent (DNAPL) while maintaining hydraulic containment of the site through the use of a dual pump system. The system has recovered over 25,000 gallons of DNAPL product.

Remedial design and permitting for the closure of several surface impoundments, and solid waste landfills (in accordance with RCRA) in Louisiana, Mississippi, and Arkansas.

Implementation of construction quality assurance activities and subsequent certification of closure reports for surface impoundments and landfills in Louisiana, Mississippi, and Arkansas.

Design of the expansion and partial closure of an existing hazardous waste landfill in Mississippi.

Development of design alternatives, prepared construction and post closure cost estimates for the eventual technical design for a hazardous waste landfill in southern Arkansas.

Responsible for quality assurance activities of a dual pond closure and remediation in south Louisiana which included documentation, inspections, field testing and verification of various remediation and construction activities. These closure and remediation activities included steam stripping and centrifuging of pond sludges, placement of remediated materials, and installation of the final cover system.

#### ENVIRONMENTAL MONITORING AND ASSESSMENT

Management and participation of investigations of various sites including petroleum fuel service stations, commercial businesses, and industrial and manufacturing facilities.

Management and participation of investigations pertaining to surface releases and subsurface migration of various chemicals (chlorinated and brominated organics, and other compounds) at several sites in Louisiana, Arkansas, and Mississippi. The investigations were performed as pre-RFI activities under the corrective measures program or were used as part of the program after investigation activities were initiated.

Response to a spill of a chlorinated solvent (DNAPL) from an underground pipeline into nearby ditches. The scope of work entailed the installation of borings and monitoring wells which were used to monitor the groundwater flow direction and gradient, refine hydraulic coefficients based on aquifer testing, define stratigraphy at the site, and delineate the horizontal and vertical extent of the release. Bioassay samples were collected and it was determined that naturally-occurring microorganisms were present. The regulatory agency was convinced that in selected aquifers, the contaminant was "self-remediating" and that no actions were warranted other than monitoring the decline in concentrations of the contaminant.

Management and performance of several Phase I and II property transfer site assessments for industrial and commercial clients. These assessments of various exploration and production facilities, oil and gas gathering and refining facilities, and chemical facilities were used to identify possible environmental liabilities for buyer, lenders, and sellers.

Participated in the report preparation and field investigation phases of a multi-location real estate transfer/site assessment project determining the environmental liabilities due to the presence of on-site underground storage tanks.

### JARED KING, P. G.

#### ENVIRONMENTAL INVESTIGATIONS ENVIRONMENTAL PERMITTING ENVIRONMENTAL REMEDIATION

### **EDUCATION**

McNeese State University, B.S., Environmental Science, December 2004

### **PROFESSIONAL HISTORY**

04/18-Date	Owner and Senior Environmental Scientist, Southland Environmental,
	LLC
07/03-05/18	Senior Environmental Scientist, Arabie Environmental Solutions, LLC
01/03-07/03	Environmental Co-op, Sasol North America

### **PROFESSIONAL REGISTRATIONS**

Registered Professional Geoscientist in Louisiana, No. 836

## TRAINING/CERTIFICATION

- Southwest Safety Council Training
- Westlake South Site Specific Safety Training
- OSHA 40-Hour HAZWOPER Training
- RCRA Hazardous Waste Training
- Transportation Worker Identification Credential (TWIC)
- Certified Stormwater Inspector

### **REPRESENTATIVE EXPERIENCE**

Mr. King has over ten years experience in environmental projects including environmental sampling, permit applications, and maintenance and monitoring of several groundwater remediation systems.

Mr. King has worked on numerous environmental projects. For the past fourteen years, Mr. King has managed and performed RCRA compliance inspections, operated a groundwater recovery system, and operated a stormwater treatment system at the a local industrial facility. He has collected stormwater samples for this facility. He has also inspected and monitor leachate for two hazardous waste landfills.

Mr. King has worked on the installation of soil boring and groundwater monitoring wells. He has performed sampling and development of groundwater monitoring wells including low-flow purging and sampling. He has collected stormwater samples for various industrial and commercial facilities. He has been involved maintenance and outfall monitoring of several recovery systems and has prepared discharge monitoring reports (DMRs) for these outfalls. He has also worked on groundwater monitoring reports for commercial and industrial facilities. He is also proficient with integration and mapping of

Global Position System (GPS) data into Geographical Information Systems (GIS) software.

Mr. King has performed numerous Phase I Environmental Site Assessments (ESA) in accordance with the ASTM standards for real estate transactions. These Phase I ESAs have been performed in Louisiana, Texas, Mississippi, Alabama, and Florida. He has prepared checklists for FCC towers and structures and historical reports in accordance with the National Environmental Protection Act guidelines. He was worked on Army Corps of Engineers Permit Applications, Coastal Use Permit Application, and assisted in wetland delineations. He has performed field activities associated with installation, removal, and processing of sediment traps as part of an estuary evaluation. Mr. King has also assisted engineers with the preparation and submittal of Solid Waste Permit Application to the LDEQ.

Mr. King has extensive experience with the performance of Phase II ESAs, which have included assessments of soil, sediment, surface water, storm water, and groundwater on non-developed, commercial, light industrial, and heavy industrial properties. Mr. King has supervised and/or performed various methods of soil and groundwater collection and has processed samples utilizing various types of sampling methods. Such sampling methods include, but are not limited to, EPA Method 5035 soil sampling for volatile organic compounds and collection of groundwater samples utilizing low-flow groundwater sampling procedures. Mr. King has also performed various soil-vapor studies which have included the use of vacuum-air canisters and methane detection meters.

Mr. King has performed and documented Health and Safety Monitoring and is familiar with the operation of Organic Vapor Analyzers. He also has performed several monitoring tasks using gas detection pumps and detector tubes.

Mr. King has assisted in the maintenance and operation of a large groundwater monitoring and recovery system at an industrial facility. He has been involved in the shut down and start up of the recovery system, removal, reinstalling, and jetting of recovery wells as part of maintenance activities. He has performed troubleshooting and repaired on pneumatic pumps and controllers. Mr. King has repaired submersible electric pumps, motors, and motor leads. He has maintained transfer lines on the recovery systems and performed sampling of the recovery wells, monitoring wells, collection tanks, and transfer headers.

While working as a co-op, Mr. King has assisted in environmental projects and environmental incident investigations. He has performed weekly hazardous waste inspections and assisted with hazardous waste profiling and shipments. He has assisted engineers in air compliance permitting and calculating emissions for production units. He has performed groundwater sampling events and has coordinated maintenance activities on a groundwater recovery system. During the groundwater sampling events, Mr. King has utilized low-flow purging and sampling techniques and equipment.

# **APPENDIX I**

Environmental Professional's Statement

# ENVIRONMENTAL PROFESSIONAL'S STATEMENT

Southland Environmental, LLC declares that, to the best of its knowledge and belief, Southland Environmental, LLC personnel meet the definition of Environmental professional as defined in §312.10 of 40 CFR 312 and,

Southland Environmental, LLC personnel have specific qualifications based on education, training, and experience to assess a property of the nature, history, and setting of the subject property. Southland Environmental, LLC personnel have developed and performed the all appropriate inquiries in conformance with the standards and practices set forth in 40 CFR Part 312.

APPENDIX 10. DR-4559-LA and EM-3538-LA Public Notice and FONSI

# PUBLIC NOTICE FEMA-4559-DR-LA and FEMA-3538-EM-LA

The Federal Emergency Management Agency (FEMA) hereby gives notice to the public of its intent to reimburse eligible applicants for eligible costs for assistance to repair and/or replace facilities damaged by Hurricane Laura, occurring August 22 to August 27, 2020. This notice applies to the Public Assistance (PA), Individual Assistance (IA), and Hazard Mitigation Grant (HMGP) programs implemented under the authority of the Robert T. Stafford Disaster Relief and Emergency Assistance Act, 42 U.S.C. §§ 5121-5207.

Under an Emergency declaration (FEMA 3538-EM–LA) signed by the President on August 23, 2020 and amended on August 25, 2020, and August 26, 2020, FEMA is authorized to identify, mobilize, and provide at its discretion, equipment and resources necessary to alleviate the impacts of the emergency. Emergency protective measures Category B, limited to direct federal assistance under the Public Assistance program and reimbursement for mass care including evacuation and shelter support are available for the following Parishes: Acadia, Allen, Ascension, Assumption, Beauregard, Calcasieu, Cameron, East Baton Rouge, East Feliciana, Evangeline, Iberia, Iberville, Jefferson, Jefferson Davis, Lafayette, Lafourche, Livingston, Orleans, Plaquemines, Pointe Coupee, St. Bernard, St. Charles, St. Helena, St. James, St. John the Baptist, St. Landry, St. Martin, St. Mary, St. Tammany, Tangipahoa, Terrebonne, Vermilion, Washington, West Baton Rouge and West Feliciana. The President also authorized Public Assistance-Category B to include reimbursement for eligible emergency protective measures for all parishes.

Under a major disaster declaration (FEMA-4559-DR-LA) (for the incident beginning August 22, 2020) signed by the President on August 28, 2020 and amended August 30, 2019 and August 31, 2020, the following parishes have been designated eligible for PA Category A: Acadia, Allen, Beauregard, Bienville, Bossier, Calcasieu, Cameron, Catahoula, Evangeline, Grant, Jackson, Jefferson Davis, Lincoln, Natchitoches, Rapides, Sabine, Vermilion, Vernon, Webster, and Winn Parishes. All Parishes are designated eligible for PA Category B (emergency protective measures), including Direct Federal Assistance under the major disaster declaration. Currently, the following Parishes are designated eligible for PA Category C-G: Allen, Beauregard, Calcasieu, Cameron, Jefferson Davis, and Vernon Parishes. Additional parishes may be designated at a later date.

Under FEMA-4559-DR- LA the following parishes have been designated eligible for IA: Acadia, Allen, Beauregard, Caddo, Calcasieu, Cameron, Grant, La Salle, Jackson, Jefferson Davis, Lincoln, Morehouse, Natchitoches, Ouachita, Rapides, Sabine, St. Landry, Union, Vermilion, Vernon, and Winn Parishes. Additional parishes may be designated at a later date. All parishes in the State of Louisiana are eligible for HMGP under FEMA-4459-DR- LA.

This public notice concerns activities that may affect historic properties, activities that are located in or affect wetland areas or the 100-year floodplain, and critical actions within the 500-year floodplain. Such activities may adversely affect the historic property, floodplain or wetland, or may result in continuing vulnerability to flood damage.

Presidential Executive Orders 11988 and 11990 require that all federal actions in or affecting the floodplain or wetlands be reviewed for opportunities to relocate, and evaluated for social, economic, historical, environmental, legal and safety considerations. Where there is no opportunity to relocate, FEMA is required to undertake a detailed review to determine what measures can be taken to minimize future

damages. The public is invited to participate in the process of identifying alternatives and analyzing their impacts through this notification.

FEMA has determined that for certain types of facilities there are normally no alternatives to restoration in the floodplain/wetland. These are facilities that meet all of the following criteria: 1) FEMA's estimate of the cost of repairs is less than 50% of the cost to replace the entire facility, and is less than \$100,000; 2) the facility is not located in a floodway; 3) the facility has not sustained major structural damage in a previous Presidentially declared flooding disaster or emergency; and 4) the facility is not critical (e.g., the facility is not a hospital, generating plant, emergency operations center, or a facility that contains dangerous materials). FEMA intends to provide assistance for the restoration of these facilities to their pre-disaster condition, except that certain measures to mitigate the effects of future flooding or other hazards may be included in the work. For example, a bridge or culvert restoration may include a larger waterway opening to decrease the risk of future washouts.

For routine activities, this will be the only public notice provided. Other activities and those involving facilities that do not meet the four criteria are required to undergo more detailed review, including study of alternate locations. Subsequent public notices regarding such projects will be published if necessary, as more specific information becomes available.

In many cases, an applicant may have started facility restoration before federal involvement. Even if the facility must undergo detailed review and analysis of alternate locations, FEMA will fund eligible restoration at the original location if the facility is functionally dependent on its floodplain location (e.g., bridges and flood control facilities), or the project facilitates an open space use, or the facility is an integral part of a larger network that is impractical or uneconomical to relocate, such as a road. In such cases, FEMA must also examine the possible effects of not restoring the facility clearly outweighs the Executive Order requirements to avoid the floodplain/wetland, and that the site is the only practicable alternative. State of Louisiana and local officials will confirm to FEMA that proposed actions comply with all applicable State and local floodplain management and wetland protection requirements.

FEMA intends to provide IA program funding for disaster-related housing. These actions may adversely affect a floodplain or wetland or may result in continuing vulnerability to floods. These actions may include repair, restoration, or construction of housing or private bridges, purchase and placement of travel trailers or manufactured housing units, or repair of structures as minimum protective measures. This will be the only public notice concerning these actions.

FEMA also intends to provide HMGP funding to the State of Louisiana to mitigate future disaster damages. These projects may include construction of new facilities, modification of existing facilities, undamaged facilities, relocation of facilities out of floodplains, demolition of structures, or other types of projects to mitigate future disaster damages. In the course of developing project proposals, subsequent public notices will be published, if necessary, as more specific information becomes available.

The National Historic Preservation Act requires federal agencies to take into account the effects of their undertakings on historic properties. Those actions or activities affecting buildings, structures, districts or objects 50 years or older or that affect archeological sites or undisturbed ground will require further review to determine if the property is eligible for listing in the National Register of Historic Places (Register). If the

property is determined to be eligible for the Register, and FEMA's undertaking will adversely affect it, FEMA will provide additional public notices. For historic properties not adversely affected by FEMA's undertaking, this will be the only public notice.

Interested persons may obtain information about these actions or a specific project by writing to Jerame Cramer, Environmental Historic Preservation Advisor (EHAD), Federal Emergency Management Agency, 1500 Main St., Baton Rouge, LA 70802 or by emailing fema-liro-ehp-pa@fema.dhs.gov. Comments should be sent in writing within 30 days of the date of this notice.

#### FEDERAL EMERGENCY MANAGEMENT AGENCY FINDING OF NO SIGNIFICANT IMPACT ST. LOUIS CATHOLIC HIGH SCHOOL CAMPUS CHANGE OF LOCATION PROPOSAL CALCASIEU PARISH, LOUISIANA FEMA-4559-DR-LA

#### BACKGROUND

Hurricane Laura made landfall on August 27, 2020, at Cameron, Louisiana, as a Category 4 storm with sustained winds of more than 150 miles per hour and a minimum central pressure of 939 millibars. President Donald Trump declared a major disaster for the State of Louisiana (FEMA-DR- 4559-LA) on August 28, 2020, authorizing the U.S. Department of Homeland Security's (DHS) Federal Emergency Management Agency (FEMA) to provide federal assistance in designated areas of Louisiana. This assistance is under the Robert T. Stafford Disaster Relief and Emergency Assistance Act (Stafford Act), Public Law (P.L.) 93-288, as amended.

The Society of the Roman Catholic Church of the Diocese of Lake Charles has submitted an application for Federal Emergency Management Agency (FEMA) grant funding under FEMA's Public Assistance Program being administered in response to FEMA-4559-DR-LA. The St. Louis School Campus was substantially damaged by Hurricane Laura's winds and coastal flooding and were deemed eligible for grant funding to relocate and reconstruct the St. Louis High School Facilities at an alternative site. The applicant proposes to demolish the damaged facilities, render them safe, and then construct new facilities that includes the development of new school buildings, a gymnasium, a courtyard, a central plant, a pavilion, detention ponds, and six sports fields/courts, such as a football field, baseball field, softball field, soccer field, practice field, and tennis courts in Lake Charles, Calcasieu Parish, Louisiana. The facility is proposed to be reconstructed east of the intersection of Corbina Road and James Court in Lake Charles (30.1817°N, -93.1586°W) located approximately 4.0 miles southeast of the current location. The parcel is approximately 47 acres.

In accordance with the Council on Environmental Quality (CEQ) regulations implementing NEPA (40 Code of Federal Regulations (CFR) Parts 1500–1508) and FEMA's Instruction 108-1-1 for implementing NEPA, an Environmental Assessment (EA) was prepared. The purpose of this EA is to analyze the potential environmental impacts associated with the change of location proposal and to determine whether to prepare an Environmental Impact Statement (EIS) or a Finding of No Significant Impact (FONSI).

Three project alternatives were considered in this DEA: Alternative 1 (No-Action Alternative); Alternative 2 (Relocation and construction of a new campus on an alternate site (west of Corbina Blvd.)), and Alternative 3 (Relocation and construction of a new campus for St. Louis Catholic High School in Lake Charles, Louisiana). (Proposed Action)

#### FINDING OF NO SIGNIFICANT IMPACT

The Proposed Action would not result in any significant adverse impacts related to floodplains, wildlife, state and federally listed threatened and endangered species, and hazardous materials. The Proposed Action as described in the DEA may have short-term, temporary, negligible to minor impacts to geology, topography, soils, wetlands and waters of the U.S., floodplains and hydrology, water quality and resources, land use and planning, air quality, cultural resources, low income and minority populations, noise, and traffic. The Proposed Action may have long-term, permanent, negligible to minor impacts to socioeconomics, wetlands through the unavoidable loss of wetlands and water resources and quality through a temporary increase in suspended solids through stormwater runoff during and after construction. Based on the information analyzed, FEMA has determined that the implementation of the proposed action would not result in significant adverse impacts to the quality of the natural and human environment. The proposed action is not anticipated to have the potential for significant cumulative effects when combined with past, present, and reasonably foreseeable future actions. As a result of this FONSI, an EIS will not be prepared and the proposed action as described in the EA may proceed. All adverse impacts require conditions to minimize or mitigate impacts to the proposed project site and surrounding areas.

#### CONDITIONS

The following conditions must be met as part of this project. Failure to comply with these conditions may jeopardize the receipt of federal funding.

- In accordance with applicable local, state, and federal regulations, the applicant is responsible for acquiring any necessary permits and/or clearances prior to the commencement of any construction related activities.
- FEMA Public Assistance grant funded projects carried out in the floodplain or affecting the floodplain must be coordinated with the local floodplain administrator for a floodplain development permit and the action must be undertaken in compliance with relevant, applicable and required local codes and standards and thereby, will reduce the risk of future flood loss, minimize the impacts of floods on safety, health, and welfare, and preserve and possibly restore beneficial floodplain values as required by Executive Order 11988.
- Fill or borrow material used must be sourced from sites that do not contain any buried cultural materials (*i.e.*, wells, cisterns, foundations, basements, prehistoric Indian artifacts, human burials, and the like). If during the course of work, archaeological artifacts (prehistoric or historic) or human remains are discovered, Plaquemines Parish and/or its contractors must immediately stop work in the vicinity of the discovery and take all reasonable measures to avoid or minimize

harm to the finds. The Applicant and GOHSEP must inform the FEMA Public Assistance program, who would in turn contact the FEMA Historic Preservation staff. The Applicant must not proceed with work until FEMA completes consultation with the SHPO. In addition, if unmarked graves are present, compliance with the Louisiana Unmarked Human Burial Sites Preservation Act is required. In that situation, the Applicant must notify the local law enforcement agency within 24 hours of the discovery, and notify FEMA and the Louisiana Division of Archaeology at (225) 342-8170 within 72 hours of the discovery. Failure to comply with these stipulations may jeopardize FEMA funding of the project.

- If any solid or hazardous wastes, or soils and/or groundwater contaminated with hazardous constituents are encountered during the project, notification to LDEQ's Single-Point-of-Contact at (225) 219-3640 is required. Additionally, precautions should be taken to protect workers from these hazardous conditions.
- To manage fugitive dust resulting from earth-moving activities, storage piles, disturbed surface areas, unpaved sections, and other construction-related operations, the project will employ one or more of the following measures: watering, coverings, wind fencing, haul bed coverings, wheel washers, vegetation, restricted site access, and street sweeping.
- To the greatest extent feasible, the project will endeavor to minimize the disturbed area and preserve the existing vegetation, while also maintaining topsoil whenever possible.
- In compliance with Executive Order 11990, due to the unavoidable impacts and loss of wetlands, compensatory wetland mitigation is required. Compensatory mitigation must be completed prior to, or concurrent with, wetland conversion activities. A minimum ratio of 1 to 1 (acreage) is required. For the wetland impacts associated with this project there is a loss of 6 acres; therefore, 6 acres of wetland mitigation credits must be purchased at an approved mitigation bank. Proof of purchase of mitigation bank credits must be provided to FEMA and GOHSEP. Documentation will be requested at project close out. All credits must be purchased and support wetlands in the State of Louisiana.
- Existing trees and other vegetation within the construction area that might be affected by the public right-of-way will be safeguarded on a case-by-case basis. Protective measures will involve the installation of fencing and appropriate signage. Any necessary trimming, root pruning, or removal of trees or stumps within the public right-of-way due to construction will be minimized and conducted under the supervision of a licensed arborist. If feasible, any trees

removed from the construction site within the public right-of-way will be relocated to an area near the project site. Any disturbed existing vegetation or ground cover resulting from construction activities will be restored through seeding and fertilization.

- Per Louisiana Administrative Code 1-315 B.6, the Society of the Roman Catholic Church of the Diocese of Lake Charles would be required to plant two trees for every tree removed.
- The contractor will be responsible for developing and maintaining a comprehensive Storm Water Pollution Prevention Plan (SWPPP) that outlines the Contractor's strategies to prevent stormwater collection system contamination during the project. Each project's SWPPP will align with the requirements of the Municipal Separate Storm Sewer System (MS4) Permit for the area. Contractors must take all necessary precautions to prevent the entry of fuels, oils, asphalt, concrete, chemicals, and other hazardous materials into the drainage system and groundwater table as per relevant specifications. Implementation of Storm Water Control Measures (SCMs) will encompass safeguarding the storm drain system, spill prevention and cleanup, employee training, site cleanliness, and temporary erosion controls. Residues from dust collectors, concrete mixers, vehicle wash racks, and entrance/exit debris will be appropriately disposed of at an approved disposal facility.
- Create stabilized construction entrances and exits utilizing methods such as employing large, crushed rocks, stone pads, steel wash racks, hose-down systems, and pads to effectively manage construction-related traffic and minimize environmental impact.
- Calcasieu Parish's Code of Ordinances has made unlawful the operation of "any equipment used in construction work within one hundred sixty-five (165) feet of any residential or noise-sensitive area between sunset and sunrise on weekdays and Saturdays, and 9:00 p.m. to 8:00 a.m. on Sundays and holidays, except for emergency work". Additionally, all construction machinery and vehicles must be equipped with effective sound muffling devices and operated in a manner that minimizes noise while ensuring efficient work performance. Activities in the vicinity of noise and vibration-sensitive areas, such as churches, hospitals, and schools, will be minimized to the extent practically feasible.
- Guarantee the proper maintenance of equipment, which includes regular engine upkeep, ensuring adequate tire inflation, and the proper maintenance of pollution control devices.

- Implement thorough monitoring and control of construction traffic as necessary. Ensure that all construction operations adhere to the safety regulations outlined in the Occupational Safety and Health Act (OSHA). Provide a minimum of 48 hours' notice to residents and emergency response agencies before any street closures and expected areas of reduced water pressure.
- The project construction may entail the handling of potentially hazardous materials, such as petroleum products, cement, caustics, acids, solvents, paint, electronic components, pesticides, herbicides, fertilizers, and treated timber, which could lead to the generation of limited quantities of hazardous wastes. It is imperative to implement suitable measures to prevent, minimize, and manage the occurrence of spills involving hazardous materials. Moreover, any hazardous and non-hazardous wastes generated during the construction process must be disposed of in strict accordance with the pertinent regulations at the Federal, state, and local levels.
- To mitigate indirect effects such as erosion, sedimentation, dust, and other disturbances associated with the construction, the contractor needs to adhere to all relevant local, state, and federal regulations about sediment control, solid waste disposal, spill management, and the release of surface runoff and stormwater into nearby waters of the U.S. and surrounding drainage areas.
- Ensure that all new construction adheres to current codes and standards. By 44 C.F.R. § 9.11(d)(6), projects must not be constructed in a floodplain management standard that offers less protection than what the community has adopted through its participation in the National Flood Insurance Program. It is the responsibility of the applicant to coordinate all construction activities with the local floodplain administrator regarding floodplain permit(s) before commencing any activities and to maintain compliance with officially adopted local floodplain ordinances. Documentation of all coordination related to these permit(s) should be provided to the local floodplain administrator, the Louisiana Governor's Office of Homeland Security and Emergency Preparedness (LA GOHSEP), and FEMA as part of the permanent project file. Under 44 CFR 9.11 (d) (9), whenever feasible, mitigation or minimization standards should be implemented.
- If human bones or unmarked grave(s) are discovered within the project area, adherence to the Louisiana Unmarked Human Burial Sites Preservation Act (R.S. 8:671 et seq.) is mandatory. The applicant is responsible for promptly informing the law enforcement agency of the relevant jurisdiction within twenty-four hours of the discovery. Additionally, FEMA and the Louisiana Division of Archaeology can be notified at 225-342-8170 within seventy-two hours of the discovery.

- If archaeological artifacts, whether prehistoric or historic, are discovered during the project's execution, the applicant must halt work in the proximity of the finding and implement all necessary measures to mitigate potential damage. It is imperative that the applicant promptly notifies their designated Public Assistance (PA) contacts at FEMA, who will subsequently engage FEMA's Historic Preservation (HP) staff. Work should not resume until FEMA HP concludes consultation with the State Historic Preservation Officer (SHPO) and any other relevant parties.
- Bald eagles, having made a remarkable recovery, were removed from the List of • Endangered and Threatened Species on August 8, 2007. Despite this change in status, it is crucial to note that bald eagles remain safeguarded under the Bald and Golden Eagle Protection Act (BGEPA) (16 U.S.C. 668 et seq.). To aid in the preservation of these majestic birds, the Service has formulated the National Bald Eagle Management (NBEM) Guidelines, designed to equip landowners, land managers, and others with comprehensive information and recommendations to mitigate potential project impacts on bald eagles. Particularly, these guidelines focus on preventing any form of "disturbance," which is strictly prohibited under the BGEPA. Outlined in the NBEM Guidelines are the following recommendations: (1) maintaining a designated distance between the project's activity and the nest (buffer area); (2) preserving natural areas, preferably forested, between the project's activities and nest trees (landscape buffers); and (3) avoiding specific activities during the breeding season. All personnel on-site must be made aware of the potential presence of nesting bald eagles within the project area. In the event of the discovery of such nests within or adjacent to the proposed project area, it is essential to conduct an assessment to ascertain whether the project is likely to disturb the nesting bald eagles. Any discovery of a bald eagle nest should be immediately reported to the relevant authorities.
- The US Fish and Wildlife Service on October 8, 2020, recommended reclassifying the red-cockaded woodpecker as a threatened species. This proposal included a section 4(d) rule outlining specific prohibitions and exceptions that we deemed necessary and advisable for the conservation of the red-cockaded woodpecker. Initially, these prohibitions involved the restriction of incidental take resulting from the damage or conversion of currently occupied red-cockaded woodpecker nesting and foraging habitat. Additionally, forest management practices within these habitats were to be restricted. The operation of vehicles or mechanical equipment, use of floodlights, and human presence within an active cavity tree cluster during the red-cockaded woodpecker breeding season were also proposed to be prohibited. Moreover, the installation of artificial cavity inserts, drilled cavities, or cavity restrictor plates, as well as activities that render active cavity trees unusable to red-cockaded woodpeckers, were included in the proposed restrictions. The use of insecticides or herbicides on any standing pine

tree within 0.50 miles from the center of an active cavity tree cluster of redcockaded woodpeckers was also prohibited (85 FR 63498, October 8, 2020). To further protect the red-cockaded woodpecker's habitat, the following additional measures are suggested: Restricting vehicle use on existing roads and avoiding the construction of new roads and trails within clusters. Limiting silvicultural and cultural operations to daylight hours, with an emphasis on avoiding activities within 1-2 hours of dawn and dusk. Permitting mechanized equipment in a cluster during the non-breeding season for red-cockaded woodpecker management activities only. Prohibiting habitat management activities other than prescribed burning during the breeding season (April – July).

#### Public Review and Comment

The EA can be viewed and downloaded from FEMA's website at <u>www.fema.gov/plan/ehp/envdocuments/ea-region6.shtm.</u> The EA was also available for public review at the [name of facility, address]. A legal notice was posted in the local newspaper on XX date through XX date. No substantive comments were received; therefore the Draft EA will become final and the initial Public Notice will also serve as the final Public Notice.

### APPROVAL AND ENDORSEMENT

Date _____

Latoya Leger Regional Environmental Officer Louisiana Integration and Recovery Office (LIRO)

Date _____

Arsany Thomas Recovery Division Director FEMA Region 6